

New Generation of Uncertainty Analysis in Basin Modeling*

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Search and Discovery Article #42508 (2020)**

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Abstract

Basin modelling englobes a range of geological disciplines which are used to describe the formation and evolution of sedimentary basins, often but not exclusively, to assess their potential for exploration and production of hydrocarbons. Understanding and being able to evaluate the uncertainties on a model are the key to deliver pertinent and in-depth analysis of the results as none of them can truly represent the reality. Current methods are based on advanced mathematical and statistical concepts that are applied on the dozens of physical parameters integrated in models to generate alternative scenarios. They stand up particularly effective when they are mastered but require a lot of experience in basin modelling as much as non-geological related field. Therefore, they remain used by a small community of experts instead of being widely adopted in E&P processes. Furthermore, the oil and gas industry face the dilemma that many of these experts will retire in the next few years without necessarily being able to pass the torch. This paper aims to present an innovative approach in basin modelling risk and uncertainty analysis. By using already developed advanced statistics optimization approaches and combining it with a new parametrization procedure based on well-known geological concepts instead of independent variables, this new workflow is designed to reach a wider and less experienced community while downsizing computing time and remaining agile and pertinent. The methodology identifies the key-elements of the petroleum system and guides the users in their estimations of the uncertainty based on the geological context in association with geological concepts coming from literature. Thus, it reduces the uncertainty evaluation to a few known concepts. In illustration of the general parametrization procedure, three new specific methodologies to assess the richness, the reactivity and the thickness of a source-rock are described following the philosophy of the workflow. They have been tested on a real case study over the Levantine Basin and present promising results as they required 50 times fewer simulations than Monte Carlo approach to provide results coherent with expected geological contexts and physical behaviors of the basin.

NEW GENERATION OF UNCERTAINTY ANALYSIS IN BASIN MODELING

PIERRE HACQUARD, MATTHIEU DUCROS, RENAUD TRABY, VÉRONIQUE
GERVAIS, NICOLAS MAURAND*



WHY AN EVOLUTION IS NEEDED?



Uncertainty analysis is done by **Experts** only



Small Community



Not a reflex in E&P processes

Evolution through a **Non-Expert** based experience

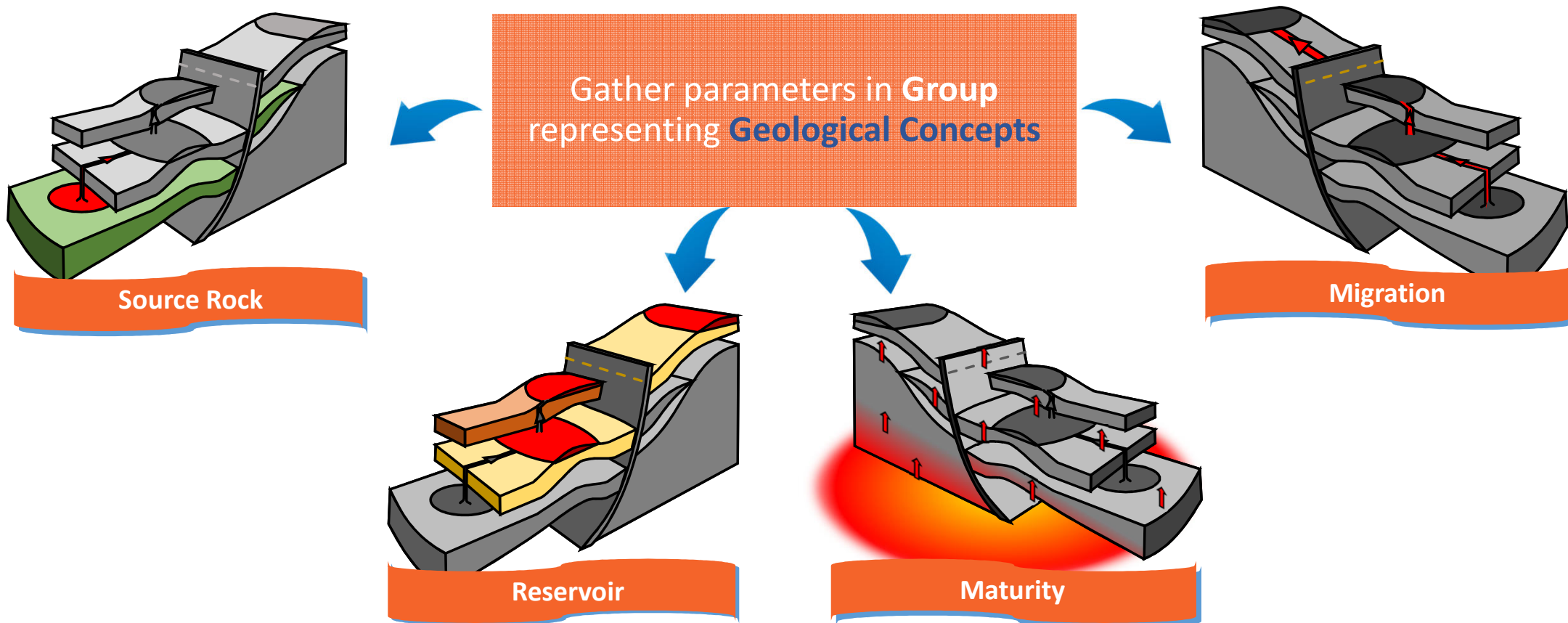


Bigger Community

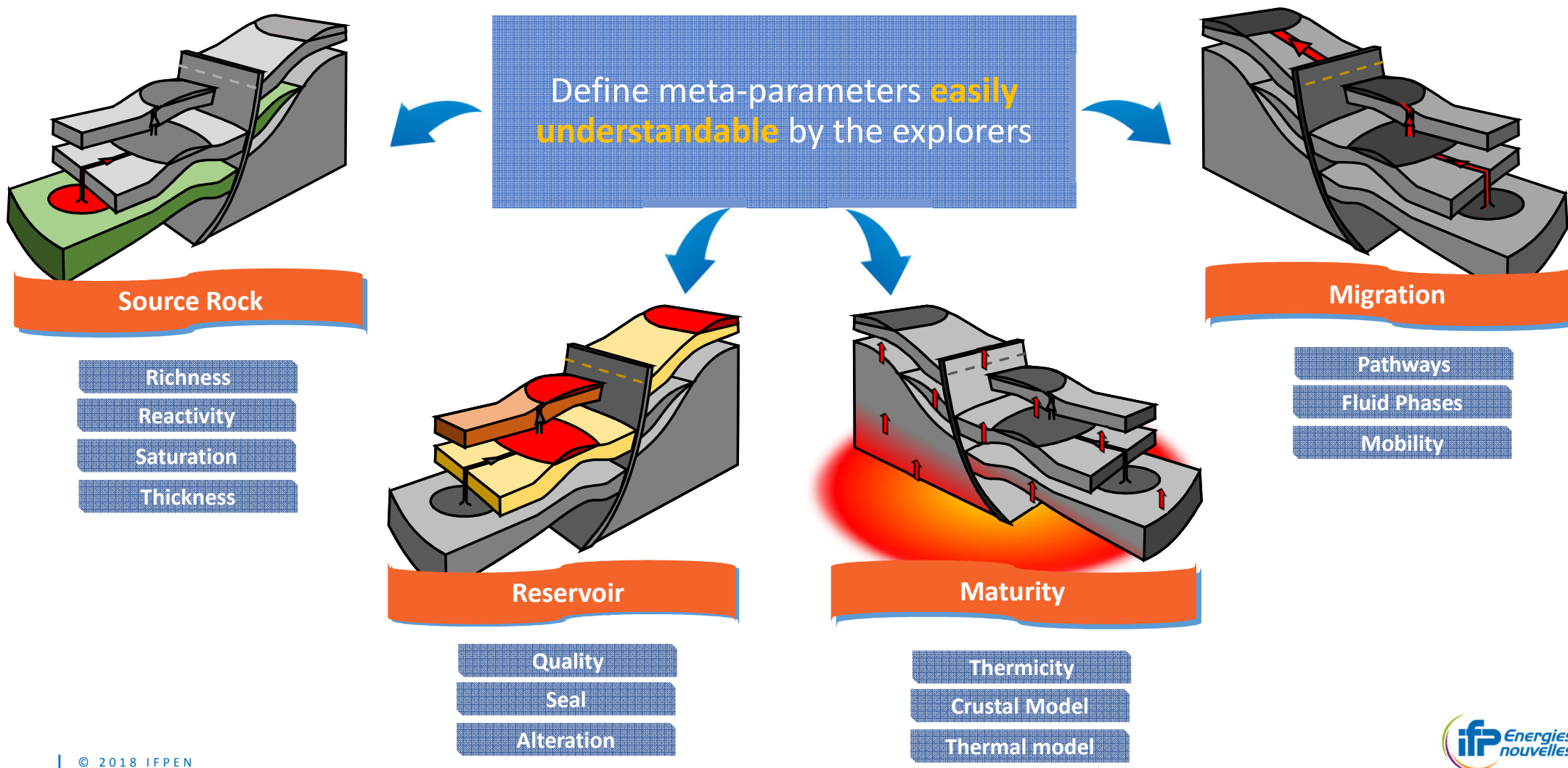


Systematic integration in E&P processes

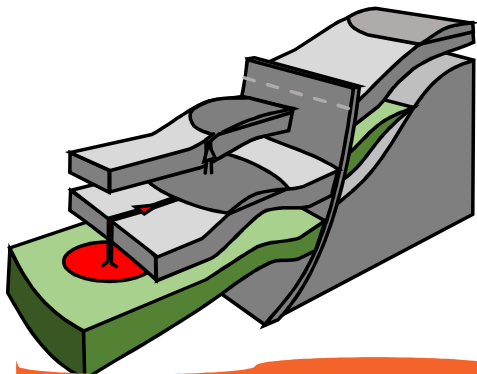
NEW APPROACH



NEW APPROACH

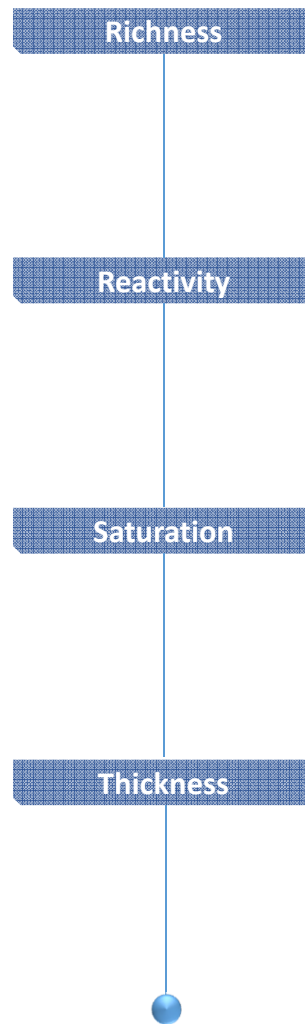


NEW APPROACH

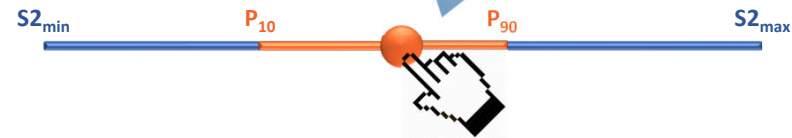


Source Rock

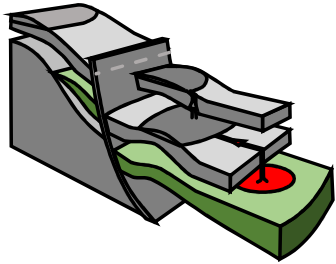
Define the uncertainties bounds in which each parameter evolve



The user modify the parameters **without worrying about process**



METHODOLOGY



Source Rock

Richness

Reactivity

Saturation

Thickness

For each **Meta-Parameter** we need to define :

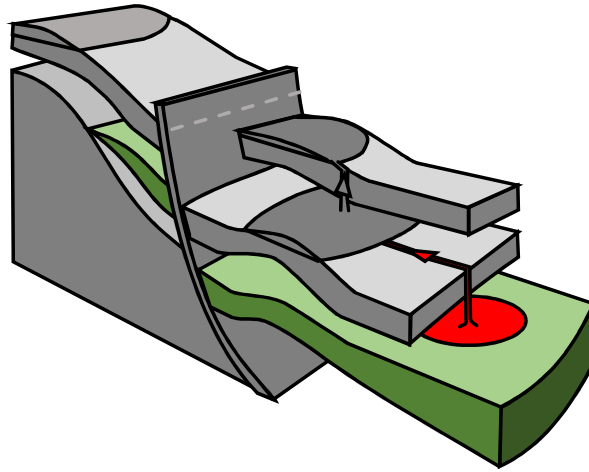
Parameters to include : TOC, IH etc...

Relation between parameters : TOC vs IH etc...

Methodology to evaluate the uncertainty on the Meta-Parameter



**DIFFERENT FOR EACH
META-PARAMETER**



GROUP : SOURCE-ROCK

META-PARAMETERS DETERMINATION AND UNCERTAINTY ANALYSIS

Richness

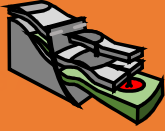
Reactivity

Thickness



PARAMETERS SELECTION

SOURCE-ROCK RICHNESS



Parameters available in a Basin Model:

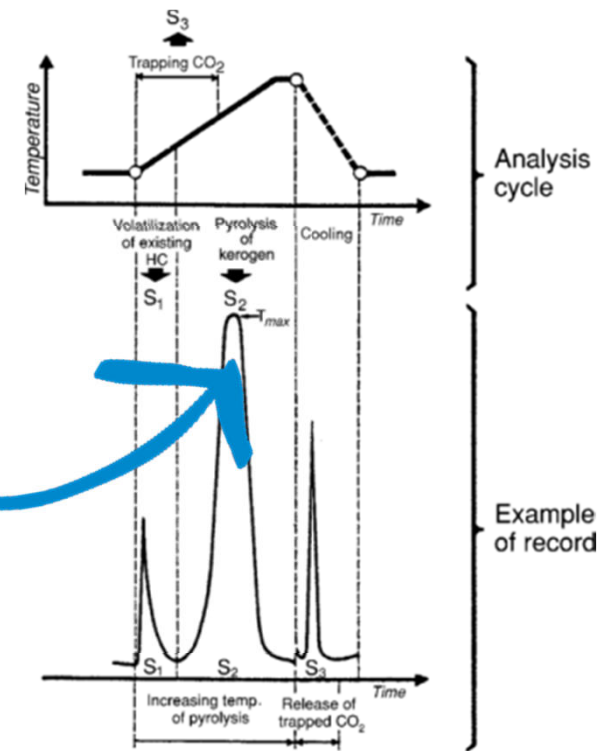
IH *TOC*

The richness meta-parameter must be a function of **IH** and **TOC**

$$S2 = IH \times TOC$$

with :

- **IH** : Hydrogen Index (mg HC/gC)
- **TOC** : Total Organic Content (mg C/ g rock)



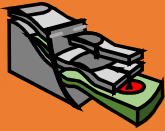
Typical RockEval pyrolysis. Tissot, 1984

RELATION BETWEEN PARAMETERS

Is there a correlation between **IH** and **TOC**?

If yes, how to model it?

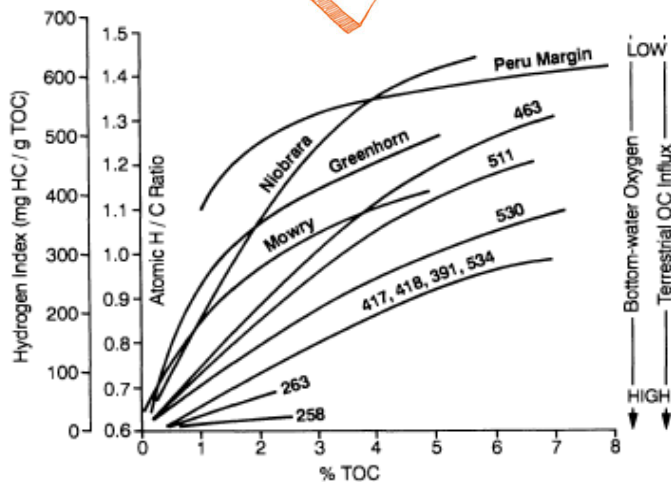
SOURCE-ROCK
RICHNESS



Bibliography : ✓



Modelization of **IH** vs **TOC**
using available data in
TemisFlow



Tyson, 2001

$$IH = a \frac{TOC}{1 + bTOC}$$

$$a = \frac{2 \times IH_{ini}}{TOC_{ini}}$$

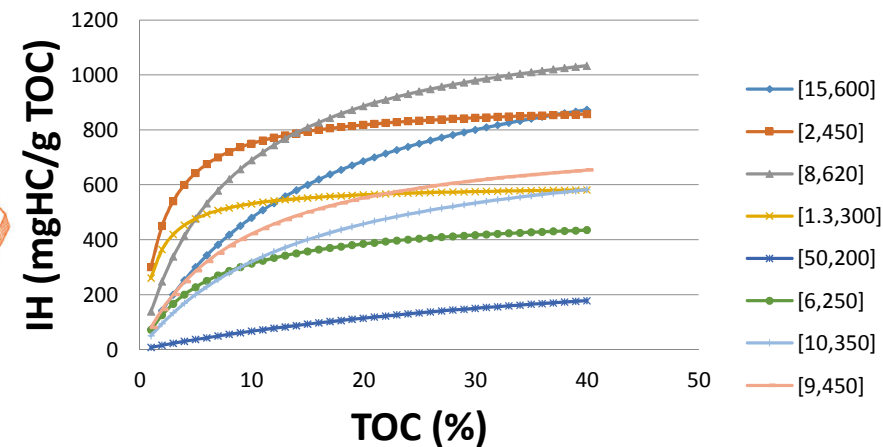
$$b = \frac{1}{TOC_{ini}}$$



Model : ✓



Modelization results for different [TOC,IH]

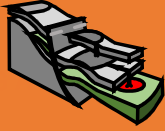


IH and **TOC** are correlated

The model is coherent

UNCERTAINTY EVALUATION METHODOLOGY

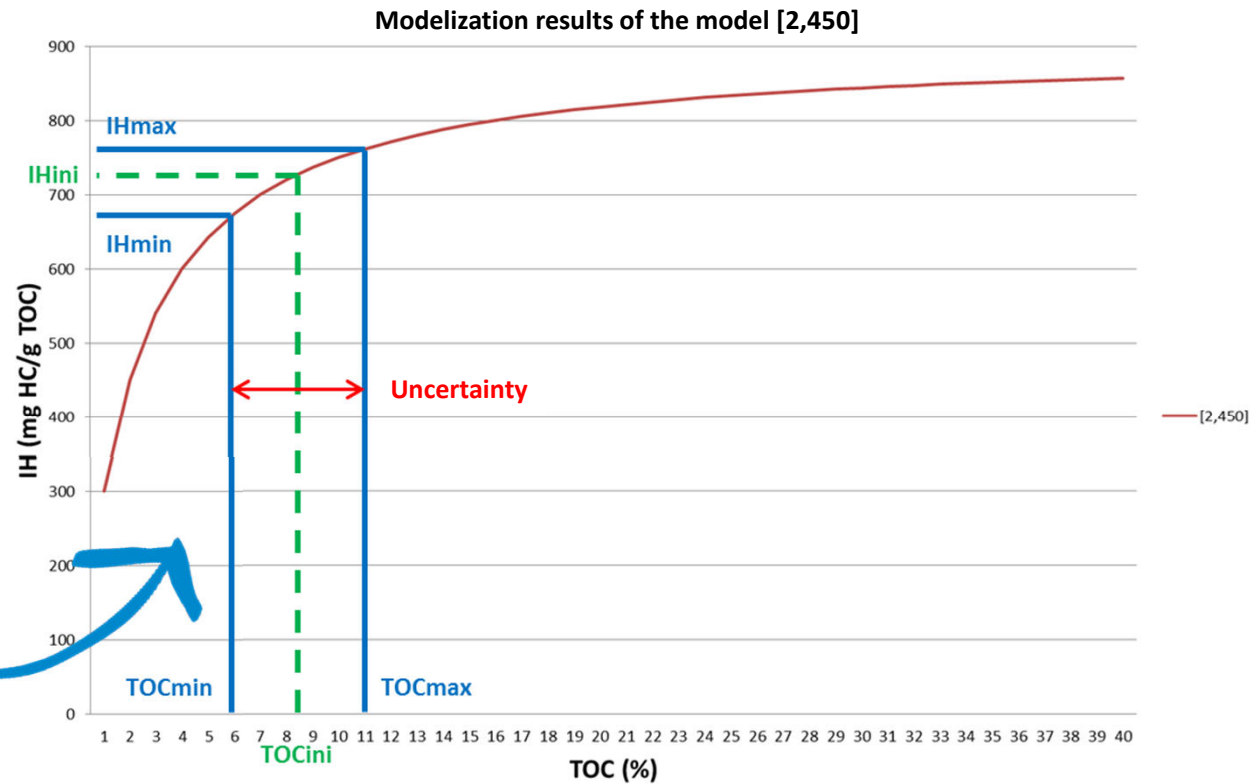
SOURCE-ROCK
RICHNESS



We now have a model correlating **IH** and **TOC**.



The uncertainty on the **TOC** or **IH** is enough to have the uncertainty on Richness.

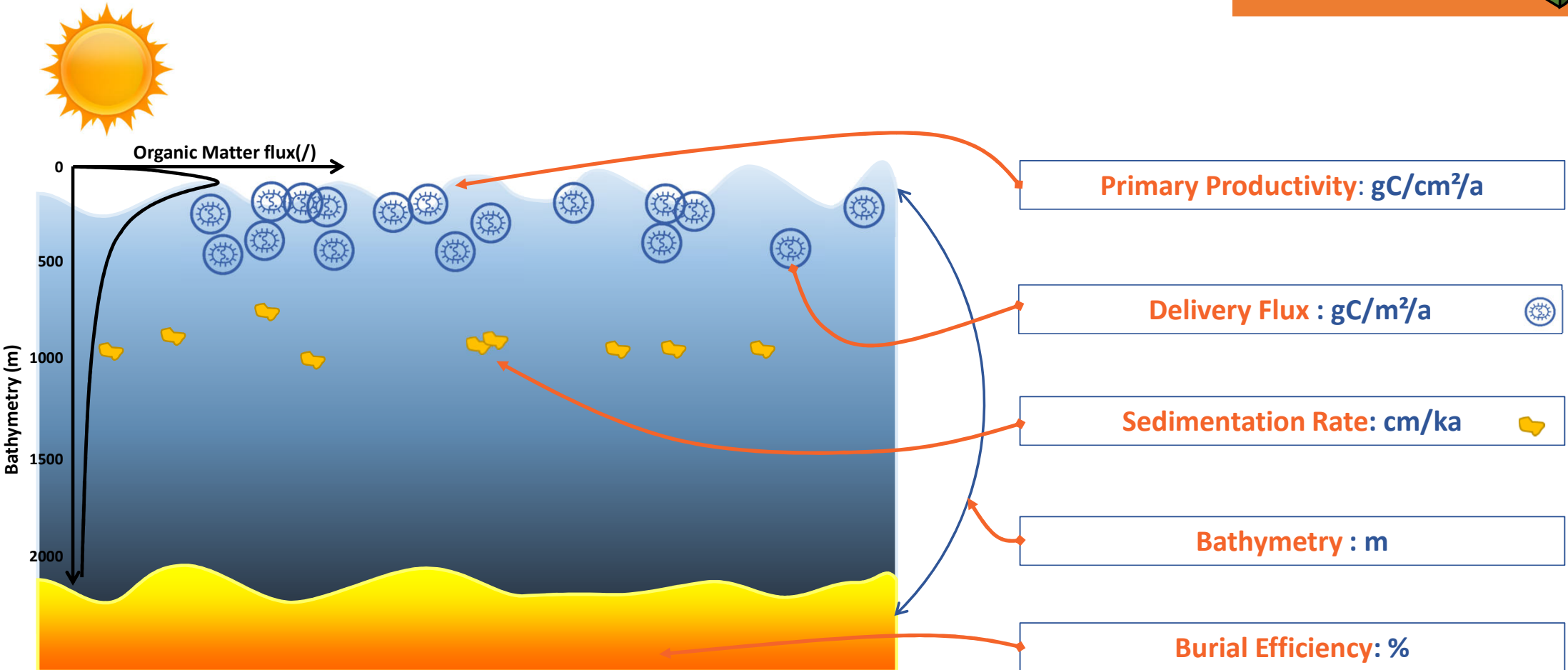
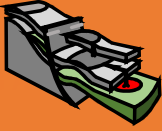


In our approach, the uncertainty on **TOC** is going to be determined

TOC

What are the parameters controlling the TOC ?

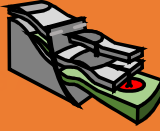
SOURCE-ROCK
RICHNESS



Hacquard, 2017

COMPUTING THEORETICAL TOC (TYPE II)

SOURCE-ROCK
RICHNESS



Delivery Flux (DF) :

$$DF = 9 \times \frac{PP}{H} + \frac{0,7 \times PP}{\sqrt{H}}$$

Bett & Holland, 1991



Burial Efficiency (BE) :

$$\text{Log}(BE) = \frac{1,39 \text{Log}(S)}{\text{Log}(S + 7,9) + 0,34}$$

Bett & Holland, 1991

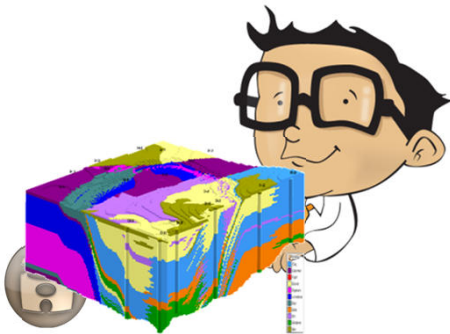


Theoretical TOC:

$$TOC = \frac{BE \times DF}{S \times 1000 \times \rho_{\text{Roche}}}$$

Tyson, 2001

Given by the user:

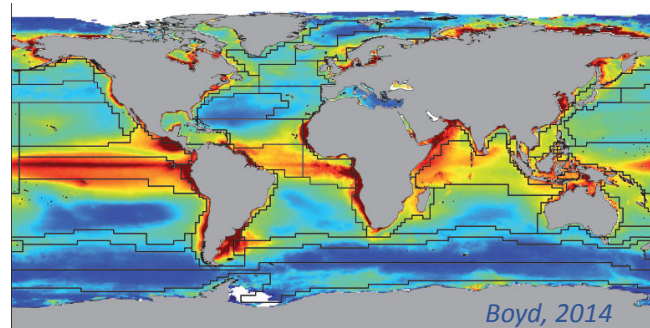


Sedimentation Rate (S) ✓

Density (ρ_{Roche}) ✓

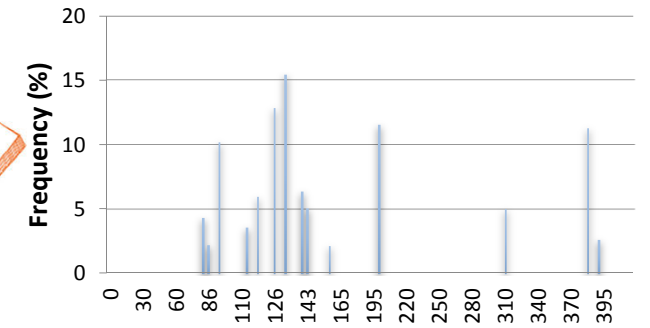
Bathymetry (H) ✓

Primary productivity (PP) ✗



NPP (g C m⁻² y⁻¹)

Primary Productivity is not **Uniform**
at the surface of the oceans



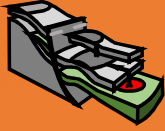
Primary Productivity (gC/cm²/a)

Longhurst
, 1995

We can determine the **frequency**
of the different PP values at the
surface of the ocean

APPLICATION CASE : LEVANTINE BASIN

SOURCE-ROCK
RICHNESS

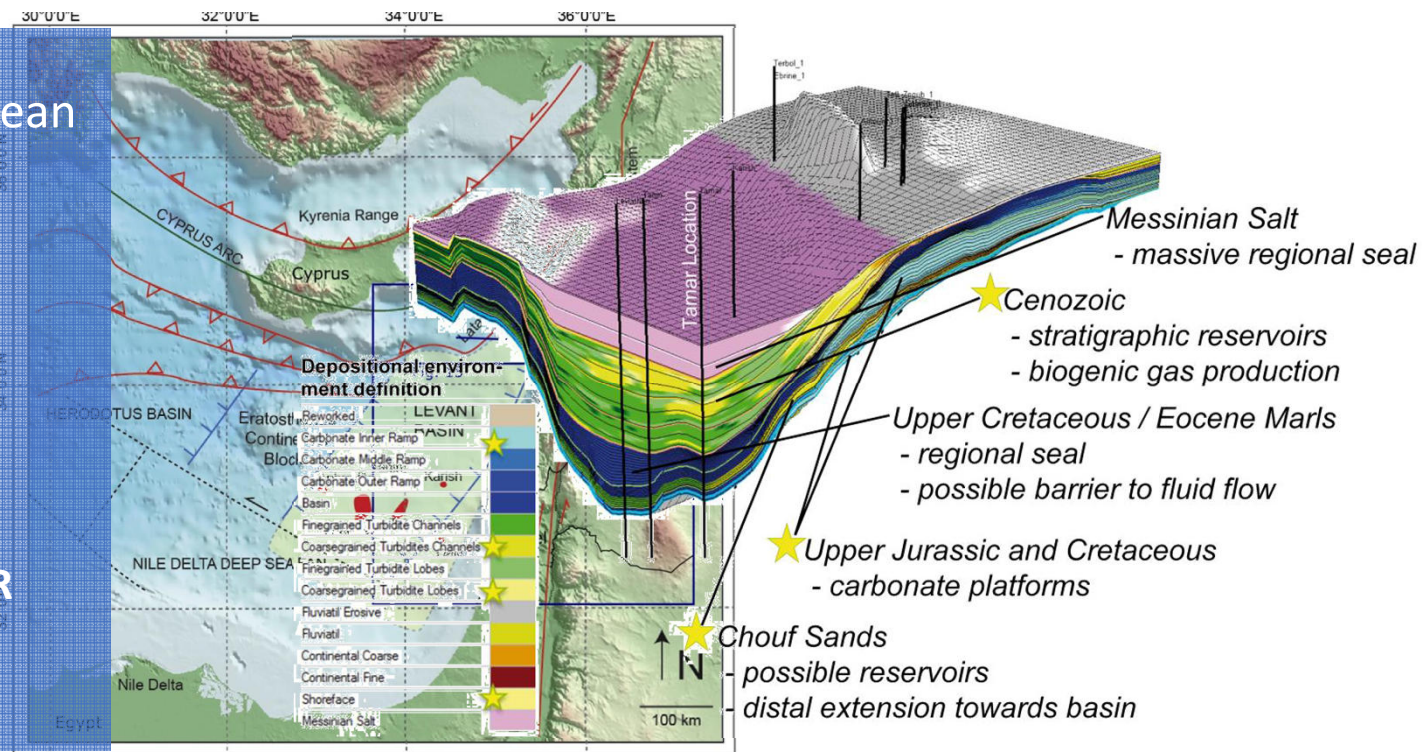


We need **to test** the methodology

- A **Frontier** basin in Mediterranean
- Recent **Giant** discoveries
- A **Lot** of uncertainties
- At least **5 source-rock**



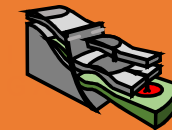
Analysis on the Cenomanian SR



Hawie, 2014

APPLICATION CASE : LEVANTINE BASIN - CENOMANIAN SR

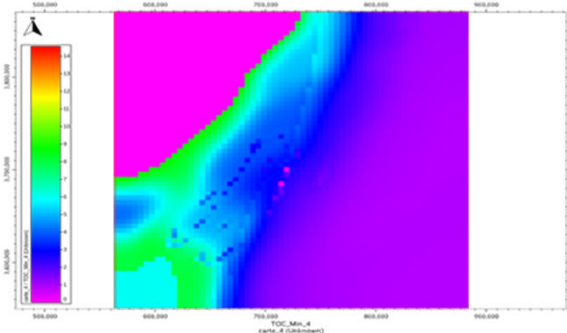
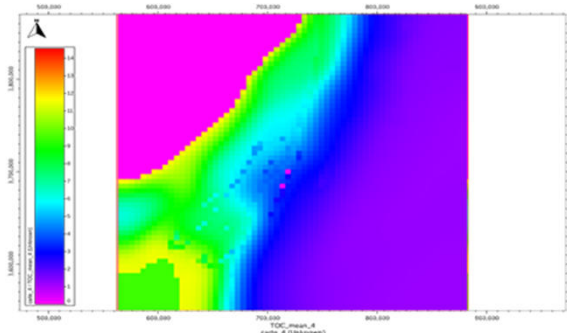
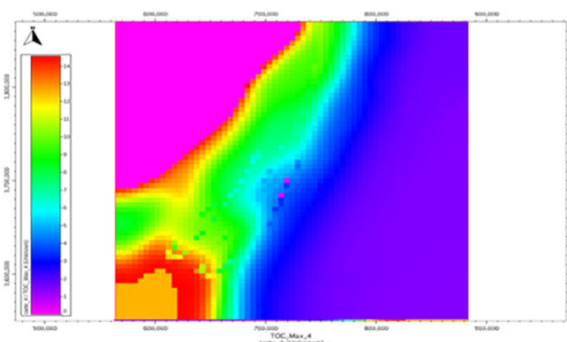
**SOURCE-ROCK
RICHNESS**



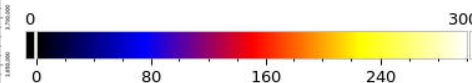
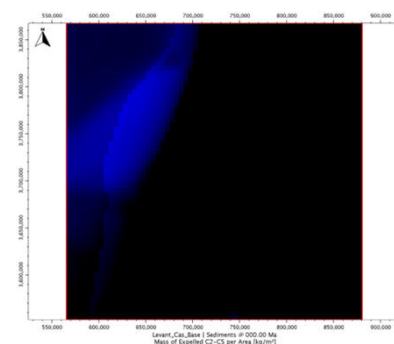
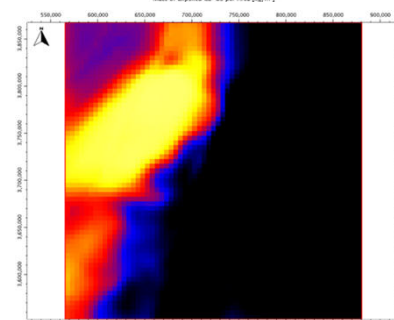
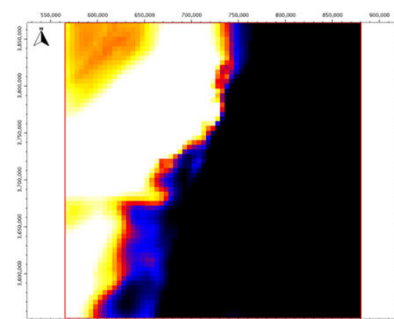
TOC_{max}

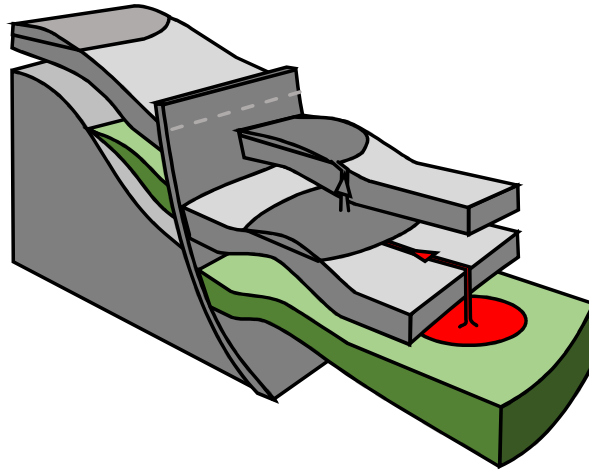
TOC_{User}

TOC_{min}



Expelled
masses





GROUP : SOURCE-ROCK

META-PARAMETERS DETERMINATION AND UNCERTAINTY ANALYSIS

Richness

Reactivity

Thickness



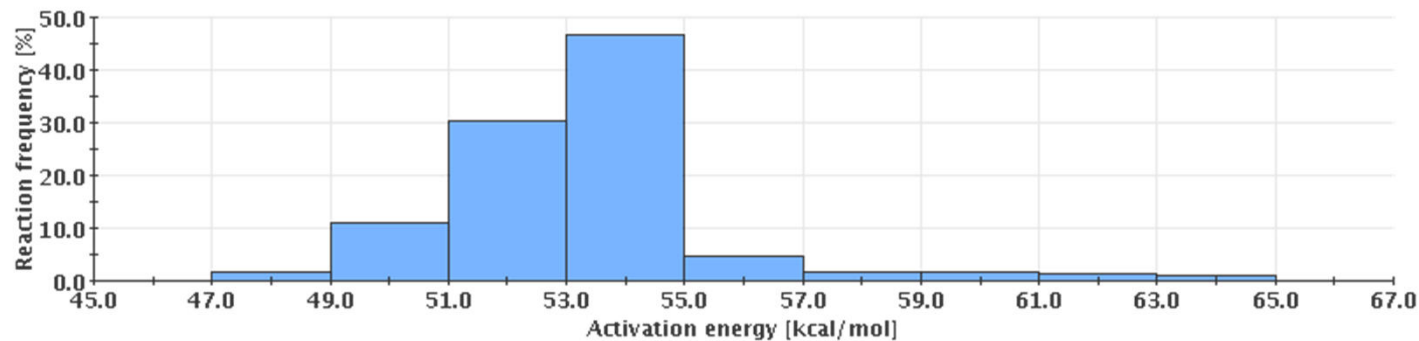
PARAMETER SELECTION

Arrhenius Law:

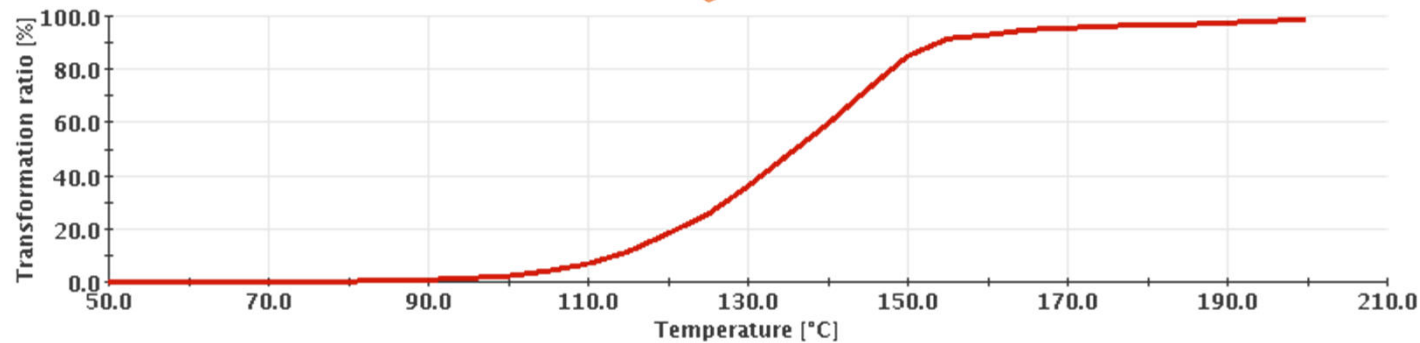
$$K = A e^{\frac{-E}{RT(t)}}$$

- **A** : Pre-Exponential factor (s⁻¹)
- **E** : Activation Energy (kJ/mol)

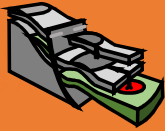
■ Reaction frequency



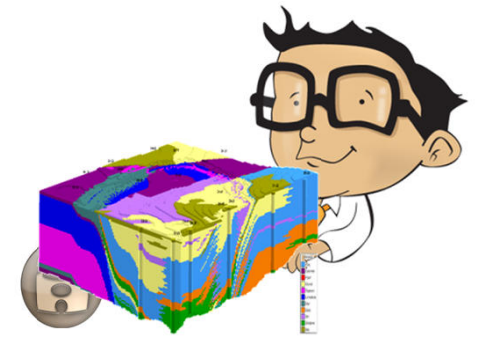
— Transformation ratio of Ebberston



SOURCE-ROCK
REACTIVITY



Given by the user:

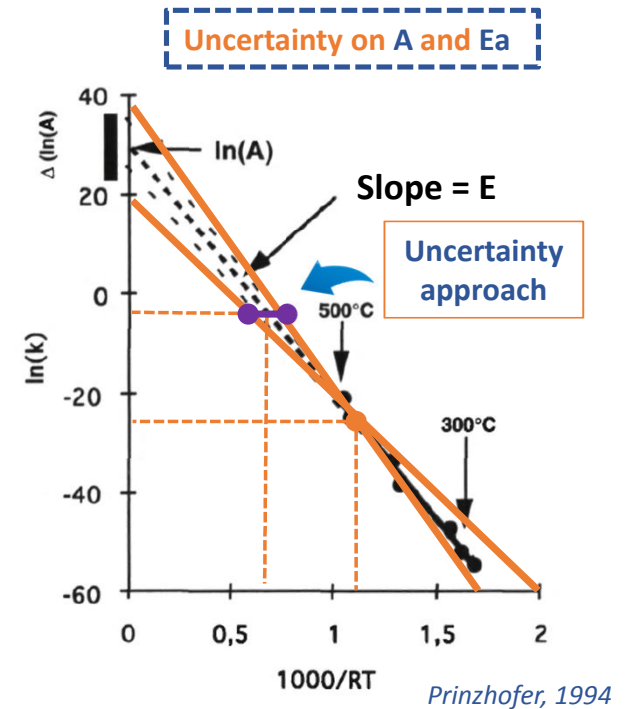
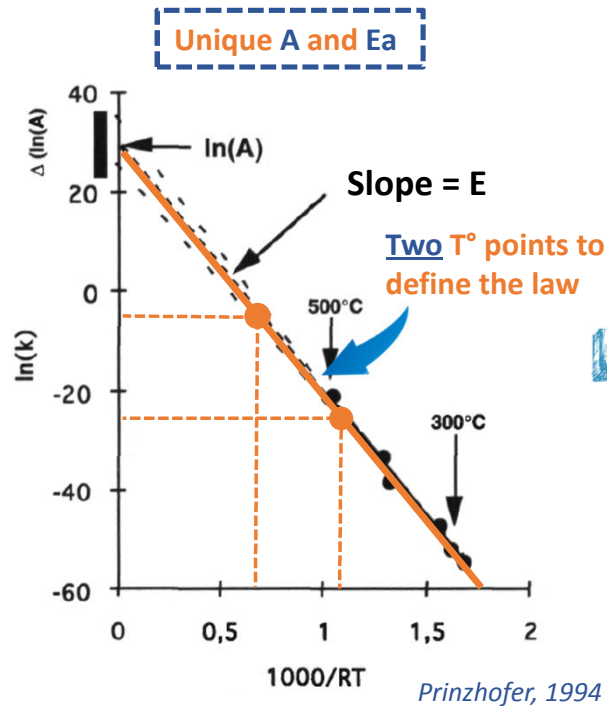
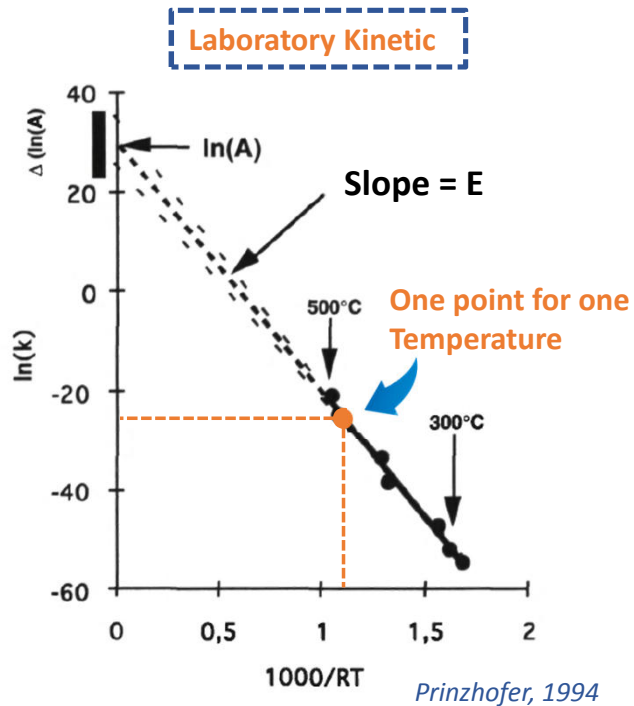
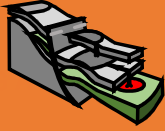


Activation Energies (**E**) ✓

Pre-exponential Factor (**A**) ✓

UNCERTAINTY EVALUATION METHODOLOGY

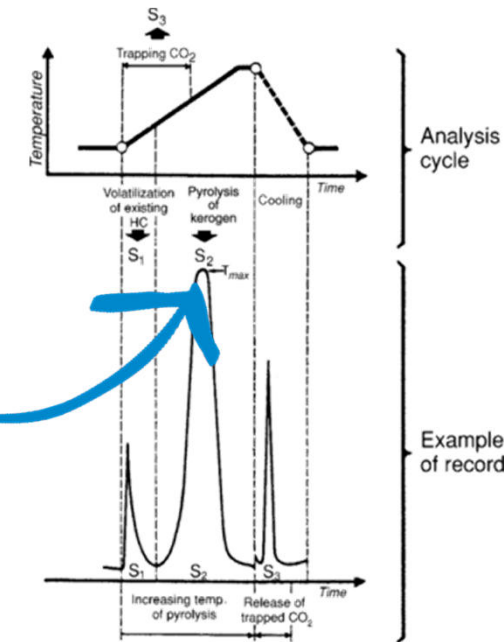
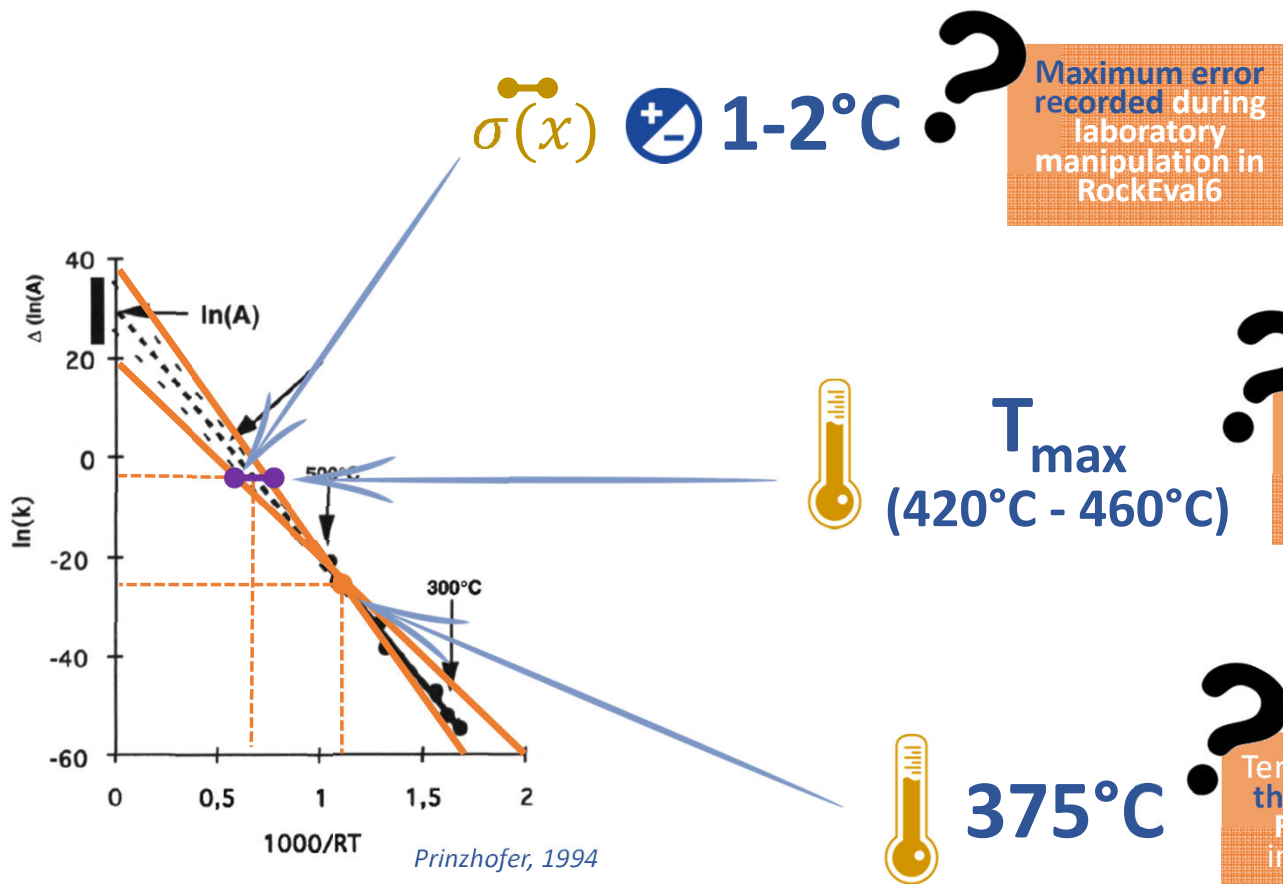
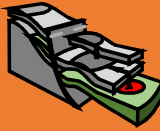
SOURCE-ROCK
REACTIVITY



To apply this methodology **we need two temperatures** that can be applied on **all the Source-Rocks**, and an uncertainty for one of them

UNCERTAINTY EVALUATION METHODOLOGY

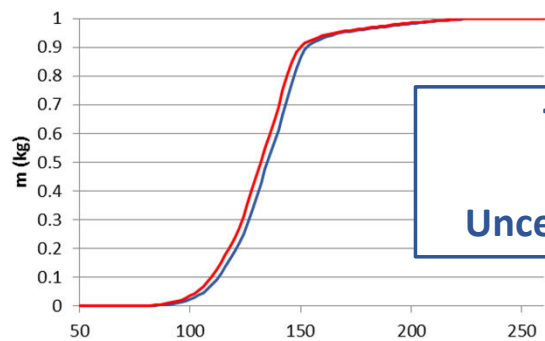
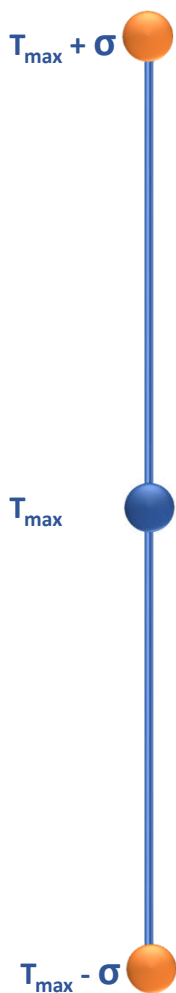
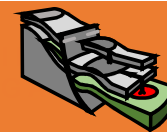
SOURCE-ROCK REACTIVITY



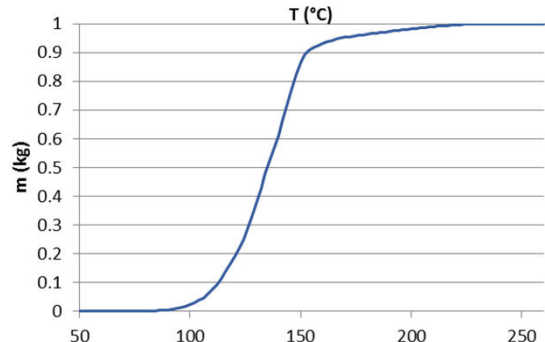
Typical RockEval pyrolysis. Tissot, 1984

APPLICATION CASE : LEVANTINE BASIN - CENOMANIAN SR

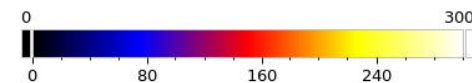
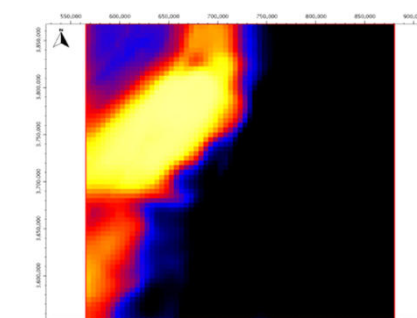
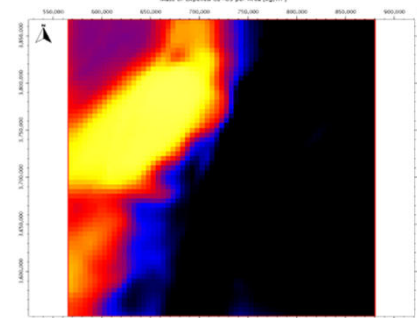
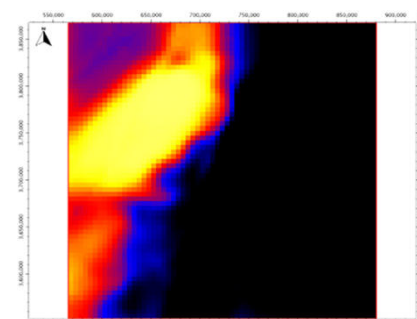
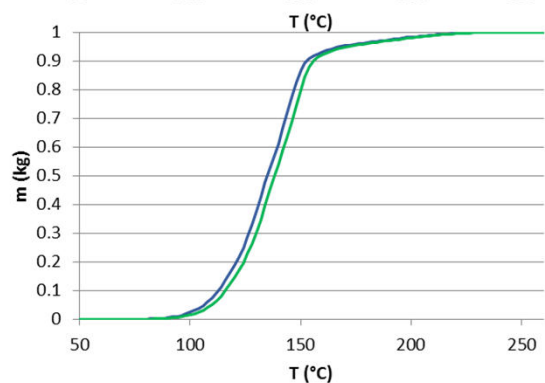
SOURCE-ROCK REACTIVITY

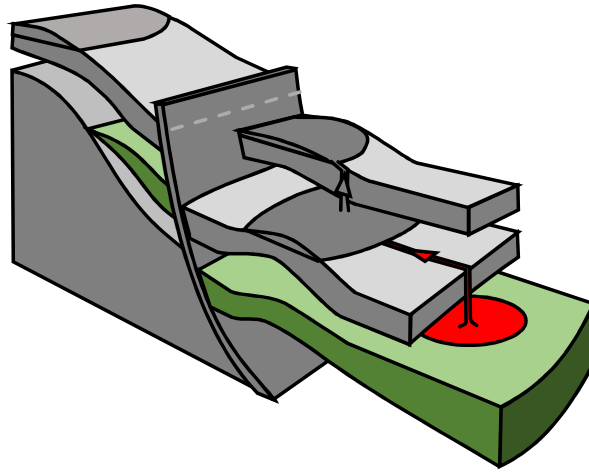


$T_{\max} = 420^{\circ}\text{C}$
 $T_{\text{fixe}} = 375^{\circ}\text{C}$
 Uncertainty = $\pm 1^{\circ}\text{C}$



Expelled masses





GROUP : SOURCE-ROCK

META-PARAMETERS DETERMINATION AND UNCERTAINTY ANALYSIS

Richness

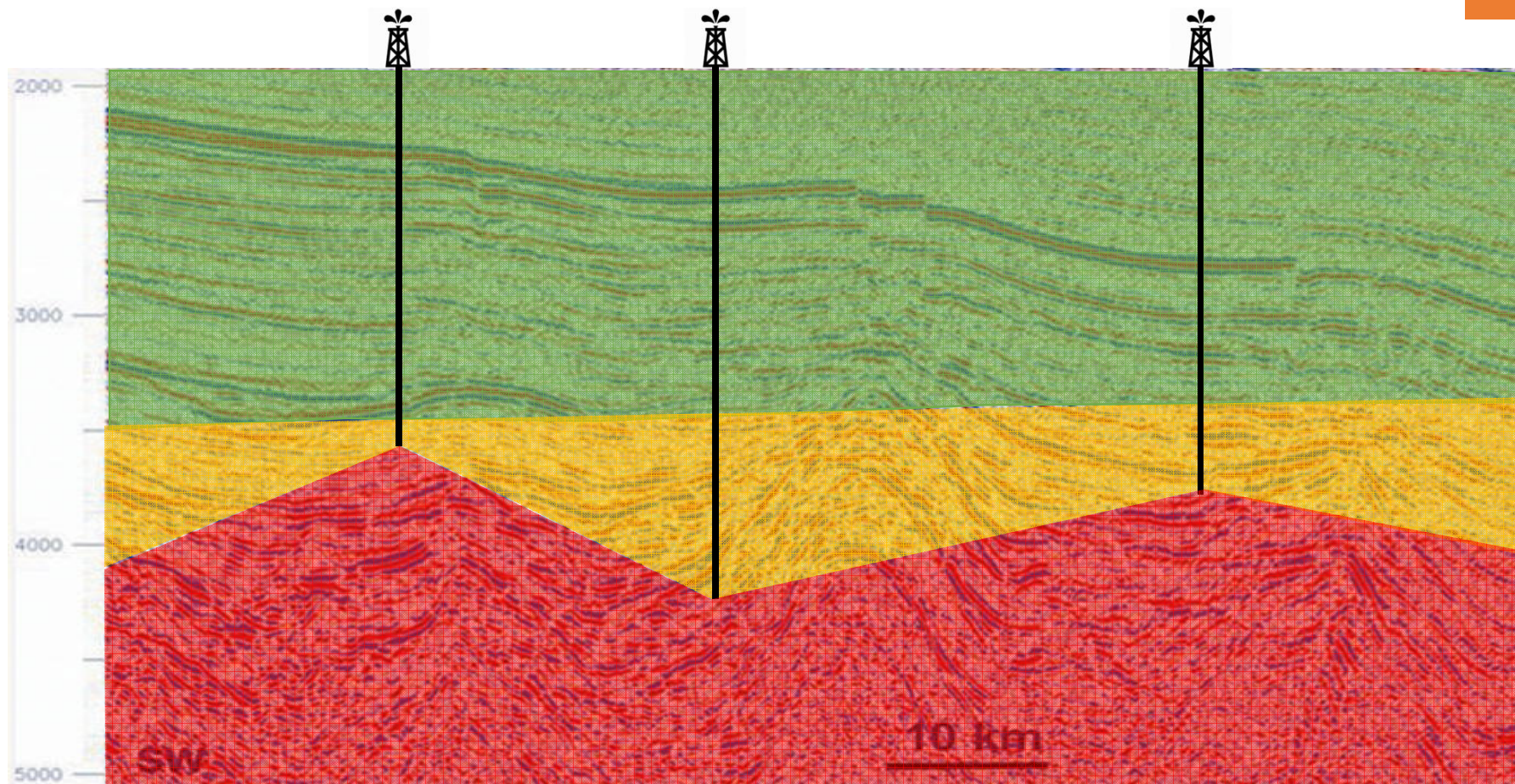
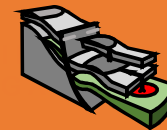
Reactivity

Thickness



REALIABILITY OF THE THICKNESS

SOURCE-ROCK
THICKNESS



Good

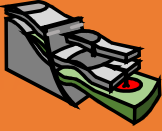


How **important**
can be the
uncertainties
in a 3D Model?

Bad

UNCERTAINTY EVALUATION METHODOLOGY

SOURCE-ROCK
THICKNESS



5-10 %

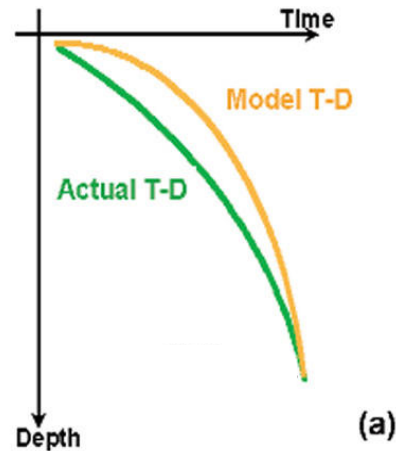
Maximum

Bibliography : ✓

Landro 2001 , Niewland 2007



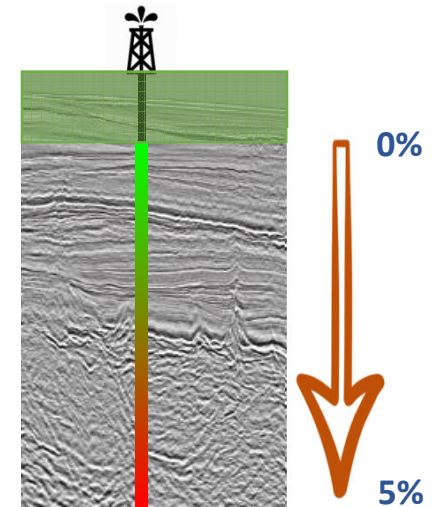
Error in Velocity Model



5 %



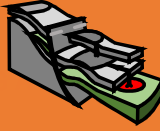
Distance from last Well



0 - 5 %

APPLICATION CASE : LEVANTINE BASIN - CENOMANIAN SR

SOURCE-ROCK THICKNESS

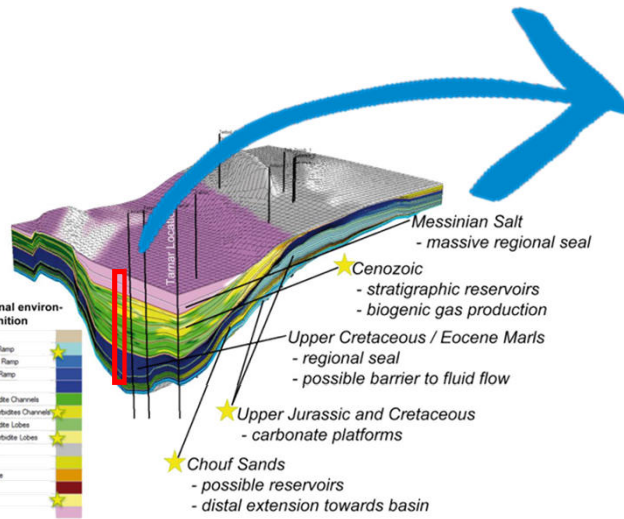
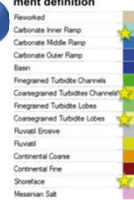


Thickness_{max}

Thickness_{User}

Thickness_{min}

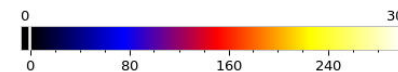
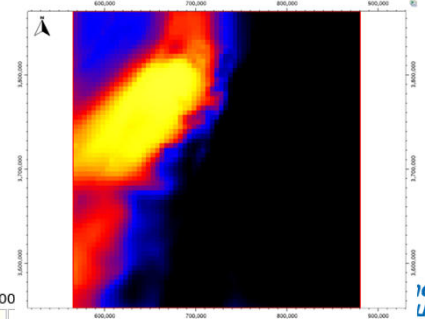
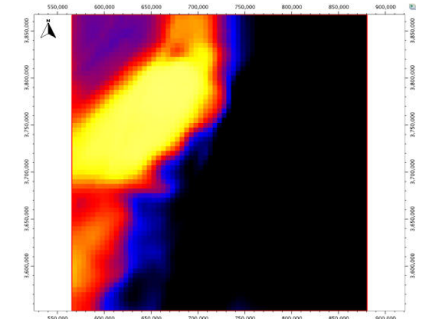
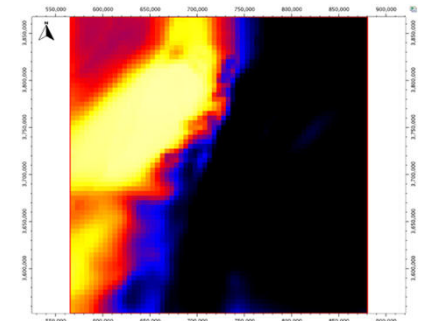
Depositional environment definition



MINIMUM
238
374
622
830
1005
1188
1207
1490
1645
1826
2043
2323
2436
2524
2639
2745
2949
3233
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4365
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4580
4617
4987
5235
5329
5381
5709
6077
6287

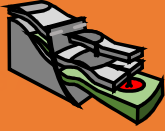
MAXIMUM
263
414
688
918
1111
1314
1334
1646
1819
2018
2259
2567
2692
2790
2917
3033
3259
3573
3663
4047
4258
4589
4825
4949
5062
5103
5511
5787
5889
5947
6309
6717
6949

Expelled masses



FURTHER WORK: LEVANTINE BASIN (COUGAR ANALYSIS)

SOURCE-ROCK Further Work



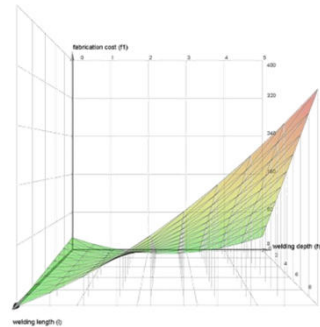
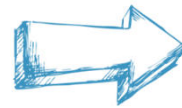
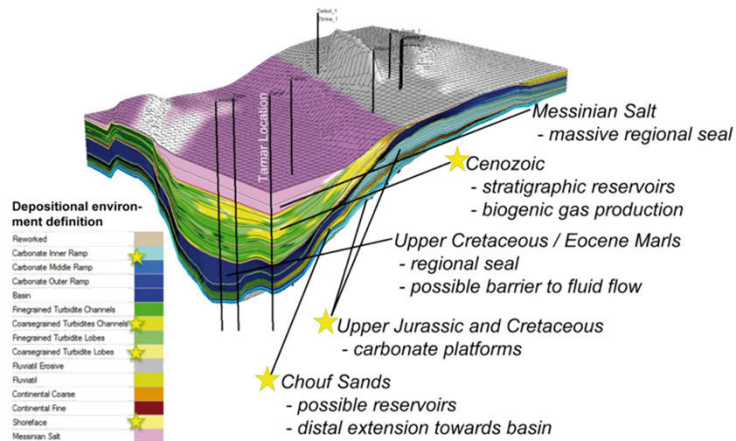
Richness



Reactivity



Thickness



RESPONSE AREA

CAS 1

$S2_{min}$ P_{10} P_{90} $S2_{max}$

T_{min} P_{10} P_{90} T_{max}

H_{min} P_{10} P_{90} H_{max}

CAS 2

$S2_{min}$ P_{10} P_{90} $S2_{max}$

T_{min} P_{10} P_{90} T_{max}

H_{min} P_{10} P_{90} H_{max}

CAS 3

$S2_{min}$ P_{10} P_{90} $S2_{max}$

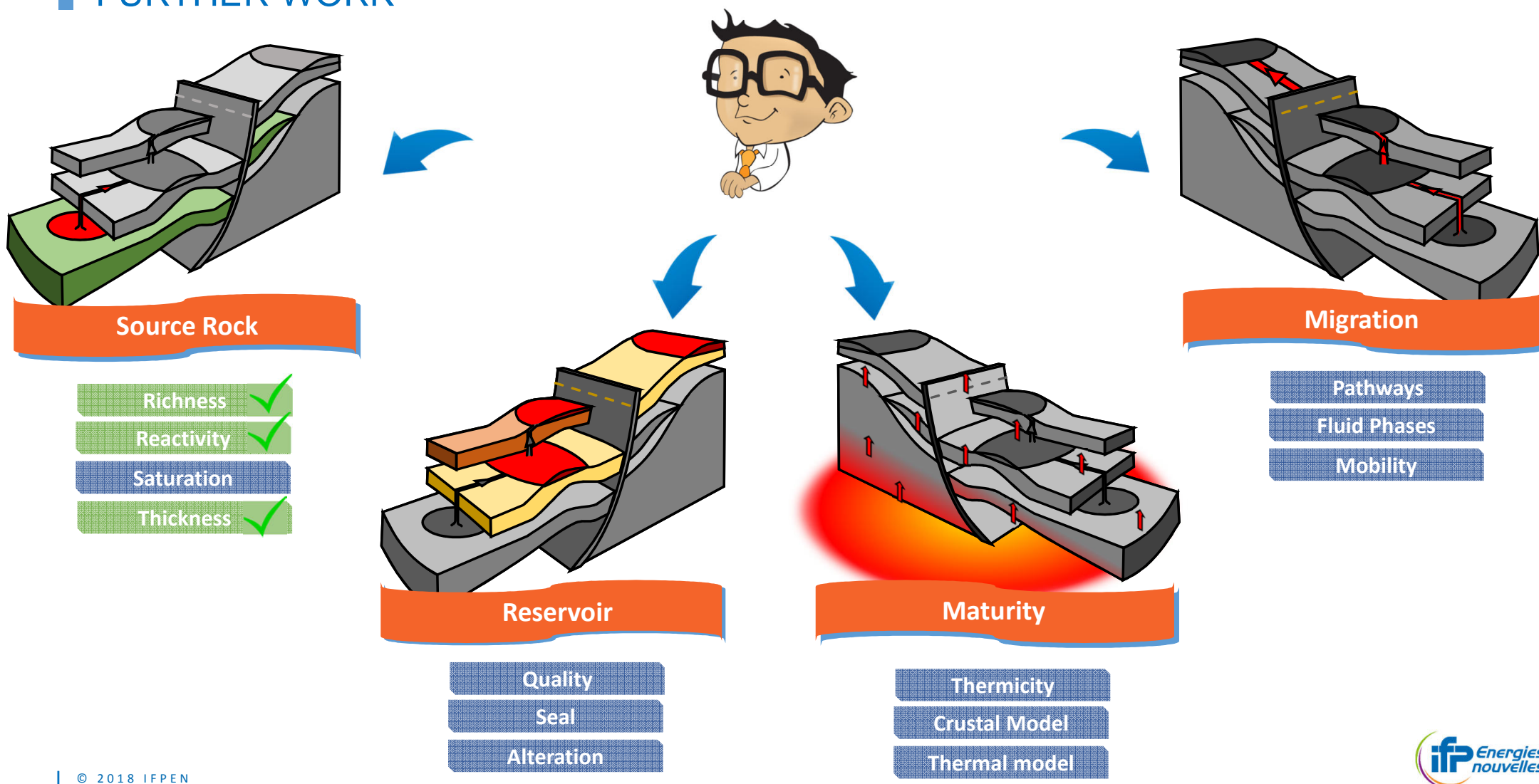
T_{min} P_{10} P_{90} T_{max}

H_{min} P_{10} P_{90} H_{max}

CAS X



FURTHER WORK



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