Fast and Economic Gas Isotherm Measurements Using Small Shale Samples*

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Abstract

Automated field desorption experiments and laboratory adsorption isotherms, performed with various gases and shale samples, are used to compare and validate the total gas content of the shale, to define the free and adsorbed gas proportions, to verify the USBM lost gas calculation, sample crushing size and sample preparation and handling techniques. Normal and abnormal desorption curves are examined. Full diameter and sidewall desorption data is compared.

High pressure mercury injection - pore size distribution experiments are performed on solid and crushed small shale samples to illustrate the reservoir quality and the crushed rock analysis concept. The diffusion parameter ratio (plug to crushed sample) is used to describe the shale pore network interconnectivity. Crushed and powdered adsorption isotherms are generated and used to show the crushing size importance in determining the total gas content. Over crushing the shale can seriously overestimate the adsorption isotherms by generating new surface while destroying pore volume.

Shale evaluation procedures consist of automated desorption isotherms, microfracture evaluation, tight rock analysis, diffusion parameter measurements, geochemical (TOC and Rock Evaluation, Ro), sorption isotherms, x-ray diffraction, SEM, capillary suction time for fluid optimization, mercury injection capillary pressure and pore size distribution, acoustic velocity measurements and dynamic rock mechanics are all performed on a small plug sample in a timely and economic manner.

Acknowledgments

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References

Faraj, B., A. Hatch, D. Krivak, and P. Smolarchuk, 2004, Mechanism of hydrogen generation in coalbed methane desorption canisters: Causes and remedies: GasTips, v. 10/2, p. 15-19.

Kissell, F.N., C.M. McCulloch, and C.H. Elder, 1973, The direct method of determining methane content of coalbeds for ventilation design: U.S. Bureau of Mines Report of Investigations 7767, 17 p. (Hartshorne coal, p. 7-9, 12, 15)

Lu, X.-C., F.-C. Li, and A. Watson, 1995, Adsorption measurements in Devonian shale: Fuel, v. 74, p. 599-603. DOI: 10.1016/0016-2361(95)98364-K.

Lu, X-C., F-C. Li, and A.T. Watson, 1995, Adsorption studies of natural gas storage in Devonian shales: SPE Formation Evaluation, v. 10/2, p. 109-113.

Luffel, D. L. and F. K. Guidry, 1992, New core analysis methods for measuring reservoir rock properties of Devonian shale: paper SPE-20571, Journal of Petroleum Technology, v. 44, p. 1184-1190. DOI: 10.2118/20571-PA.

Luffel, D. L., F. K. Guidry, and J. B. Curtis, 1992, Evaluation of Devonian Shale with new core and log analysis methods: Paper SPE-21297, Journal of Petroleum Technology, v. 44, p. 1192-1197. DOI: 10.2118/21297-PA

Mango, F.D., and L.W. Elrod, 1999, The carbon isotopic composition of catalytic gas: A comparative analysis with natural gas: Geochimica et Cosmochimica Acta, v. 63/7-8, p. 1097-1106.

McLennon, J.D., P.S. Schafer, and T.J. Pratt, editors, 1995, A Guide to Determining Coalbed Gas Content, v. I: Topical Report No. GRI-94/0396, Gas Research Institute (GRI), irregularly paginated.

Reed, R.M., R.G. Loucks, D.M. Jarvie, and S.C. Ruppel, 2008, Morphology, genesis, and distribution of distribution and genesis of nanometer-scale pores in siliceous mudstones of the Mississippian Barnett Shale: Journal of Sedimentary Research, v. 79, p. 848-861.

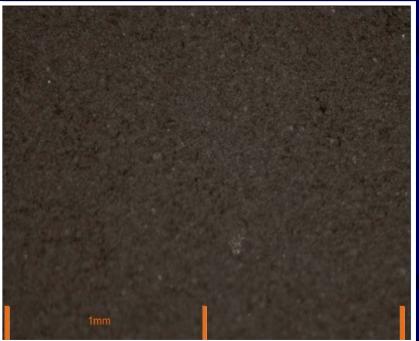
Saulsberry, J.L. P.S. Schafer, and R.A. Schraufnagel, editors, 1996, A Guide to Coalbed Methane Reservoir Engineering, v. II: Topical Report No. GRI-94/0397, Gas Research Institute (GRI), irregularly paginated.

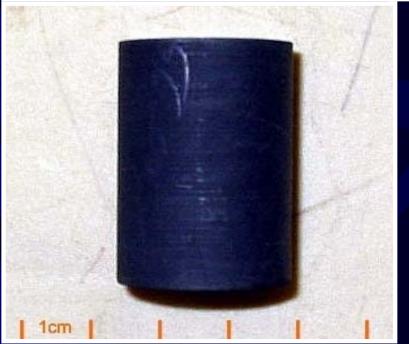
Waechter, N.B., G.L. Hampton III, and J.C. Shipps, 2004, Overview of coal and shale gas measurements: Field and laboratory procedures: International Coalbed Methane Symposium University of Alabama, Tuscaloosa, Alabama, May 2004, Web accessed November 16, 2010,

http://pttc.mines.edu/CBM/overview/overview.pdf

Zielinski, J.M., P. McKeon, and M.F. Kimak, 2007, A simple technique for the measurement of H₂ sorption capacities: Industrial Engineering and Chemical Research, v. 46/1, p. 329-335.







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Shale is Source, Seal and Lately ... Reservoir Rock

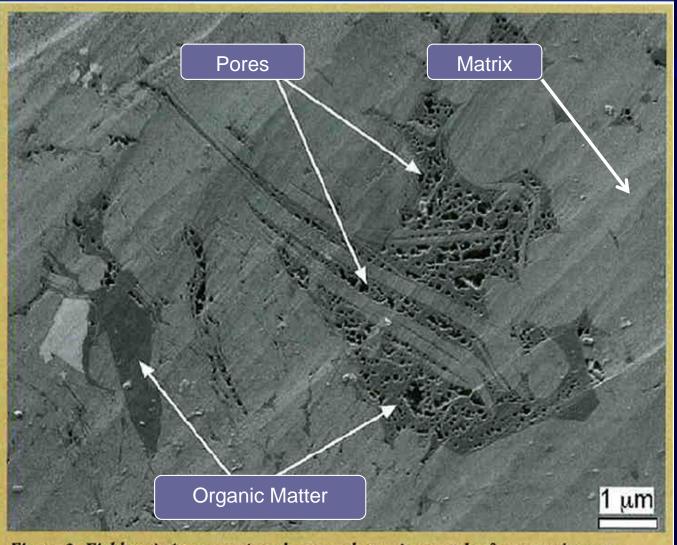


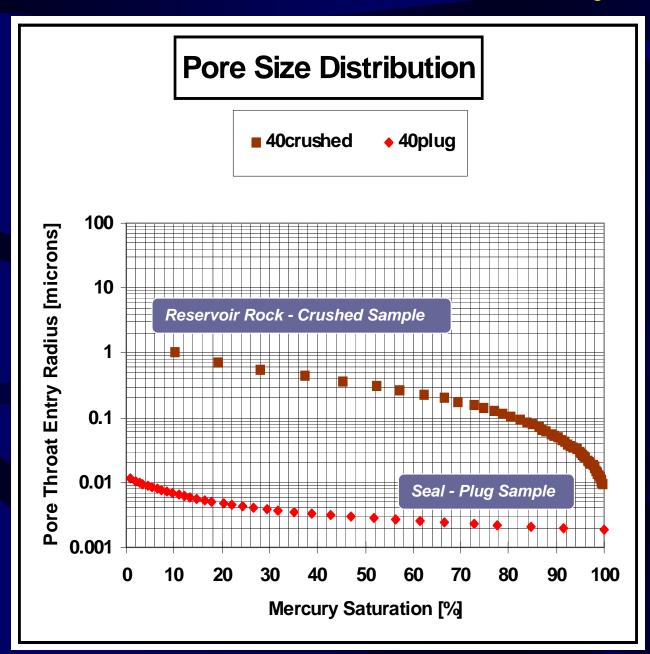
Figure 3. Field emission scanning electron photomicrograph of nanoscale pore architecture in the Barnett Formation. Image provided by R. Reed.

"More mature samples show well-developed nanopores concentrated in micron-scale carbonaceous grains. Large numbers of subelliptical to rectangular nanopores are present, and porosities within individual grains of as much as 20% have been observed. Shallowly buried, lower thermal maturity samples, in contrast, show few or no pores within carbonaceous grains.

These observations are consistent with decomposition of organic matter during hydrocarbon maturation being responsible for the intragranular nanopores found in carbonaceous grains of higher maturity samples. As organic matter (kerogen) is converted hydrocarbons, nanopores created to contain the liquids and With continued thermal gases. maturation, pores grow and may form into networks. The specific thermal maturity level at which nanopore development begins has not been However, determined. current observations support nanopore formation being tied to the onset of conversion of kerogen to hydrocarbons."

Picture and text from Robert M. Reed, Bureau of Economic Geology | John A. and Katherine G. Jackson School of Geosciences, The University of Texas at Austin, Austin, TX | Robert G. Loucks, Bureau of Economic Geology, The University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel, Bureau of Economic Geology, University of Texas at Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel | Bureau of Economic Geology, University of Texas at Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Stephen C. Ruppel | Bureau of Economic Geology, University of Texas at Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Bureau of Economic Geology, University of Texas at Austin, Austin, TX | Daniel Jarvie, Worldwide Geochemistry, Humble, TX | Bureau of Economic Geology, University of Texas at Austin, A

Shale as a Seal and as a Reservoir Rock The Crushed Rock Analysis Concept



A sidewall sample was divided in 2 parts. One part was crushed to approx 45 mesh. High pressure mercury injection test (60,000 psia) was performed on each part (plug and crushed). The plug sample pore size distribution looks like a "seal" while the crushed sample looks more like a "reservoir rock".

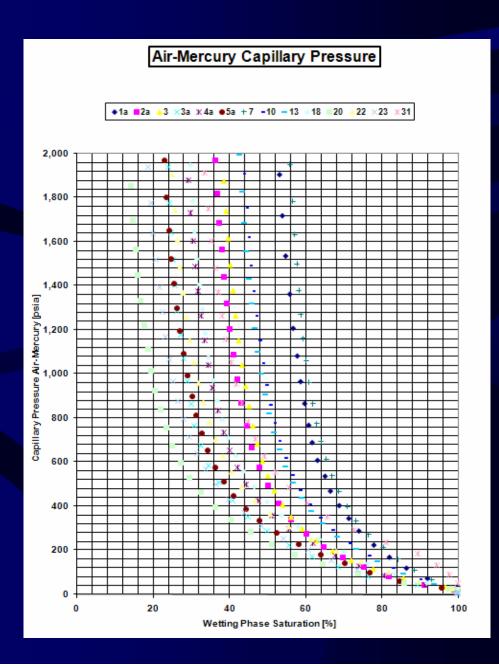
The pore sizes measured on the crushed sample are similar to the ones showed in the SEM picture.

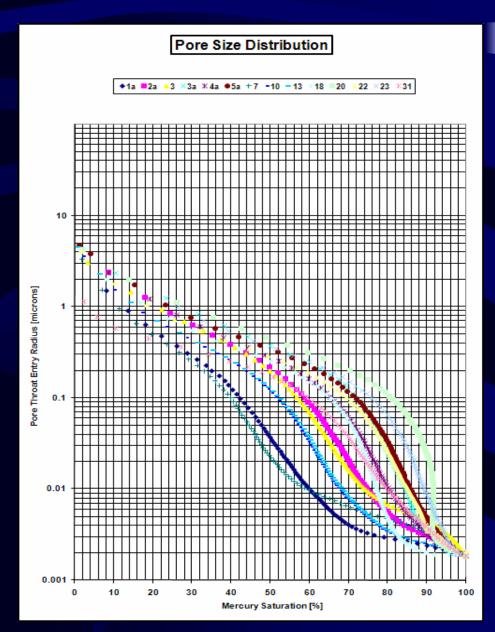
The kerogen to hydrocarbon conversion pores form a local network (LAN). However these pores are not very well connected in a wide area network (WAN).

These pores observed in the crushed sample are large enough for a mD range permeability. However, the measured shale matrix permeability is often nano to micro Darcy range, therefore the connectivity is limited at best.

The pore network connectivity can be described using the Diffusion Parameter Ratio for the plug and crushed sample.

Capillary Pressure and Pore Size Distribution Crushed Barnett Shale





The shale gas reservoir has two components:

Free Gas (Conventional) – is the gas stored by compression and solution in the larger pores.

Adsorbed Gas (Unconventional) – is the gas stored by molecular attraction to the surface of the organic material present in the shale.

The surface area of the organic shale is very large and known to attract natural gas.

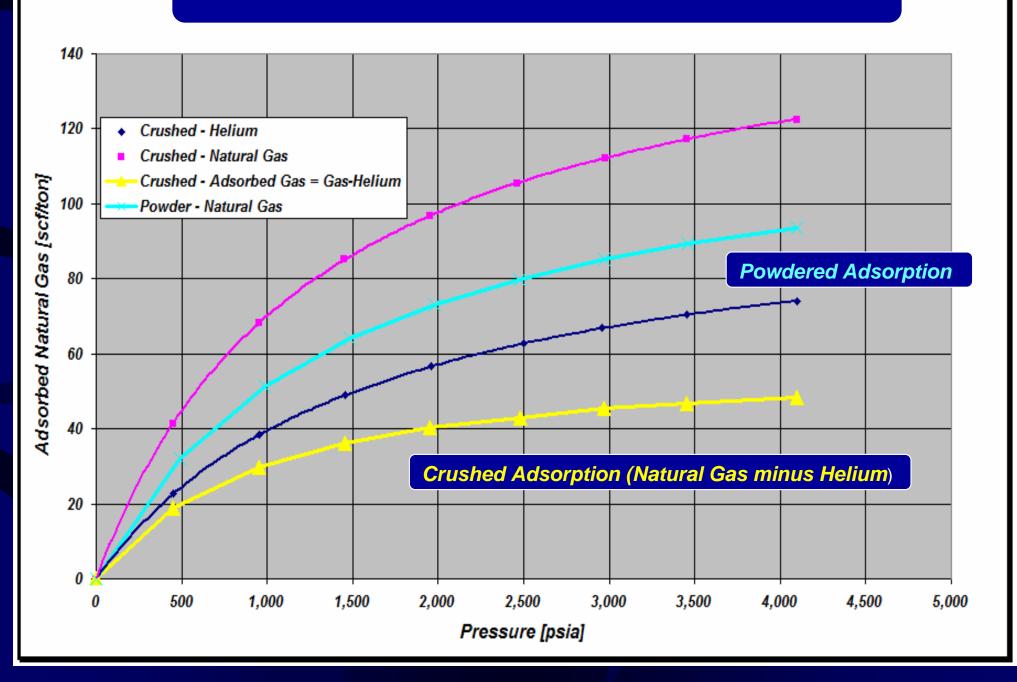
Capillary Condensation can occurs in micro pores due to the molecular vapor-solid attraction in a multilayer adsorption environment. The interesting aspect of capillary condensation is that this vapor condensation occurs well below the saturation vapor pressure. Abnormally high gas condensate densities are observed at low pressures due to strong molecular attraction (much like a compressed liquefied gas). This can explain relatively large gas reserves found in some shale reservoirs.

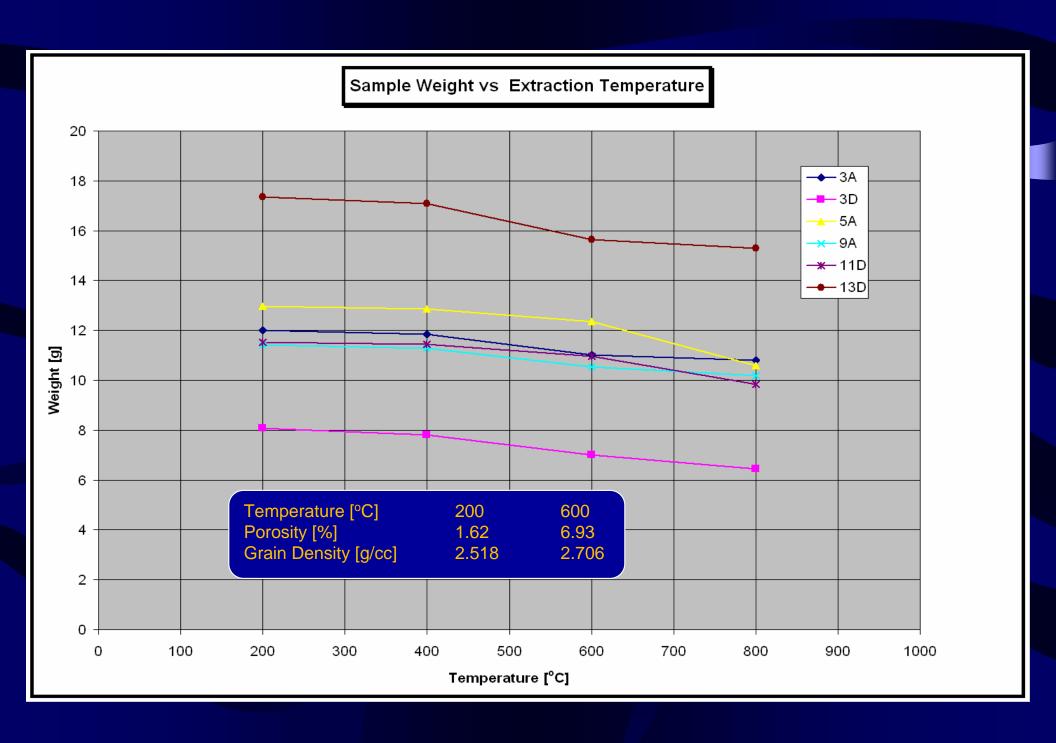
Shale Analysis Problems

- 1.Sample Crushing and/or Grinding. Provides measuring access to the local pore systems, however the adsorption surface area is increased and exposed to oxygen.
- 2.Baking the Kerogen and Liquid Hydrocarbons. The higher the extraction temperature in the laboratory the higher the measured total porosity.
- 3.Large lost gas calculations when the sample retrieval time is long (conventional cores).
- 4. Unusual measured gas curves showing gas generation (bacterial, capillary evaporation in dual pore size, catalytic generation ...)

A good correlation of the desorption and adsorption isotherms can address these problems

Crushed and Powdered Shale Adsorption





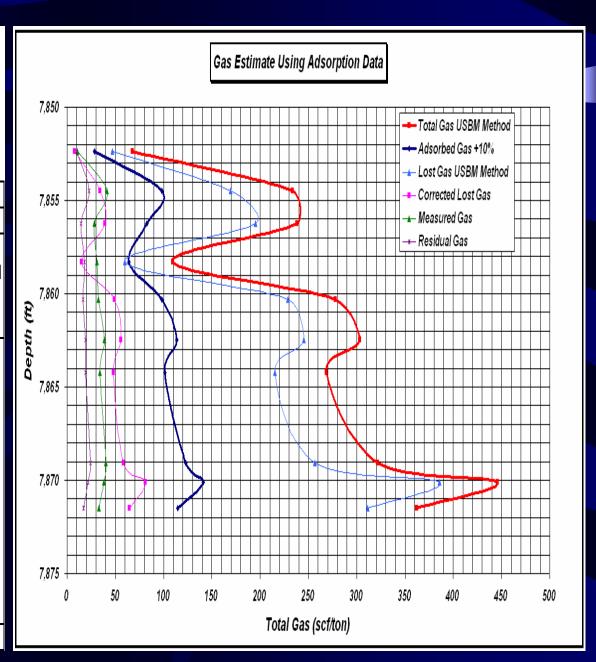
Gas Estimate Using Adsorption Data Conventional Core with Long USBM Time

Quick-Desorption™ and Shale Evaluation

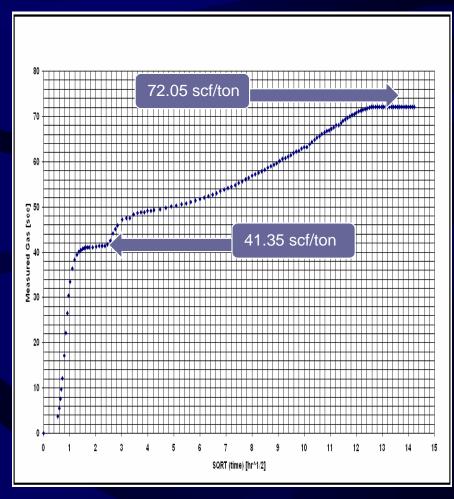
Company: SCAL, Inc. Desorption Temperature: 200 °F

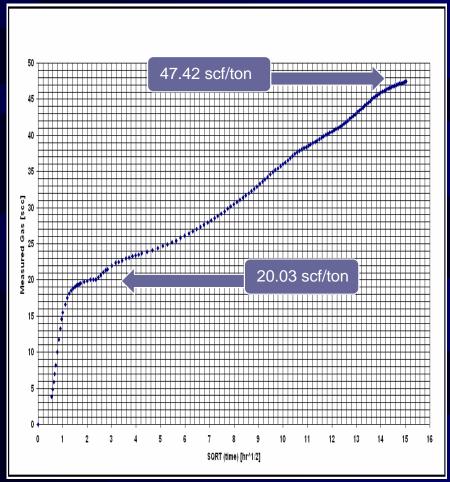
County: Midland County, Texas

Sam	ple		Quick-De	esorption	Adsorption Data					
				A	As receive	d				
No.	Depth ft	Measured Gas scf/ton*	Lost Gas scf/ton*	Residual Gas scf/ton*	TOTAL Gas scf/ton*	ADS Gas scf/ton*	ADS Gas + 10% scf/ton*	Corrected Lost Gas scf/ton*		
1	7 050 25	10.8	47.1	9.8	67.7	25.6	28,2	7.5		
2	7,852.35 7,854.50	41.1	169.5	9.0 22.7	233.3	89.2	98.1	34.2		
3	7,856.25	28.6	195.0	14.6	238.2	75.1	82.7	39.5		
4	7,858.30	31.1	60.2	18.2	109.5	58.3	64.1	14.8		
5	7,860.30	32.6	228.8	16.7	278.1	89.3	98.2	48.9		
6	7,862.45	38.7	245.3	18.9	303.0	103.4	113.7	56.0		
7	7,864.25	33.9	215.6	19.3	268.8	92.0	101.2	48.0		
8	7,869.05	40.3	256.9	24.4	321.6	111.9	123.1	58.3		
9	7,870.10	38.2	385.6	21.8	445.6	128.1	140.9	81.0		
10	7,871.50	33.3	311.6	16.9	361.8	104.3	114.8	64.5		
Average	1	32.9	211.6	18.3	262.8	87.7	96.5	45.3		



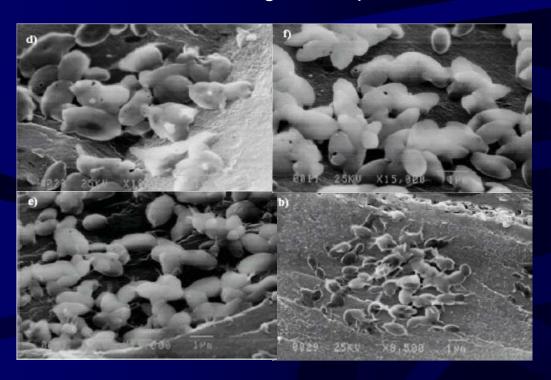
Unusual Measured Gas Curves Gas Generation (catalytic, bacterial, capillary evaporation in dual pore size distribution) Reservoir Pressure 3,900 psia, Temperature 200 °F





A fast desorption also prevents the errors associated with hydrogen generation by anaerobic bacterial growth.

Bacterial hydrogen generation starts several days into the test. The bacterial hydrogen can be a significant portion of the total gas (up to 82 mole %).

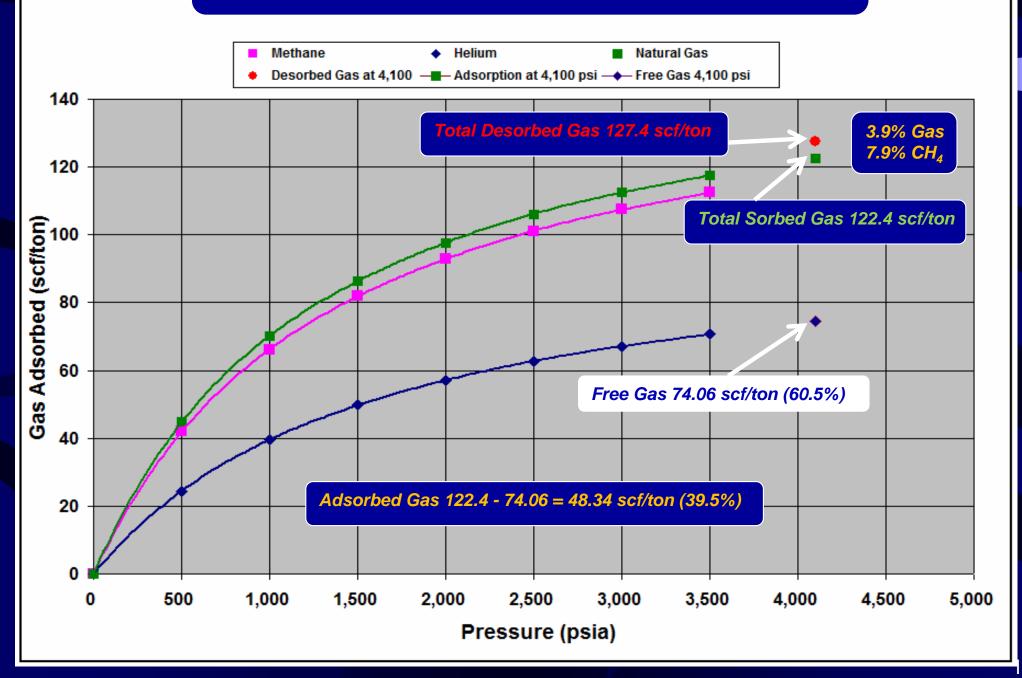


"The time range for the first occurrence of H₂ identified in this study is the variable and found to occur at any time between 5 days and 100 days from the start of the desorption experiments. Trace amounts of H₂ may have been generated earlier than 5 days. However, no GC analysis was performed for periods less than 5 days, making this impossible to confirm."

Sample No	Total Desorbed H ₂ Volume (cm ₃)	Total Desorbed CH ₄ Volume 8(cm³)	Experiment Duration	Mole% of H ₂ to Total Gas Desorbed	Corrected Gas Content (Scf/ton)	Air-dry Sample Weight (gm)
1	2,079.8	2,753.8	71.0	43%	47.4	1,861
2	4,430.4	950.4	70.6	82%	14.2	2,145
3	1,041.9	1,373.1	242.5	43%	50.3	
4	14.8	7,885.2	172.9	0.2%	1,153.0	
5	1,789.4	5,553.6	254.2	24%	116.2	
6	1,887.2	2,635.9	71.1	42%	50.5	1,670
7	117.6	5,337.1	172.7	2.2%	79.6	2,145
8	165.7	542.3	245.3	23.4%	12.7	
9	1,537.5	2,816.5	250.1	35.3%	91.1	
10	1,280.6	2,563.4	337.9	33.3%	64.9	1,264.3
11	0.01	2,799.0	337.9	0.01%	61.0	1,468.1
12	963.9	5,733.1	337.3	14.4%	88.8	2,067.2
13	464.2	864.8	236.6	35%	36.5	1,165.8
14	1,713.8	1,949.2	236.4	47%	36.9	1,689.3
15	142.1	6,240.4	260.5	1.9%	92.9	
16	7.9	9,089.2	260.4	0.1%	132.5	
17	55.2	3,000.5	258.4	1.8%	54.3	1,768
18	692.8	2,832.0	253.5	19.7%	42.7	2,121
19	141.9	3,945.1	272.7	3.5%	82.0	
20	1,030.4	2,285.6	272.1	31.1%	67.9	



Desorption-Adsorption Correlation Reservoir Pressure 4,100 psia, Temperature 175 °F



Shale Gas Reserves

1. Calculate Total Gas (not a function of porosity):

 $G = 1359.7 A h \rho_c G_c$

G = Gas-in-Place, scf

A =Reservoir Area, acres

h = Thickness, feet

 ρ_c = Average In-Situ Shale Density, g/cm³

 G_C = Average In-Situ Gas Content, scf/ton

- 2. Determine the free (conventional) gas. The total and free gas proportions are determined by measuring sorption isotherms with natural gas and helium on preserved sidewall samples.
- 3. Calculate the porosity responsible for holding the conventional gas (compressed and solution) and compare to the laboratory porosity. Adjust the laboratory procedures (extraction temperature) to match the calculated porosity for a given area.

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The Quick-Desorption[™] System





SCAL, Inc.

Quick-Desorption[™] Portable Laboratory



The equipment is installed in an SUV consists of 2 and accurate mechanical convection laboratory ovens (0.3 °C uniformity), stainless steel canisters and a very accurate measuring system operating gas isothermal at reservoir temperature. The measuring system includes an industrial computer interfaced with a laptop computer. The equipment is by digital powered invertergenerators and in-line digital UPS systems. A backup generator is also included in the system.

Desorption Canisters



The sidewall cores are cut top to bottom to minimize the lost gas. After retrieval the samples are sealed in canisters at the well site. We collect desorption data at reservoir temperature as we drive back to our laboratory facility where the testing is continued.



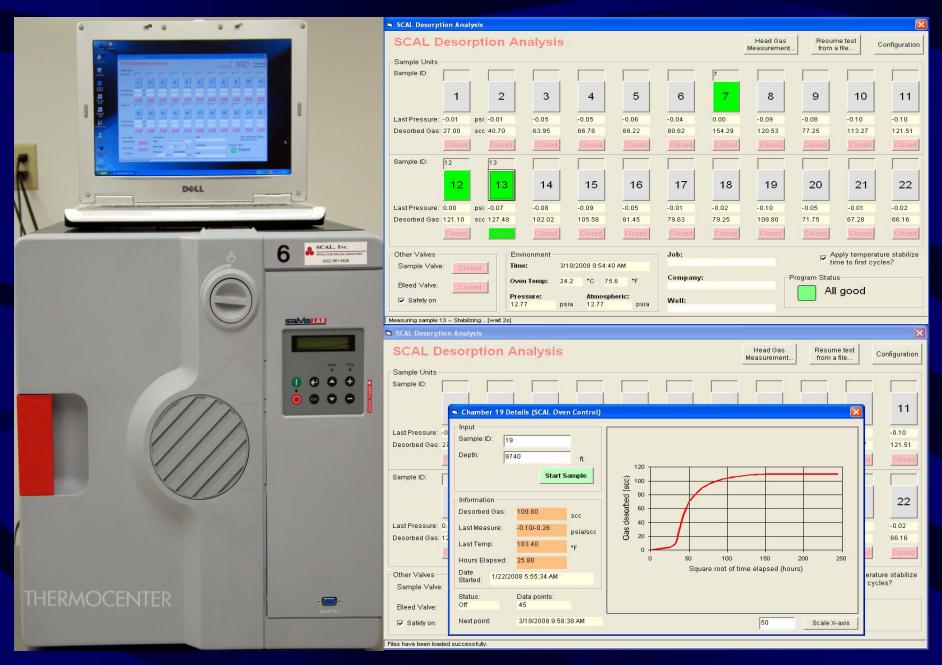
Full Diameter Quick-Desorption™



Using a portable diamond drill, 1 inch diameter plugs are drilled vertically into the center of the full diameter sample at the well site. These smaller samples are loaded into our standard desorption canister.

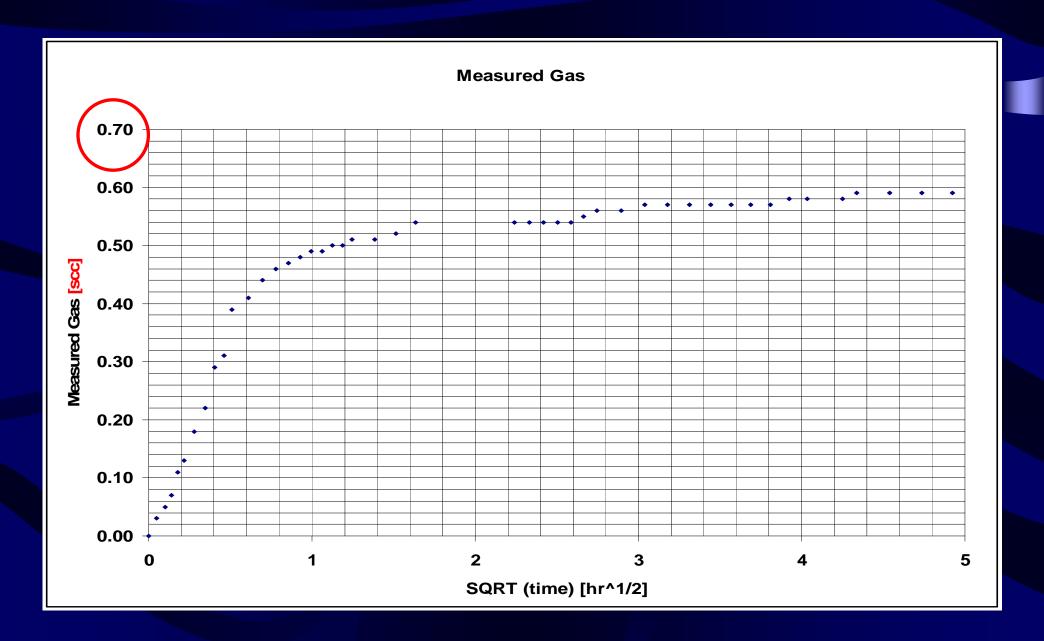


Quick-Desorption™ Equipment and Software





Quick-Desorption[™] Resolution



Quick-Desorption™ Test

 Company:
 SCAL, Inc.
 Sample:
 1

 Well Name:
 Test #1
 Depth:
 9,500.0 ft

File No.: 8000

Standard pressure: 14.7 psia Fluid: drilling mud

Standard temperature: 60 °F

Date 1/22/2008

14

15

16

17

18

19

20

21

22

23

24

25

26

27

28

29

30

1.81

1.86

1.92

1.97

2.02

2.07

2.12

2.16

2.28

2.38

2.49

2.59

2.68

2.77

2.86

2.93

3.02

93.27

97.33

100.64

103.40

105.63

107.40

108.69

110.02

112.88

114.96

116.00

117.09

117.72

118.70

119.26

119.56 119.93

Start tripping out:3:08Trip time :2:02 hr:minAt surface :5:10At the surface :0:37 hr:minIn the canister :5:47USBM time :1:38 hr:min

 Measured Gas (M)
 2.40 scc/g
 76.7 scf/ton*

 Lost Gas (L)
 8.70 scc/g
 278.7 scf/ton*

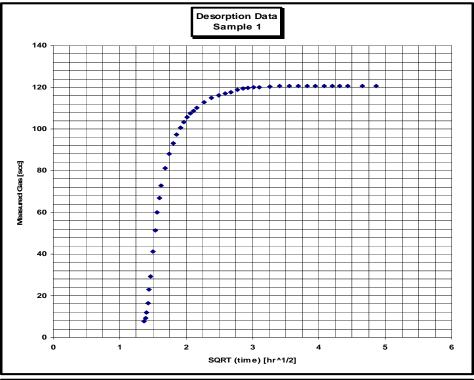
 Residual Gas (R)
 0.89 scc/g
 28.6 scf/ton*

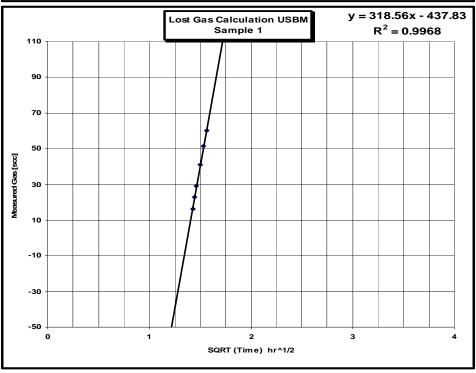
Total Gas Content (M-1 11.99 scc/g 384.1 scf/ton*

Measured Gas 120.53 scc Weight: 50.322 g Lost Gas Intercept 437.83 scc Desorption temperature: 180 °F

No. SQRT(TotalTime) Gas Regression Data for Lost Gas Calculation USBM: hr^1/2 scc

1	1.37	7.64		
2	1.39	9.16		
3	1.41	12.01		
4	1.43	16.38	1.43	16.38
5	1.45	22.94	1.45	22.94
6	1.46	29.26	1.46	29.26
7	1.50	41.15	1.50	41.15
8	1.53	51.46	1.53	51.46
9	1.57	59.98	1.57	59.98
10	1.60	66.98		
11	1.63	72.71		
12	1.69	81.24		
13	1.75	87.94		





Micro fracture Porosity and Permeability

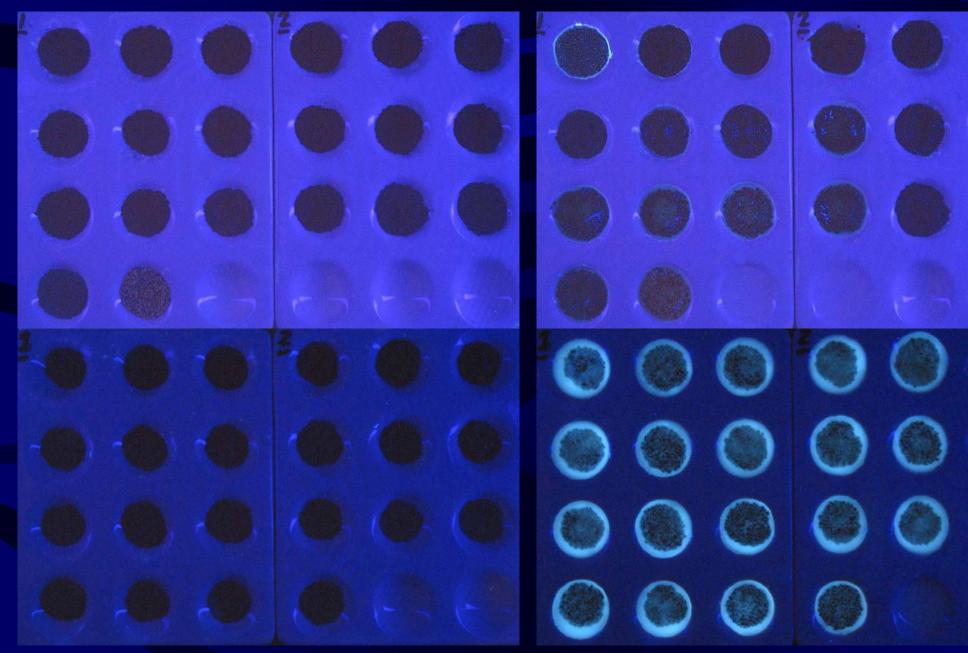
The plug or sidewall porosity and permeability are measured at confining stress "as received" with the reservoir fluids intact. An automated porosimeter and permeameter expands helium into the gas filled microfractures of the sample. The micro fracture porosity and permeability are measured.



Crushed Rock Analysis and Diffusion Parameters

- Properties measured before extraction (as received):
 - » Matrix Permeability
 - » Gas-Filled Porosity
 - » Shale Density
 - » TOC and Rock Evaluation
- Properties measured after Dean-Stark extraction:
 - » Oil and Water Saturations
 - » Total Porosity
 - » Grain Density
- The diffusion parameter is determined from the slope of the desorption curve for the plug sample and also for the crushed sample. The diffusion parameter ratio is an indication of pore network interconnectivity.
 - » D/r² = Diffusion Parameter [1/sec]
 - » D = Diffusion Coefficient [cm²/sec]
 - » r = Sphere Radius [cm]

Fluorescence



Before the addition of a cutting solvent

After the addition of a cutting solvent, with empty wells for comparison

Quick-Desorption[™] and Shale Evaluation

Quick-Desorption™ and Shale Evaluation

Company: SCAL, Inc. County: Midland Desorption Temperature: 200 °F

Well: Test 1 State: Texas Confining Pressure: 1,500 psi

Sample			Quick	-Desorptio	on		Plug (m	nicrofracti	ure) Data	Crushed Sa	ample Data	Dea	n-Stark	Data	Diffusi	on Parame	neter			
36	ampie				A	s receiv	ed				Extr	Extracted and dried				As received				
															Plug	Crushed				
No.	Depth	Measured	Lost	Residual	TOTAL	Matrix	Plug	Plug	Bulk	Gas Filled	Total	Satur	ations	Grain	D/r ²	D/r ²	Ratio			
		Gas	Gas	Gas	Gas	Perm	Perm	Porosity	Density	Porosity	Porosity	Water	Oil	Density						
	ft	scf/ton*	scf/ton*	scf/ton*	scf/ton*	nD	mD	%	g/cc	%	%	%	%	g/cc	1/sec	1/sec				
1	9,210.0	29.1	23.7	22.4	75.1	604.4	0.0901	0.28	2.655	2.20	3.78	32.1	0.8	2.605		3.17E-04				
2	9,270.0	60.4	47.3	50.9	158.6	1363.0	tbfa	2.84	2.590	3.60	4.92	31.0	1.3	2.470	1.87E-05					
3	9,304.0	29.6	22.2	16.6	68.4	584.6	0.0234	0.55	2.538	1.09	4.10	35.2	1.2	2.532	1.74E-05					
4	9,415.0	39.3	27.4	31.8	98.6	793.7	0.0234	1.43	2.495	1.88	4.48	29.6	1.1	2.571	1.39E-05					
5	9,445.0	34.0	26.8	25.7	86.5	990.5	0.0310	0.33	2.547	1.67	4.10	33.8	1.5	2.627	1.77E-05	2.27E-04	0.08			
6	9,456.0	34.9	31.9	39.1	105.9	842.5	0.0233	2.19	2.649	2.92	3.47	33.4	1.8	2.648	2.28E-05	2.32E-04	0.10			
7	9,510.0	47.4	28.0	50.2	125.6	1129.8	0.0251	1.58	2.474	2.41	5.72	26.6	1.4	2.512	9.55E-06	2.11E-04	0.05			
8	9,539.0	124.8	63.0	79.5	267.2	386.6	tbfa	2.64	2.791	2.93	5.09	25.8	1.3	2.318	6.66E-06	1.97E-04	0.03			
9	9,550.0	30.4	19.0	19.6	68.9	262.4	0.0002	0.29	2.544	1.91	5.68	35.9	1.0	2.632	1.02E-05	2.08E-04	0.05			
10	9,562.0	37.8	24.4	16.7	78.8	483.8	0.0002	1.03	2.497	2.32	4.66	30.0	1.6	2.632	1.02E-05	2.17E-04	0.05			
11	9,580.0	40.9	28.3	30.9	100.0	506.2	0.0541	0.51	2.540	1.62	4.55	27.6	1.4	2.618	1.19E-05	1.46E-04	0.08			
12	9,599.0	38.7	23.0	27.8	89.5	617.3	0.0002	0.82	2.598	1.51	3.03	32.1	1.5	2.613	8.16E-06	1.45E-04	0.06			
13	9,613.0	26.2	17.7	12.3	56.1	831.6	0.0002	1.64	2.576	3.49	5.36	29.7	0.7	2.646	1.04E-05	2.48E-04	0.04			
14	9,643.0	32.8	23.1	13.3	69.2	159.9	0.0002	0.44	2.532	2.02	4.43	29.9	0.8	2.643	1.15E-05	1.23E-04	0.09			
15	9,666.0	34.0	21.2	30.0	85.2	523.1	0.0004	0.01	2.550	1.60	3.53	36.5	0.6	2.615	6.91E-05	1.55E-04	0.45			
16	9,692.0	31.8	21.6	16.7	70.1	331.4	0.0003	0.01	2.500	1.05	4.45	31.5	0.9	2.638	1.02E-05	1.52E-04	0.07			
17	9,718.0	29.2	24.6	15.6	69.4	418.7	0.0307	0.30	2.572	1.81	5.31	30.0	0.9	2.666	1.55E-05	1.22E-04	0.13			
18	9,732.0	32.8	23.5	16.7	73.0	653.7	0.0001	0.58	2.595	1.31	3.97	31.8	1.0	2.640	1.10E-05	1.52E-04	0.07			
19	9,740.0	30.3	22.1	15.9	68.3	282.5	0.0001	0.20	2.507	2.76	3.81	30.2	1.2	2.671	1.12E-05	1.00E-04	0.11			
20	9,752.0	20.4	17.8	13.0	51.2	301.0	0.0013	0.17	2.744	2.00	1.63	27.3	8.0	2.772	1.57E-05	1.05E-04	0.15			
21	9,766.0	33.5	26.6	19.9	79.9	674.0	0.0006	0.32	2.607	1.81	4.19	24.1	1.1	2.714	1.29E-05	1.39E-04	0.09			
22	9,778.0	31.8	26.4	13.9	72.1	391.7	0.0006	0.11	2.524	1.74	3.67	26.0	1.3	2.655	1.38E-05	1.80E-04	0.08			
A۷	erage	38.6	26.8	26.3	91.7	596.9	0.0153	0.83	2.574	2.08	4.27	30.5	1.1	2.611	1.59E-05	1.77E-04	0.10			

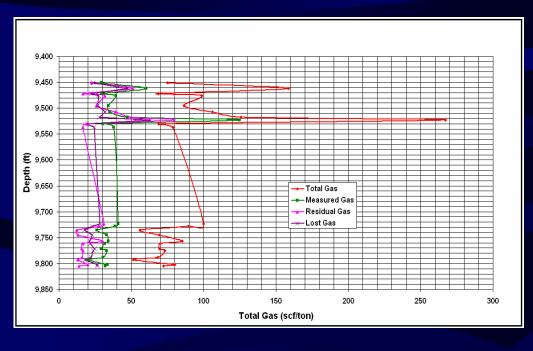
Notations: D Diffusion coefficient [cm²/sec]

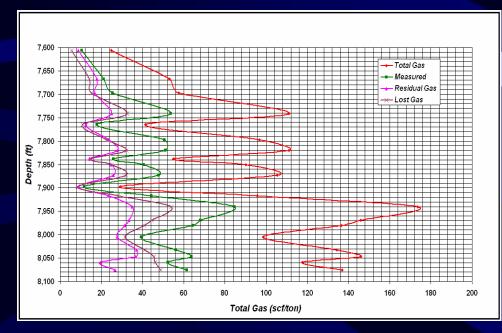
r Sphere Radius [cm]
D/r² Diffusion parameter [1/sec]

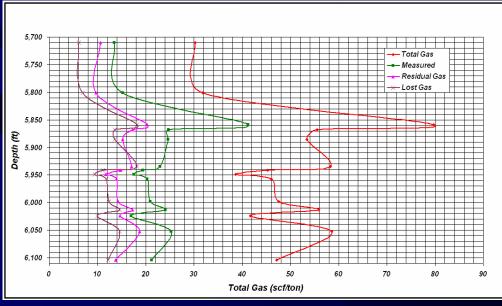
ton* US Short ton equal to 2,000 lbs

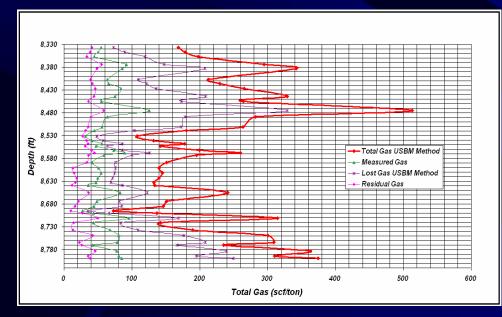


Quick-Desorption[™] Gas Composite Plots









Shale Evaluation using Desorption Isotherms

- 1 Measured gas. A fully automated laboratory is present on location when the rotary sidewall samples are taken. The cores are cut from top to bottom and retrieved from the coring tool ASAP to minimize the lost gas. The wire line trip out time is recorded and used in the USBM lost gas calculation. Vertical plug samples can be cut, in the center of a conventional core, at the well site and used for Quick-Desorption and Shale Evaluation. The portable laboratory returns to our laboratory facility while collecting desorption data at constant reservoir temperature. The desorption is conducted until the gas production ends.
- 2 Lost gas and matrix permeability. The linear portion of the desorption curve is used to determine lost gas and the diffusion parameter for the plug samples.
- 3 Bulk density, micro fracture porosity and permeability at confining stress. Bulk density and micro fracture permeability and porosity measurements are performed at reservoir confining stress on the wet shale sample (if a straight cylinder can be shaped from the recovered core material). If the sample quality is poor, only the bulk density is measured.
- 4 Residual gas. The shale is grinded to about 45 mesh using special mills. Another desorption is performed at reservoir temperature on the granular sample to measure the residual gas and the diffusion parameter.
- 5 Total gas. Total gas is calculated by adding measured, lost and residual gas.
- 6 Geochemistry. A small portion of the sample is collected to perform TOC and Rock-Evaluation. The plug end trims are also available for further geochemistry and/or petrography analysis (TS, XRD, SEM).
- 7 Gas filled porosity. The gas filled porosity is measured on the crushed sidewall sample by gas expansion into the "as received" shale.
- 8 Water and oil saturations, total porosity, and grain density. The samples are extracted to measure the water and oil saturations. The total porosity and the grain density are also measured.

Sorption Isotherms – Reservoir Performance

Sorption isotherms can be measured on sidewall samples using a new 8 cell design. Various gases can be used. The Langmuir gas storage for a particular pressure can be calculated:

$G_s=VL \times P/(P+PL)$

Where:

G_s = Gas storage capacity (scf/ton)

VL = The Langmuir Volume (scf/ton) is the maximum amount of gas that can be adsorbed at infinite pressure

P = Absolute pressure (psia)

PL = The Langmuir pressure (psia) affects the curvature of the isotherm and corresponds to the pressure at which half of the VL is adsorbed.

Sorption Isotherm Methane 191 °F

Company: Good Oil Company

Well Name : Well #1
County : This County
State : New Mexico

 Sample :
 1
 Porosity :
 0.4
 %

 Depth :
 12,000 ft
 Grain Density :
 2.541 g/cc

Confining Pressure: 3,600 psi

Temperature: 191 °F Sample Weight: 13.00 g

Atmospheric Pressure: 13.1 psi

Test Results:

Step	Pressure	Adsorption	Adsorption	Langmuir Gas Storage*
No.	psia	scc/g	scf/ton	scf/ton
4	540.7	0.0	04.4	00.0
1	512.7	0.6	21.4	20.8
2	1007.4	0.97	34.1	35.5
3	1503.1	1.3	46	46.8
4	2001.1	1.54	54.3	55.8
5	2493.4	1.81	64	63
6	2989.4	2.06	72.8	69.1
7	3475.2	2.14	75.5	74.1
8	3968.4	2.12	74.9	78.4

* Langmuir Regresion and Coefficients:

PL: 2,781.50 psia $Gs=VL \times P/(P+PL)$

VL: 133.33 scf/ton

Where:

Gs Gas storage capacity (scf/ton)

VL The Langmuir volume (scf/ton) is the maximum amount of gas that can be adsorbed

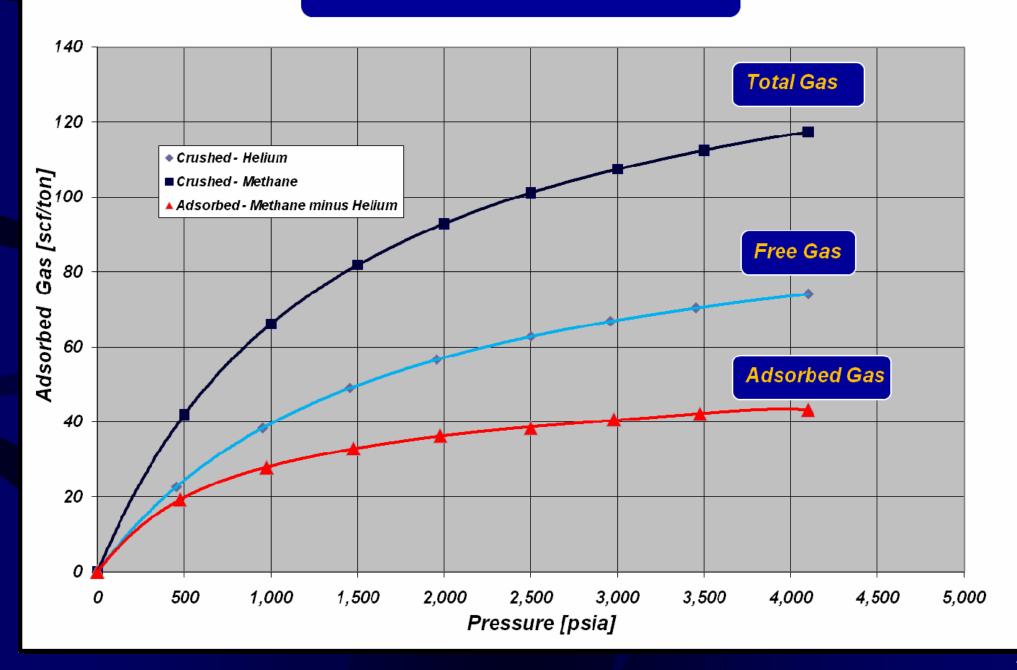
at infinite pressure.

P Absolute pressure (psia)

PL The Langmuir pressure (psia) affects the curvature of the isotherm and corresponds to the

pressure at which half of the LV is adsorbed.

Free and Adsorbed Gas



Shale Evaluation using Sorption Isotherms

Only one sidewall sample is required for this new test procedure.

- 1. Rotary sidewall samples are preserved at the well site and shipped to our laboratory in Midland, Texas; therefore there are not any field expenses associated with this procedure. The preservation consists of surface mud cleaned with a wet towel, then the samples are wrapped in saran wrap and aluminum foil. A few drops of water are added to each glass jar before the samples are sealed to prevent evaporation during transportation.
- 2. The samples are trimmed and photographed in UV and white light.
- 3. Micro fracture analysis. The as-received samples are loaded at reservoir stress and the porosity and permeability of the gas filled micro fractures are measured. The bulk density and matrix permeability are also measured.
- 4. Residual gas measurement. The sidewall samples are ground to an approximate 45 mesh. A complete desorption isotherm is performed at reservoir temperature to determine the residual gas and the diffusion parameter.
- 5. The gas filled porosity is measured by helium expansion into the as-received samples.
- 6. Sorption isotherms at reservoir temperature with methane are measured on each sample. These isotherms are normally close to the desorption isotherms (not measured in the field).
- 7. Cut fluorescence. A small fraction of the ground sample is photographed in UV without and with a cut solvent to document the cut fluorescence.
- 8. Geochemistry. A small portion of the sample is collected to perform TOC and Rock-Evaluation. The plug end trims are also available for further geochemistry and/or petrography analysis (TS, XRD, SEM).
- 9. Water and oil saturations, total porosity, and grain density. The samples are extracted to measure the water and oil saturations. The total porosity and the grain density are also measured.

Fluid Optimization: XRD and Capillary Suction Time

X-Ray Diffraction Mineral Data

Company: SCAL, Inc. Well: Test #1

Midland County, Texas Location :

Sample	Depth	Air	KK	Por	Grain	Qtz	Plag	K	Cal	Dol	Ank	Sid	Anhy	Gyp	NaCl	Pyr	Total	Illite	EML	Sme	Kao	Chl	Total
Number		Perm	Perm		Density			Feld									Bulk	+	i/s				Clay
	ft	mD	mD	%	g/cc												%	Mica					%
1	6073.5	0.01	0.01	3.12	2.50	50	6		1	2		1				4	64	20	6		3	7	36
2	6435.5	tbfa	tbfa	2.83	2.53	35	5	2	1	2		1				3	49	30	11		+	10	51
3	6,855.8	0.03	0.02	2.01	2.55	34	5			3						4	46	30	14			10	54
4	6,875.5	tbfa	tbfa	3.95	2.46	34	5			3		1				7	50	25	15			10	50
5	7,042.5	0.01	0.01	2.23	2.72	25	4			16						3	48	30	15			7	52
6	7,438.0	0.01	0.0056	3.48	2.64	22	4		9	14						5	54	30	16				46
7	7,462.0	0.01	0.0025	8.11	2.39	51	5		19	3		1				5	84	10	6				16
8	7491.5	0.01	0.0034	2.24	2.41	38	5		20	4						8	75	15	10				25
9	7,524.0	0.01	0.0072	4.47	2.23	18	2		78	2							100						О
10	7,550.0	О	0.0002	3.56	2.53	37	3		40	2						3	85	10	5				15
11	7,578.5	0.01	0.0044	2.81	2.56	39	3		8	2		1				8	61	25	14				39
12	7,623.0	0.01	0.0029	3.26	2.49	39	4		8	4		1				7	63	20	17				37
13	7,656.0	О	0.0019	1.8	2.43	42	4		4	2						11	63	20	17				37
14	7,694.0	0.4	0.3253	3.32	2.46	46	5		2	3						7	63	20	17				37

Anhy

Qtz Cal Sid Pyr Gyp Ank

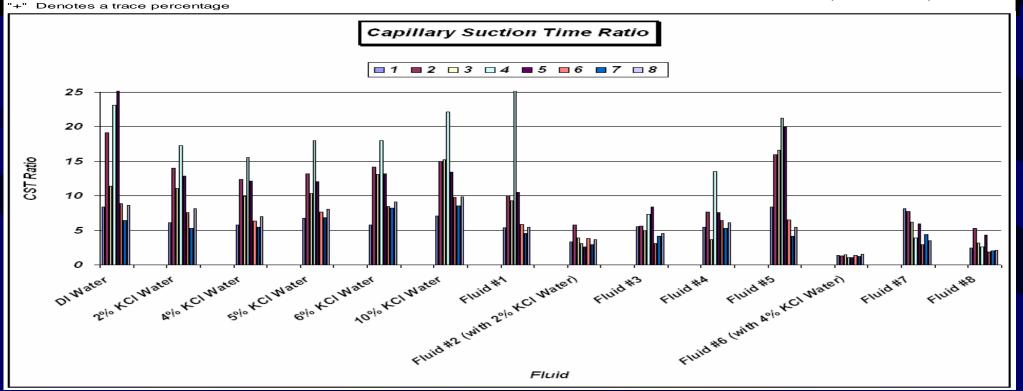
Quartz SiO2 Calcite Ca CO3 Siderite Fe CO3 Pyrite Fe S2 Gypsum CaSO4.2H2O Ankerite

KFeld Potassium Feldspar KAISi3O8 Clay Minerals = Aluminosilicates Dolomite CaMg(CO3)2 Dol Barite BaSO4 Bar Plag (Ca, Na)AI(1-2)Si(3-2)O8

Anhydrite CaSO4

Kaolinite Kao Chl Chlorite Sme Smectite

Expandable Mixed Layer (Illite/Smectite)



Dynamic Rock Mechanics

Brine Density:

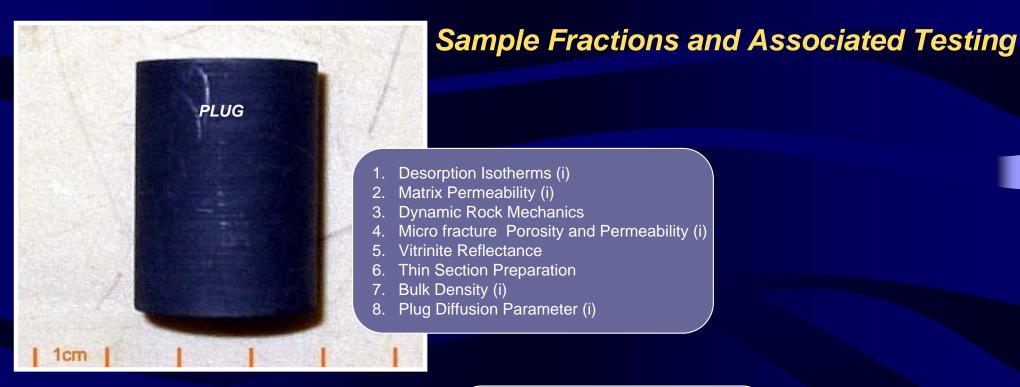
Acoustic Velocities Measurements

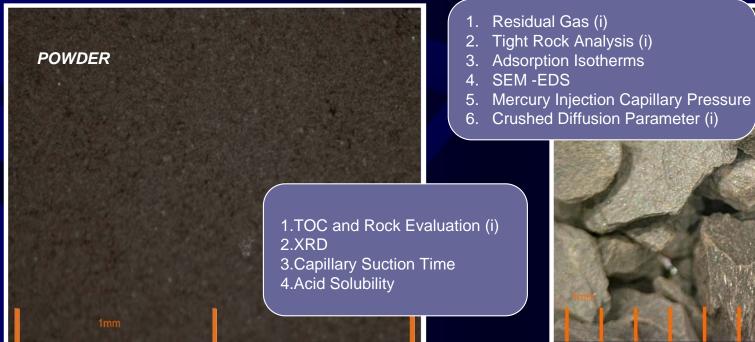
Company: Good Oil Company

Well Name: Good Well #2

1.03 g/cc 23 °C County: Some County, Oklahoma Temperature:

Sample	Depth	Porosity %	y Matrix Permeability nD		•		Confining Pressure F psi		Compresional Velocity ft/sec		Dynamic Bulk Moduli psi	Dynamic Shear Moduli psi	Young's psi	Poisson Ratio -
1	10,950.0	0.13	73.8	2.52	2.514	2.515	10,000	4,700	16,967	10,409	4,858,581	3,670,824	8,796,996	0.198
2	10,960.0	0.33	62.0	2.29	2.281	2.285	10,000	4,700	14,358	8,965	3,046,125	2,473,666	5,840,132	0.180
3	10,970.0	0.51	97.2	2.39	2.377	2.382	10,000	4,700	14,758	9,277	3,307,017	2,761,236	6,480,147	0.173
4	10,980.0	0.41	113.1	2.41	2.399	2.403	10,000	4,700	14,639	9,422	3,105,248	2,874,052	6,589,265	0.146
5	10,990.0	0.24	70.2	2.36	2.352	2.355	10,000	4,700	15,286	9,730	3,407,480	3,002,770	6,962,983	0.159
6	11,000.0	0.57	107.5	2.45	2.432	2.438	10,000	4,700	15,227	9,639	3,545,909	3,050,792	7,112,565	0.166
7	11,100.0	0.25	135.3	2.44	2.430	2.432	10,000	4,700	15,821	10,115	3,731,575	3,352,466	7,739,625	0.154





Conclusions:

- The desorption adsorption correlation is very important to assure accurate shale gas content. Is the best check available for the lost gas calculations, sample grinding size and saturation preservation. It can also validate a total gas measurement curve with gas generation (if the generated gas is bacterial the adsorption isotherm will be closer to the first plateau).
- The averaging technique currently used, where a number of sidewall samples from various depths are sealed inside the same desorption canister, can turn an excellent prospect into a mediocre one. Small canisters and high resolution equipment are necessary to measure the gas content of individual shale sidewall samples.
- The technology can accurately find the "sweet gas zone" before horizontal drilling begins.
- This technique is time and cost effective and provides major savings when compared with the cost of a full diameter core project.

References

- Faraj, Basim, and Anna Hatch. "Mechanism of Hydrogen Generation in Coalbed Methane Desorption Canisters: Causes and Remedies," GTI E&P Services. GasTIPS, (Spring 2004).
- Kissell, F.N., C.M. McCulloch, and C.H. Elder. "The Direct Method of Determining Methane Content of Coalbeds for Ventilation Design," U.S. Bureau of Mines Report of Investigations, RI 7767 (1973).
- Lu, Xiao-Chun, Fan-Chang Li, and A. Ted Watson. "Adsorption Measurements in Devonian Shales," Department of Chemical Engineering, 77843-3122. Fuel Vol. 74, No. 4 (1995).
- Lu, Xiao-Chun, Fan-Chang Li, and A. Ted Watson. "Adsorption Studies of Natural Gas Storage in Devonian Shales," SPE Formation Evaluation Texas A&M University. (June 1995).
- Luffel, D.L., F.K. Guidry, and J B. Curtis. "Evaluation of Devonian Shale with New Core and Log Analysis Methods," SPE Paper 21297, presented at SPE Eastern Regional Meeting, Columbus, Ohio (October 31-November 2, 1990).
- Luffel, D.L., and F.K. Guidry. "New Core Analysis Methods for Measuring Reservoir Rock Properties of Devonian Shale," SPE Paper 20571, presented at SPE Technical Conference and Exhibition, New Orleans, Louisiana (September 23-26, 1990).
- Mango, F.D., and L.W. Elrod, The carbon isotopic composition of catalytic gas: A comparative analysis with natural gas: Geochimica et Cosmochimica Acta, v. 63, p. 1097-1106 (1999).
- Mavor, Matthew J., George W. Paul, Jerrald L. Saulsberry, Richard A. Schraufnagel, Peter F. Steidl, D.P. Sparks, and Michael D. Zuber. "A Guide to Coalbed Methane Reservoir Engineering," Ed. Jerrald L. Saulsberry, Paul S. Schafer, and Richard A. Schraufnagel. Chicago: Gas Research Institute (1996).
- McLennon, John D., Paul S. Schafer, and Timothy J. Pratt. "A Guide to Determining Coalbed Gas Content," Gas Research Institute (1996).
- Reed, Robert M., Robert G. Loucks, Daniel M. Jarvie, and Stephen C. Ruppel, Morphology, genesis, and distribution of distribution and genesis of nanometer-scale pores in siliceous mudstones of the Mississippian Barnett Shale: Journal of Sedimentary Research, v. 79, p. 848-861 (2008).
- Waechter, Noel B., George L. Hampton III, and James C. Shipps. "Overview of Coal and Shale Gas Measurements: Field and Laboratory Procedures," 2004 International Coalbed Methane Symposium University of Alabama. Hampton, Waechter, and Associates, LLC., Tuscaloosa, Alabama (May 2004).
- Personal conversations with Dr. Dan Suciu consultant, Mr. Alton Brown consultant and Dr. Martin Thomas of Quantachrome Corporation.