## PS Suitability of the Dryland Fluvial-Aeolian Sediments and Its Depositional System for CO<sub>2</sub> Sequestration, Analogues Study from Umbum Creek, Lake Eyre, Central Australia\*

Saju Menacherry<sup>1</sup>, John Kaldi<sup>1</sup>, Simon Lang<sup>2</sup>, and Tobias Payenberg<sup>3</sup>

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#### **Abstract**

The efficiency of CO<sub>2</sub> geological storage is determined by the depositional system of the sedimentary basins, in which the storage reservoir qualities of subsurface reservoir rocks are primarily controlled by their composition, texture and grain size. The ability to quantifiably predict such porosity and permeability is a significant factor in storage reservoir quality forward modeling.

The degree of reaction, reaction rates and mineralogical storage of CO<sub>2</sub> are dependent on mineral assemblage, concentration of CO<sub>2</sub> in the gas and CO<sub>2</sub>-water ratios. Immediately after injection, the CO<sub>2</sub> will be stored as a free phase within the host rock. Over time, it will dissolve into the local formation water and initiate a variety of geochemical reactions.

Sediments from the modern dryland fluvial-aeolian Umbum Creek, western Lake Eyre Basin, Central Australia reflect the nature of the hinterland region, drainage basin and depositional environment. Initial rock compositions such as mineralogy, texture and grain size are the main influence on geochemical processes to become permanently trapped in the sedimentary basin by 'ionic' or 'mineral' trapping.

In the case of the Umbum Creek sands, the medium to coarse grain size, 88-92% of quartz, less than 2% of feldspar and less than 10% of lithic fragments, together with subrounded to rounded grains, moderately well sorting and very little in clay content, leads to a suitable candidate for good storage reservoir quality, if buried. However, the high evaporation conditions in the terminal splay complex environment lead to the growth of gypsum, anhydrite and salt in the sands. A similar analysis of a sedimentary basin could lead to a better assessment of CO<sub>2</sub> geological storage quality prior to sequestration.

<sup>&</sup>lt;sup>1</sup>Australian School of Petroleum, University of Adelaide, Adelaide, SA, Australia (jkaldi@asp.adelaide.edu.au)

Woodside Energy Ltd, Perth, WA, Australia (Simon, Lang@woodside.com.au)

<sup>&</sup>lt;sup>3</sup>Chevron Energy Technology Pty Ltd, Perth, WA, Australia (tobi.payenberg@chevron.com)

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Saju Menacherry<sup>1</sup>, John Kaldi<sup>1</sup>, Simon C. Lang<sup>2</sup> and Tobias Payenberg<sup>3</sup>

<sup>1</sup>CO2CRC (CRC for Greenhouse Gas Technologies), Australian School of Petroleum, The University of Adelaide, Adelaide SA 5005, Australia. Email:smenacherry@asp.adelaide.edu.au Web: http://www.asp.adelaide.edu.au/ & http://www.co2crc.com.au/

<sup>2</sup> Woodside Energy Ltd, Perth, Australia.

<sup>3</sup> Chevron Energy Technology Company Pty Ltd, Perth, Australia.

#### **ABSTRACT/SUMMARY**

The efficiency of CO<sub>2</sub> geological storage is determined by the depositional system of the sedimentary basins, in which the storage reservoir qualities of subsurface reservoir rocks are primarily controlled by their composition, texture and grain size. The ability to quantifiably predict such porosity and permeability is a significant factor in storage reservoir quality forward modeling.

The degree of reaction, reaction rates and mineralogical storage of CO<sub>2</sub> are dependent on mineral assemblage, concentration of CO<sub>2</sub> in the gas and CO<sub>2</sub>-water ratios. Immediately after injection, the CO<sub>2</sub> will be stored as a free phase within the host rock. Over time, it will dissolve into the local formation water and initiate a variety of geochemical reactions. Sediments from the modern dryland fluvial-aeolian Umbum Creek, western Lake Eyre Basin, Central Australia reflect the nature of the hinterland region, drainage basin and depositional

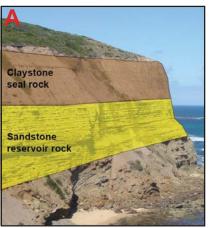
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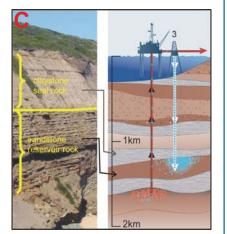
#### **INTRODUCTION**

Carbon dioxide (CO<sub>2</sub>) capture and geological storage can contribute to reduce emissions of greenhouse gas provided it is implemented on a large scale. Several types of storage reservoir may provide storage capacities of this magnitude. Conventional geological constraints on finding the right place to store CO<sub>2</sub> include having a porous and permeable reservoir rock (e.g. sandstone) to allow injection and storage of the CO<sub>2</sub>, overlain by an impermeable seal rock (e.g. claystone) to retain the injected CO<sub>2</sub> in the geological subsurface (Fig.1) (Bachu et al., 1994).

The injection and storage of carbon dioxide (CO<sub>2</sub>) in subsurface reservoirs results in chemical interaction between CO<sub>2</sub>, the formation waters and the rock itself. However, in order to understand the behaviour of CO<sub>2</sub> migration and long term safe storage of CO<sub>2</sub> such as residual, mineral and solubility trapping in the subsurface, a petrological assessment of the reservoir and seal rocks with respect to the depositional system will be undertaken. The objective of this poster is to provide a comprehensive review of the site characterisation and reservoir quality for CO<sub>2</sub> storage with respect to dryland fluvial-aeolian sediments and its depositional setting. For this purpose, an analogue study was conducted of the dryland fluvial-aeolian depositional settings of western Lake Eyre Basin, Central Australia.







**Figure 1.** Illustrating the various steps involved in geological storage of CO<sub>2</sub>. A. Site identification, B. Site characterisation and C. Injection and storing CO<sub>2</sub>.

### 2 GEOLOGICAL STORAGE

CO<sub>2</sub> can be stored geologically by a variety of different options (Fig. 2). Of these, the three main alternatives are: saline formations; oil and gas fields (once depleted or in conjunction with enhanced oil or gas recovery); and coal seams (deep unmineable or in conjunction with enhanced coal seam methane) (Bachu & Gunter, 1999; Cook et al., 2000).

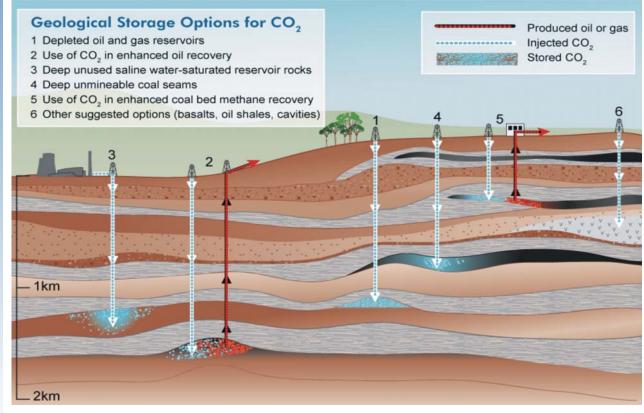


Figure 2. Options for the geological storage of carbon dioxide (CO<sub>2</sub>)

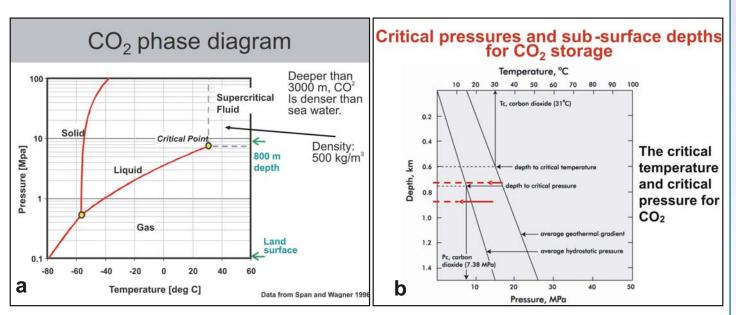






#### PROPERTIES OF CO.

The physical state of  $CO_2$  varies with temperature and pressure as shown in Figure 3a & b. At low temperatures  $CO_2$  is a solid; on warming, (if the pressure is below 5.1 bar) the solid will sublime directly into the vapour state. At intermediate temperatures (between  $-56.5^{\circ}C$  and  $31.1^{\circ}C$ ),  $CO_2$  may be turned from a vapour into a liquid by compressing it to the corresponding liquefaction pressure (and removing the heat produced). At temperatures higher than  $31.1^{\circ}C$  (if the pressure >7.38MPa (73.9 bar), the pressure at the critical point),  $CO_2$  is said to be in a supercritical state where it behaves as a gas. Indeed under high pressure, the density of the gas can be high, approaching or even exceeding the density of liquid water. This is an important aspect of  $CO_2$ 's behaviour and is particularly relevant for its storage.



**Figure 3.** (a) CO<sub>2</sub> phase diagram (after Bachu, 2000). (B) Critical temperature and pressure for CO<sub>2</sub> sequestration

The dissolution of  $CO_2$  in water (this may be seawater, or the saline water in geological formations) involves a number of chemical reactions between gaseous and dissolved carbon dioxide  $(CO_2)$ , carbonic acid  $(H_2CO_3)$ , bicarbonate ions  $(HCO_3^-)$  and carbonate ions  $(CO_3^-)$  which can be represented as follows:

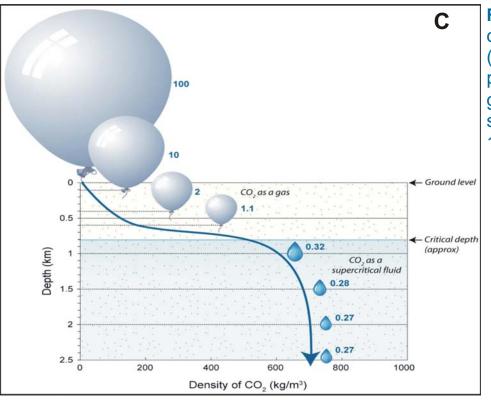
$$CO_{2 (g)} \ll CO_{2 (aq)}$$
 (1)  
 $CO_{2 (aq)} + H_2O \ll H_2CO_{3 (aq)}$  (2)

$$H_2CO_{3 (aq)} \ll H^{+}_{(aq)} + HCO_{3 (aq)}^{-}$$
 (3)

$$HCO_{3 (aq)} imes H_{(aq)}^+ + CO_{3 (aq)}^{2-} imes (4)$$

Addition of  $CO_2$  to water initially leads to an increase in the amount of dissolved  $CO_2$  (1). The dissolved  $CO_2$  reacts with water to form carbonic acid (2). Carbonic acid dissociates to form bicarbonate ions (3), which can further dissociate into carbonate ions (4). The net effect of dissolving anthropogenic  $CO_2$  in water is the removal of carbonate ions and production of bicarbonate ions, with a lowering in pH.

The depth of CO<sub>2</sub> injection and density of CO<sub>2</sub> are important parameters to consider for intermediate storage of carbon dioxide. For ease of transport and greater storage capacity, CO<sub>2</sub> is best injected as a dense, supercritical fluid. The critical point where CO<sub>2</sub> enters the supercritical phase is defined as 31.1°C and 7.38 MPa (Fig. 3a) (Holloway & Savage, 1993; Bachu, 2000). Based on worldwide average geothermal and hydrostatic pressure conditions, this equates to an approximate minimum subsurface depth of about 800 m (Fig. 3c) (Holloway & Savage, 1993). Below this depth (under normal sedimentary basin conditions) supercritical CO<sub>2</sub> is 30–40% less dense than a typical saline formation water under the same conditions (Ennis-King & Paterson, 2001, 2002). Lighter CO<sub>2</sub> will naturally rise upwards by buoyancy through the reservoir rock until trapped by various physical, hydrodynamic or geochemical trapping mechanisms (although in the longer term storage, CO<sub>2</sub> saturated brine may sink under the right conditions [Ennis-King & Paterson, 2005]).



**Figure 3c.** Variation of density with depth (assuming hydrostatic pressure, geothermal gradient of 25°C/km and surface temperature of 15°C).

The efficiency of  $CO_2$  storage in geological media, defined as the amount of  $CO_2$  stored per unit volume (Brennan and Burruss, 2003), increases with increasing  $CO_2$  density. Storage safety also increases with increasing density, because buoyancy, which drives upward migration, is stronger for a lighter fluid. Density increases significantly with depth while  $CO_2$  is in gaseous phase, increases only slightly or levels off after passing from the gaseous phase into the dense phase and may even decrease with a further increase in depth, depending on the temperature gradient (Ennis- King and Paterson, 2001; Bachu, 2003).

#### 4CO<sub>2</sub> FLOW & TRANSPORT PROCESSES

Once injected into the formation, the primary flow and transport mechanisms that control the spread of CO<sub>2</sub> include:

Fluid flow (migration) in response to pressure gradients created by the injection processes;

Fluid flow in response to natural hydraulic gradient;

**B**uoyancy caused by the density differences between CO<sub>2</sub> and the formation fluids;

Diffusion;

**D**ispersion and fingering caused by the formation heterogeneities and mobility contrast between CO₂ and formation fluid;

Dissolution into the formation fluid;

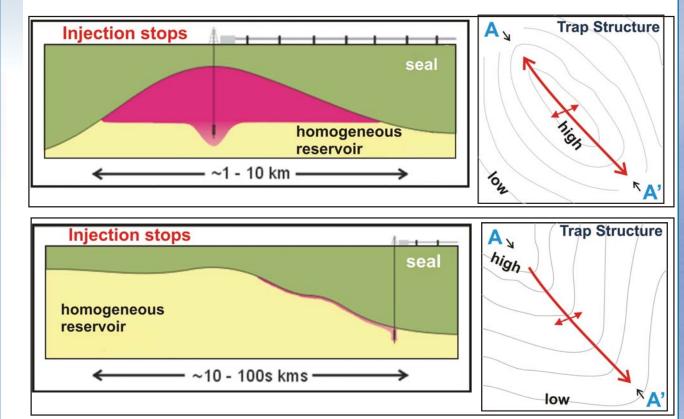
Mineralization;

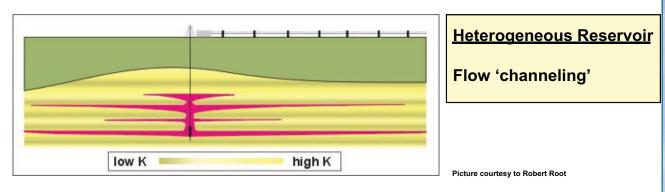
Pore space (relative permeability) trapping;

Adsorption of CO<sub>2</sub> onto organic material.

#### CONCEPTUAL CO<sub>2</sub> STORAGE SCENARIO

The storage mechanism known as physical trapping of CO<sub>2</sub> below low permeability seals (caprocks), such as very low- permeability shale or salt beds, is the principal means to store CO<sub>2</sub> in geological formations. Sedimentary basins have such closed, physically bound traps or structures, which are occupied mainly by saline water, oil and gas. Structural traps include those formed by folded or fractured rocks. Stratigraphic traps are formed by changes in rock type caused by variation in the setting where the rocks were deposited.





### Amount of CO<sub>2</sub> geologically stored influenced by:

- Rate of CO<sub>2</sub> migration
- Style of multiphase flow
- Rate of CO<sub>2</sub> dissolution
- Rate of chemical reaction with minerals

#### Controlled by many variables, including:

- Reservoir and seal structure
- Stratigraphic architecture
- Reservoir heterogeneity
- Faults/fractures
- Pressure/temperature conditions
- Hydrodynamics and chemistry of in situ formation fluids

**Figure 4.** Illustrates the conceptual CO<sub>2</sub> storage in homogenous and heterogeneous reservoirs

Reservoir heterogeneity also affects CO<sub>2</sub> storage efficiency and hence intermediate storage. The density difference between the lighter CO<sub>2</sub> and the reservoir oil and/or saline water leads to movement of the CO<sub>2</sub> to the top of the reservoir; particularly, if the reservoir is relatively homogeneous and has high permeability, it is well suited for intermediate storage of CO<sub>2</sub>. This negatively affects the CO<sub>2</sub> storage and oil recovery. Consequently, reservoir heterogeneity may have a positive effect, slowing down the rise of CO<sub>2</sub> to the top of the reservoir and forcing it to spread laterally, giving more complete invasion of the formation and greater storage potential (Flett et al., 2005).

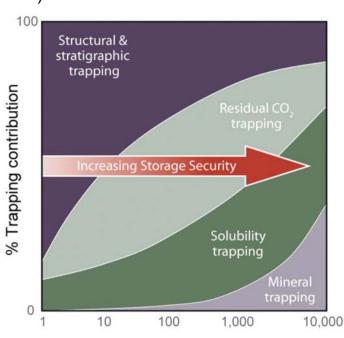






#### 6 TRAPPING MECHANISMS

In any geological storage site, the injected  $CO_2$  will ultimately be trapped by a number of the mechanisms. The type of trapping, if and when it occurs, is dependent on the dynamic flow behaviour of the  $CO_2$  and the time-scale involved. With increasing time, the dominant storage mechanism will change and typically the storage security also increases. Figure 5 is a simple representation of  $CO_2$  storage and how the trapping mechanism alters over time. Because of multiple storage mechanisms working at multiple length and time scale, the shallow crust should attenuate mobile free-phase  $CO_2$  plumes, trap them residually, & ultimately dissolve them. This means that over time risk decreases and permanent trapping increases. For example, the initial storage mechanism will dominantly be physical structural and stratigraphic trapping of the immiscible-phase  $CO_2$ . With increasing time and migration, more  $CO_2$  is trapped residually in the pore space and is dissolved in the formation water to increase the storage security. Finally, mineral trapping may occur by precipitation of new carbonate minerals after reaction of the dissolved  $CO_2$  with the host rock mineralogy, thus permanently trapping the  $CO_2$  (IPCC, 2005).

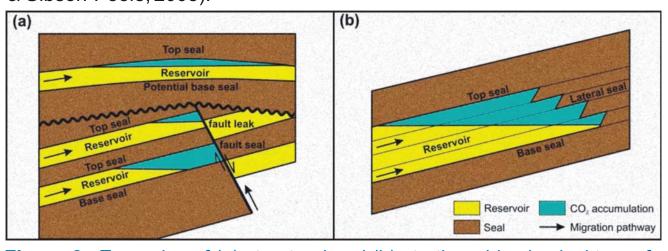


Time since injection stops (years)

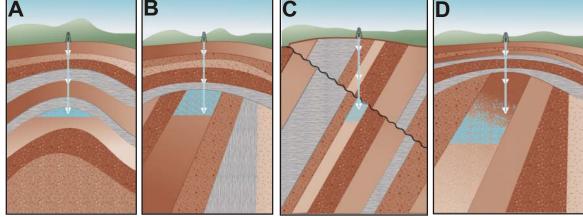
**Figure 5.** Schematic representation of the change of dominant trapping mechanisms and increasing CO<sub>2</sub> storage security with time (IPCC, 2005).

### STRUCTURAL/STRATIGRAPHIC TRAPPING

Structural/stratigraphic trapping relates to the free-phase (immiscible) CO<sub>2</sub> that is not dissolved in formation water. When supercritical CO<sub>2</sub> rises upwards by buoyancy it can be physically trapped in a structural or stratigraphic trap (as a result of the CO<sub>2</sub> being the non-wetting phase). The nature of the physical trap depends on the geometric arrangement of the reservoir and seal units. Common structural traps include anticlinal folds or tilted fault blocks (Fig 6a) and typical stratigraphic traps include those created by a lateral change in facies up-dip or a depositional pinch-out (Fig 6b). There are numerous variations of structural and stratigraphic traps (Fig 7A-D), plus combinations of both structural and stratigraphic elements that can provide physical traps for geological storage of CO<sub>2</sub> (Kaldi & Gibson-Poole, 2008).



**Figure 6.** Examples of (a) structural and (b) stratigraphic physical traps for CO<sub>2</sub> (modified from Biddle & Wielchowsky, 1994).



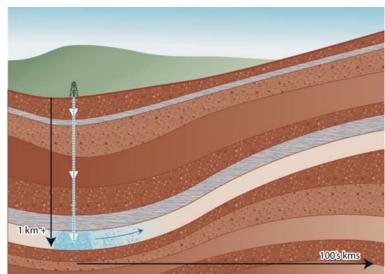
**Figure 7.** Showing examples of structural and stratigraphic trapping

A. Anticline trapping
B. Unconformity
trapping

C. Fault trapping

D. Facies change trapping

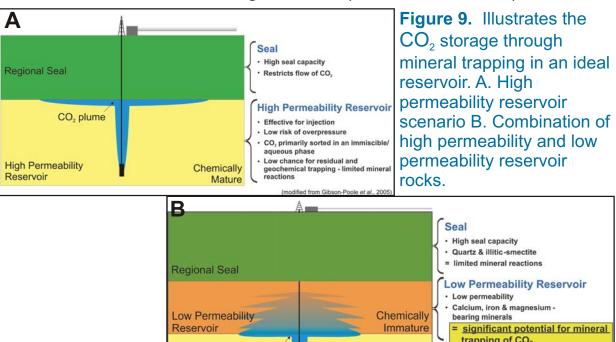
In hydrodynamic trapping the flow of the injected freephase CO<sub>2</sub> is dependent on the dip of the sealing horizon and the flow velocity and direction of the *in situ* formation water. In horizontal or gently dipping reservoirs, this can lead to very long residence times (thousands to millions of years) (Fig 8) (Bachu et al., 1994).



**Figure 8.** Hydrodynamic trapping of CO<sub>2</sub>, where the CO<sub>2</sub> migration pathway is 10s to 100s km long allowing for a long residence time (Bachu et al., 1994; Kaldi & Gibson-Poole, 2008).

#### 8 MINERAL TRAPPING

Mineral trapping is quite variable from formation to formation and thus needs to be examined as part of the site characterisation process for storage site selection. Mineral trapping is a function of the mineralogy of the reservoir rock, the chemical composition of the formation water and the formation temperature and pressure. In addition, potential reactions depend on the contact surface (interface) between the mineral grains and the formation water containing dissolved CO<sub>2</sub>, and on the flow rate of fluids through the rock (Gunter et al., 2004).

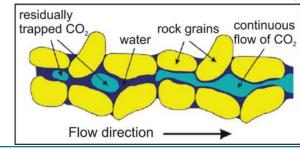


CO<sub>2</sub> plume

High Permeability

#### 9 RESIDUAL TRAPPING

Residual trapping occurs when the  $CO_2$  becomes trapped in the pore space as a residual immobile phase by capillary forces (Fig 10) (Ennis-King & Paterson, 2001; Flett et al., 2005). At the tail of the migrating  $CO_2$  plume, imbibition processes are dominant as the formation water (wetting-phase) imbibes behind the migrating  $CO_2$  (non-wetting phase). When the concentration of the  $CO_2$  falls below a certain level, it becomes trapped by capillary pressure forces and ceases to flow (Ennis-King & Paterson, 2001; Flett et al., 2005). Therefore, a trail of residual, immobile  $CO_2$  is left behind the plume as it migrates upward (Juanes et al., 2006). Residual  $CO_2$  saturation values vary between 5–30 % based on typical relative permeability curves (Ennis-King & Paterson, 2001). Over time, the residually trapped  $CO_2$  dissolves into the formation water (Ennis-King & Paterson, 2001; Flett et al., 2005).



rock grains continuous flow of CO<sub>2</sub> Figure 10. Residual trapping of Co<sub>2</sub>

High Permeability Reservoir

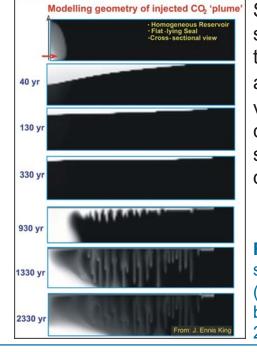
Moderate to high permeability

Non-reactive minerals

Chemically

#### **10 SOLUBILITY TRAPPING**

Solubility trapping relates to the CO<sub>2</sub> dissolved into the formation water (Koide et al., 1992). Carbon dioxide solubility increases with increasing pressure and decreases with increasing temperature and water salinity. Carbon dioxide may mix with, and then dissolve in, formation water through the processes of diffusion, dispersion and convection. The density of the CO<sub>2</sub>-saturated water increases to become about 1 % more than that of the unsaturated water. The dense CO<sub>2</sub>-saturated water overlying less dense unsaturated water creates a density instability and plume of CO<sub>2</sub>-rich water flow downward (Fig 11) (Ennis-King & Paterson, 2002; Ennis-King & Paterson, 2005).



Stratigraphic heterogeneities also improve solubility trapping, as they increase the tortuosity of the CO<sub>2</sub> migration path, and accordingly the CO<sub>2</sub> contacts larger volumes of formation water into which it can dissolve (Flett et al., 2005). The timescale for complete dissolution is critically dependent on the vertical permeability.

**Figure 11.** Solubility trapping simulation showing the high-density Co<sub>2</sub>-saturated brine (grey colours) sinking into the brine column below (white colour) (Ennis-King & Patterson, 2005).







## 11 ANALOGUE STUDY: UMBUM CREEK, WESTERN LAKE EYRE BASIN, AUSTRALIA.

Introduction: The Lake Eyre Basin is a wide shallow, low gradient intracratonic basin which records a complex history of alluvial, lacustrine and aeolian, reflecting several tens of millions years of environmental change. Lake Eyre is the fourth largest terminal playa lake in the world. It is a vast downwarped area of low relief and internal drainage of 1,140,00 km². The Umbum Creek catchment area drains the Davenport Ranges, covering approximately 200 km² of Palaeo-Proterozoic metasediments and volcanics, Neo-proterozoic metasediments and Mesozoic and Cainozoic sedimentary rocks of the Eromanga Basin. Additionally, there is reworking of Neogene gibber plains, aeolian sand dunes, and fluvial sands at the base of the Davenport Ranges. Umbum Creek flows into a modern ephemeral braid-delta/terminal splay complex build into the arid Lake Eyre playa.

The analogue study of the Umbum Creek fluvio-aeolian-dominated terminal splays associated with dryland depositional environments are significant in determining the site characteristics for CO<sub>2</sub> storage in intracratonic reservoirs in many subsurface basins around the world. Potential reservoirs include the Permian Upper Rotliegend Group of northern Europe; the Jurassic Norphlet Formation sandstone reservoirs in Mobile Bay, Alabama, USA; and the Mesozoic Etjo Sandstone Formation, northwest Namibia.



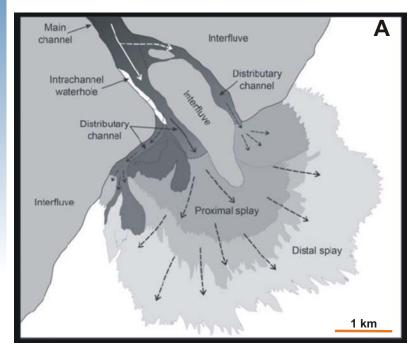






Figure 12. A. Location map. B, C and D. Aerial view of Umbum Creek Terminal splay

## 12 SEDIMENTOLOGY & ARCHITECTURE OF THE UMBUM CREEK TERMINAL SPLAY



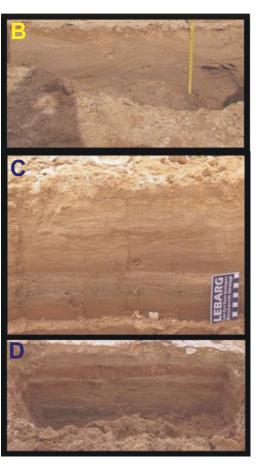


Figure 13. A. Umbum Creek Terminal Splay architectural elements. B. Distributary channel with thick cross-bedded, coarse-medium sands and basal lags. C. Stacked sheets of small-scale trough cross-bedded, massive and ripple-laminated sands overlying a thin gravel layer at the proximal splay. D. Thin stacked sheets of massive and ripple-laminated fine sands, interlayering of silt and clay as seen in the distal splay.

Variability in splay morphology and architecture reflects the influence of different depositional processes operating to build the splay complexes. Multiple factors are thought to influence splay development, including catchment size, discharge, vegetation, grain-size distribution and composition of fluvial-aeolian transported sediment, as well as the influence of successive lake filling events which may result in a change from sheetflood to deltaic processes.

Three primary facies associations have been identified which subdivide the Umbum Creek terminus into distributary channel, proximal and distal splay sections. Proximal splay sediments are characterized by erosionally based, relatively thick (> 100 mm), stacked sheets of coarse-medium sand, which commonly display trough & planar cross-bedding. The distal splay is characterized by thin (generally < 50 mm) massive beds of very fine sand, silt and clay.

#### 13 KEY OBSERVATIONS

The Umbum Creek terminal splay complex covers an area approximately 300 km<sup>2</sup>.

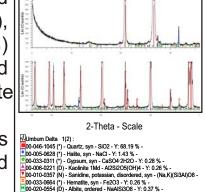
**Grain Size:** Grain-size estimates were taken qualitatively from logging trenches in the field and measured quantitatively from twenty four samples which were dried and sieved in the laboratory.

The proximal splay has an average grain-size distribution of medium-coarse-grained sand. The distal splay sediments have an average grain size of silt to medium-grained sand. Sorting improves with increasing distance from the feeder channel. The grains are subrounded to well rounded. This is indicative of the fluvio-aeolian influence on the sediments.



**Significance**: This results in moderate to low compaction, which preserves porosity and permeability for CO<sub>2</sub> injection and migration.

Mineralogy (composition): The modern sand composition is monocrystalline quartz (60-70%), polycrystalline quartz (10-20%), lithics (<15%) and feldspar (<5%). The clay fraction is dominated by quartz. However, clay minerals, feldspar, halite and gypsum comprise approximately 30% of the clay fraction. Sediment provenance comprises granitic, volcanic, metasediments and sedimentary rocks.

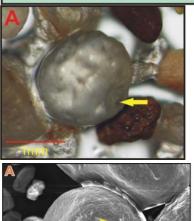


**Significance**: The high quartz content provides high mechanical and chemical stability, thus preserving porosity and permeability for CO<sub>2</sub> migration.

**Grain coating:** The shape of the grains in the terminal splay complex is angular to well rounded. Grain angularity promotes formation of cements and grain coatings. Early grain coating is aluminium silicates, titanium oxide and clay minerals. Quartz, halite and gypsum are the other cements identified within the terminal splay complex.

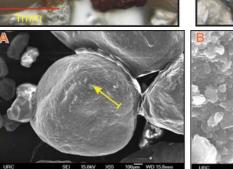
**Significance:** Cementation destroys porosity. However, late diagenesis (dissolution) creates secondary porosity and permeability, which increases CO<sub>2</sub> migration and later mineralization trapping.

Arrows showing the percussion marks (A & C) and roundness of the aeolian grains(B)









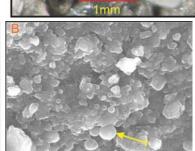


Figure 14. A. Quartz overgrowth on aeolian grain. B. Microquartz sphere balls overgrowth on polycrystalline quartz.

Sedimentary structures (bed forms): The main characteristic features are thin beds (0.1 to 0.3m) which comprise coarse-medium sands with gravel layers, trough cross-bedded, thinly stacked sheets of ripple-laminated fine sands alternating with layers of silt and clay. The predominance of horizontal laminations, widespread presence of mud drapes and mud intraclasts are associated with aeolian sand beds and cemented with silica, halite and gypsum.



**Significance**: CO<sub>2</sub> migration in the less porous and permeable distal splay deposits is slow due to reservoir heterogeneity, thus creating new mineralization. Subsequently, reservoir heterogeneity has a positive effect in slowing down the rise of CO<sub>2</sub> to the top of the reservoir.



Figure 15. A. Cross-beds, laminations. B. Association of aeolian sediments. C. Laminations of fine silt and clay layers.





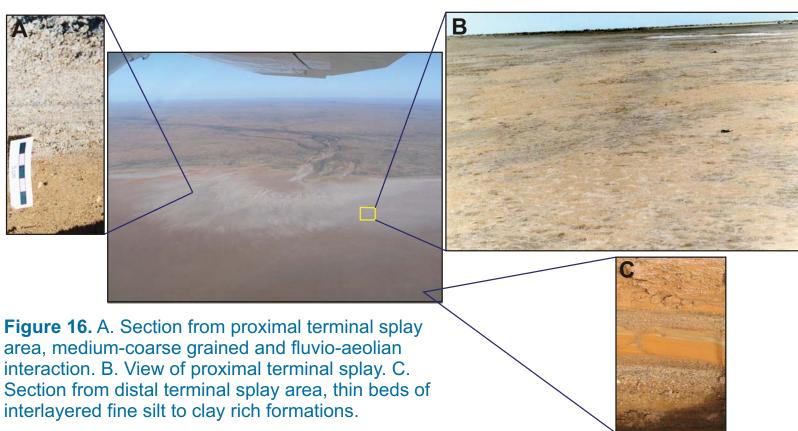




#### 14 RESERVOIR CHARACTERIZATION OF UMBUM TERMINAL SPLAY FOR CO2 SEQUESTRATION

Storage Potential: Storage site requirements depend on trapping mechanisms and geological depositional setting. The reservoir characteristics are the major criteria for selecting sites for long or intermediate term storage of CO<sub>2</sub>. Umbum Creek terminal splay deposits (of western Lake Eyre Basin) have the potential to be used as analogues for geological storage of CO<sub>2</sub>.

**Reservoir Heterogeneity:** Reservoir heterogeneity affects CO<sub>2</sub> storage efficiency and hence long or intermediate term storage. The density (buoyancy) difference between the supercritical CO, and the reservoir oil and/or saline water leads to movement of the CO<sub>2</sub> along the top of the reservoir; particularly, if the reservoir is relatively homogeneous and has high permeability, it is well suited for intermediate storage of CO<sub>2</sub>. Consequently, reservoir heterogeneity may have a positive effect, slowing down the rise of CO<sub>2</sub> to the top of the reservoir and forcing it to spread laterally, giving more complete invasion of the formation and greater storage potential (Flett et al., 2005). With respect to the Umbum Creek terminal splay complex, the proximal splay formations facilitate fast amalgamation of CO<sub>2</sub> because of high porosity and permeability within the rocks. However, the widespread interlayered clay and silt laminations in the distal splay deposits reduce the migration of CO<sub>2</sub>. Thus, the dryland depositional setting and the heterogenous reservoir nature of Umbum Creek terminal splay suggest that it is suitable for intermediate and long term storage purposes.



Saline Aquifers: When CO<sub>2</sub> is injected into a deep saline formation in a (liquid-like) supercritical phase, it is immiscible in water. Because supercritical CO<sub>2</sub> is much less viscous (flows more easily) than water and oil (by an order of magnitude or more), migration is controlled by the contrast in mobility of CO<sub>2</sub> and the *in situ* formation fluids (Celia et al., 2005). Thus due to the comparatively high mobility of CO2, some of the oil or water is displaced, leading to an average saturation of CO2 in the range of 30-60%.

In saline formations, the comparatively large density difference (30–50%) between CO<sub>2</sub> and formation water creates strong buoyancy forces that drive CO<sub>2</sub> upwards. The upward migration of the buoyant plume of injected CO<sub>2</sub>, however, may not be evenly distributed. This is because the presence of a lower permeability layer will act as a barrier/baffle and cause the CO2 to migrate laterally, thus filling any stratigraphic or structural trap it encounters. This creates conditions where part of the injected CO<sub>2</sub> is able to dissolve in the formation water. Due to changing formation water pH, solubility trapping occurs. Solubility trapping eliminates the buoyant forces that drive CO<sub>2</sub> upward migration through the reservoir.

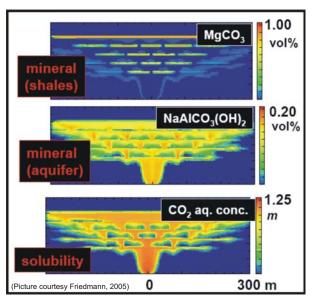
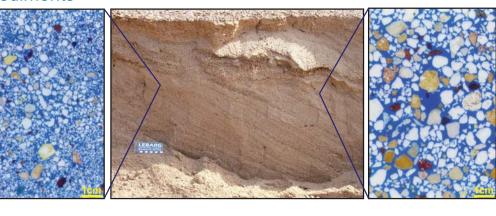


Figure 17. Illustrates mineral trapping mechanisms in shale and aquifer section of the formation and solubility trapping in deep saline aquifer formations. Thin section from the splay sediments



The residual trapping of CO<sub>2</sub> may immobilize significant amounts of CO<sub>2</sub>. Studies show that when the degree of trapping is high and CO is injected at the bottom of a highly porous and permeable heterogenous formation, all of the CO<sub>2</sub> may be trapped by this mechanism, even before it reaches the caprock at the top of the formation. While this effect is formation-specific (depositional setting), Holtz (2002) has demonstrated that residual CO<sub>2</sub> saturations may be as high as 15–25% for storage formations.

The combined effects of dissolution, solubility trapping and residual trapping thus favour the use of deep saline aquifers for long term CO<sub>2</sub> storage. However, proper injection planning such as gasphase injection may reduce the dissolution of CO<sub>2</sub> in the formation water and thus facilitate intermediate storage in saline aguifers. The Umbum Creek terminal splay complex sediment composition consists of higher quartz content, with lesser feldspar and lithics contents and cements of clay, halite and evaporites. This mineralogy suggests a high potential for geochemical reactions with CO<sub>2</sub> and formation water. Thus, Umbum Creek fluvial-aeolian terminal splay sediments may allow for permanent CO<sub>2</sub> storage in the formations, if buried.

The interaction of CO<sub>2</sub> in high permeability proximal splay formation could have low reactive potential, due to the dominance of quartz and limited labile minerals, such as feldspar, carbonates and clays. However, CO<sub>2</sub>induced diagenesis increases the partial to total dissolution reaction from feldspar to kaolinite, and minor siderite and calcite precipitation (Watson and Gibson-Poole, 2005).

The study, based on the depositional settings and the petrological aspects suggests that CO<sub>2</sub> flow and transport processes are directly linked to the geochemical trapping mechanisms. The migration pathways of CO<sub>2</sub> are highly controlled by the reservoir heterogeneities in the terminal splay complex. Other site characterization criteria such as formation pressures, in situ stresses, tectonic stability, faulting intensity and geothermal gradient are not discussed in this study.

#### 15 CONCLUSIONS

The storage of CO<sub>2</sub> in a reservoir depends very much on criteria such as the depth of injection and density, CO<sub>2</sub> flow and transport processes, storage mechanisms, reservoir heterogeneity, type of the reservoir and duration of storage (intermediate or long term).

- 1. The heterogeneous nature of Umbum Creek terminal splay complex deposition facilitates the intermediate and long term CO<sub>2</sub> storage.
- 2. Mineralogy enables high potential for porosity and permeability, which increase the geochemical reaction with CO and formation water, thus accelerating mineralization, solubility trapping and residual trapping for a long term permanent CO<sub>2</sub> storage.
- 3. Solubility trapping increases with the interaction of diagenetic minerals and cements with CO<sub>2</sub> plume.
- 4. Migration pathways are controlled by the proximal and distal splay depositional settings and mineral composition.
- 5. Understanding the variation in terminal splay architecture, depositional setting and mineral composition has very significant implications for the modeling of analogues for potential characterization of sites for CO<sub>2</sub> sequestration.

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