### Thermochemical Sulfate Reduction (TSR): H<sub>2</sub>S Risk Assessment at the Basin Scales\*

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#### **Abstract**

High concentrations (>10vol% in reservoirs) of hydrogen sulfide (H<sub>2</sub>S), a toxic and economically-damaging gas, result from thermochemical sulfate reduction (TSR) of petroleum. TSR occurs in high temperature carbonate reservoirs, and is very detrimental to the quality and the volume of hydrocarbon resources. Therefore, accurate TSR modeling is important to lower the risks during petroleum E&P. TSR involves complex redox reactions, that lead to petroleum oxidation and reduction of sulfates. The main products of reaction are either volatile (carbon dioxide (CO<sub>2</sub>), H<sub>2</sub>S) or solid (carbonate cements, pyrobitumen). The volatile products may migrate up from deeper reservoirs in both the gas and solution (either in water or in oil) phase. We developed a post-calculator approach integrated to the TemisFlow software, in order to assess maximum H<sub>2</sub>S amounts resulting from TSR. The model is based on a mass balance approach according to the overall chemical reaction which has been first proposed by Utevev (2011):  $8 \text{ CnHm} + (4n+m) \text{ CaSO}_4 = (4n+m) \text{ CaCO}_3 + (4n+m) \text{ H}_2\text{S} + (4n-m) \text{ CO}_2 + (3m-4n) \text{ H}_2\text{O}$ . The stoichiometry of the reaction is clearly related to H/C ratio of the hydrocarbon. Water may either be consumed or produced by the reaction. Temperature, pressure, porosity, HC amount, and salinity are inherited from the TemisFlow calculator. A necessary additional input is the map of sulfate minerals in the basin. The model outputs are H<sub>2</sub>S and CO<sub>2</sub> quantities, as well as their distribution in a gas phase or dissolved in the basinal brine. The volume of dissolved sulfate and the volume of precipitated calcite are also computed, and the porosity evolution related to the TSR reaction is assessed. An identification of areas where H<sub>2</sub>S is expected to be present is then workable. Devonian carbonate reservoirs of the Nisku and Leduc formations (Alberta) include HC fields that experienced TSR and may contain up to 30% of H<sub>2</sub>S. A 3D model, taking into account subsidence history and subsequent erosional profiles, of the Alberta foreland basin has been built. Results provide the timing of the Devonian petroleum system accounting for the HC charges of Devonian-Mississippian carbonate reservoirs. This study moreover investigates the impact of critical parameters (oil composition, salinity, H/C) on the production of H<sub>2</sub>S by TSR in the Devonian Formations. Our numerical results are compared to wells data and clearly show that the H<sub>2</sub>S production occurred mainly before the last erosion.

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Machel, H.G., 2005, Geological and Hydrogeological Evaluation of the Nisku Q-Pool in Alberta, Canada, for H<sub>2</sub>S and/or CO<sub>2</sub> Storage: Oil & Gas Science and Technology – Rev. IFP, v. 60/1, p. 51-65.

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Uteyev, R., L. Richard, J. Sterpenich, A. Clement, and D. Dessort, 2009, A Thermodynamic and Mass Transfer Analysis of Organic/Inorganic Interactions During Thermochemical Sulfate Reduction in Carbonate Reservoirs: Goldschmidt 2009, Jun 2009, Davos, Switzerland, 73 (13, Supplement 1), p. A1363.

Zhang, T., G.S. Ellis, K.S. Wang, C.C. Walters, S.R. Kelemen, B. Gillaizeau, and Y. Tang, 2007, Effect of Hydrocarbon Type on Thermochemical Sulfate Reduction: Organic Geochemistry, v. 38/6, p. 897-910.

## THERMOCHEMICAL SULFATE REDUCTION (TSR): H<sub>2</sub>S RISK ASSESSMENT AT THE BASIN SCALES

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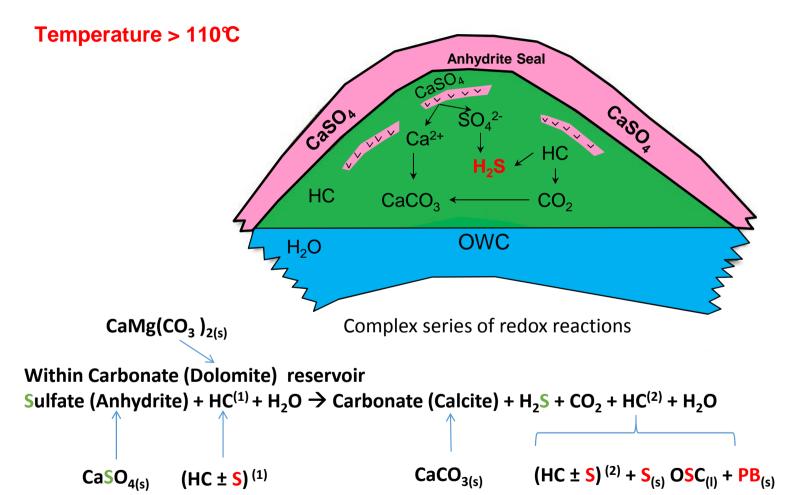
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### **OVERVIEW**

- What is TSR?
- TSR risk index within TemisFlow<sup>TM</sup>
  - Assessment of the reaction progress
  - Assessment of the masses of the reaction products
- Validation/discussion based on Alberta foreland basin Nisku Devonian formation
- Conclusion and perspectives







### INDUSTRIAL CONTEXT

- Industrial context:
  - TSR increases the risk in exploration
- Consequences :
  - A strong decrease in the hydrocarbon potential of a reservoir due to oxidation of the oil (leading to CO<sub>2</sub> and carbonates).
  - A strong decrease of the quality of the produced fluids due to the formation of large amounts of H<sub>2</sub>S (and OSC, PB)
  - A strong increase of production costs due to the highly toxicity and corrosion induced by H<sub>2</sub>S



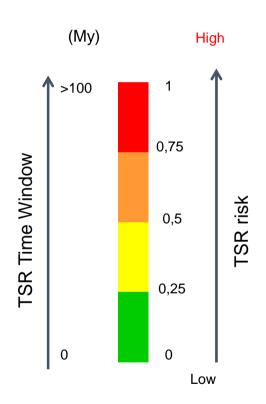
- 2 types of calculations
  - First step of TSR risk Assessment of the reaction progress
    - based on a HC residence time within the TSR conditions
    - Time window of TSR reaction = TSR occurrence probability
  - Second step of TSR risk Assessment of the masses of the reaction products
    - based on a mass balance calcutation by using a stoechiometric equation of sulfates reduction into H<sub>2</sub>S
    - Mass of fluids : HC, H<sub>2</sub>S, CO<sub>2</sub>
    - Mass of solids : Sulfate, Carbonate



### RESPONSIBLE OIL AND GAS

### FIRST STEP: ASSESSMENT OF THE REACTION PROGRESS

- Input paramaters based on geological data (Nisku (Canada), Smackover (USA), Khuff (Abu Dhabi), ...)
  - Temperature : T°C> T<sub>user</sub> (default 110°C)
  - Oil Saturation: Smin (10%) < Soil (%) < Smax (90%)</li>
  - Lithofacies: Sulfates source Anhydrite %
- Output paramaters
  - Residence time of a cell at the TSR conditions → TSR Time Window in My
  - TSR Risk assessment (normalized index)
    - Equivalent of a reaction progress or TSR occurrence probability
  - Computed at present day and through geological time
    - Allow to identify the onset of the reaction and maximum occurrence probability time



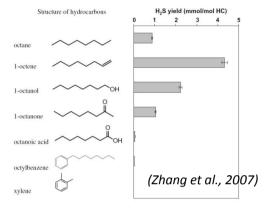


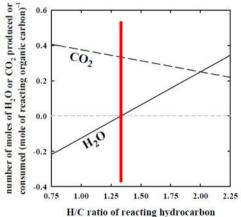
### SECOND STEP: ASSESSMENT OF THE MASSES OF THE REACTION PRODUCTS

### $8 C_n H_m + (4n+m) CaSO_4 \rightarrow (4n+m) CaCO_3 + (4n+m) H_2 S + (4n-m) CO_2 + (3m - 4n) H_2 O_3$

- Input paramaters (necessary conditions)
  - Parameters defined by the user
    - Maximum of HC consumption by TSR reaction (directly linked to H/C ratio)
  - Parameters issued from basin modelling
    - Pressure, Temperature and salinity for thermodynamical calculation
    - Masses of HC from migration calculation
  - Possibility to control the reaction progress by using the TSR occurrence probability
- Output parameters
  - Complete mass balance:
    - Mass of HC and Anhydrite consumed
    - Total Mass of H<sub>2</sub>S and CO<sub>2</sub> distributed in soluble and gaseous forms
    - Mass of Carbonate precipited
  - Complete volumetric balance
    - Porosity variation as a function of anhydrite and carbonate summary
    - Volume of gases in the available porespace → qualitative information on cap rock integrity
- Computation in a post-processing from migration calculation
  - No migration of the products

### RESPONSIBLE OIL AND GAS





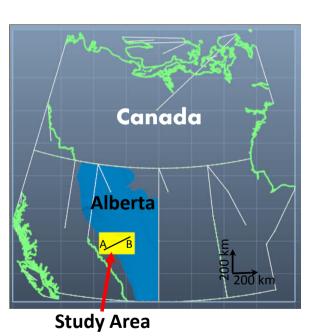
(Uteyev, 2011)

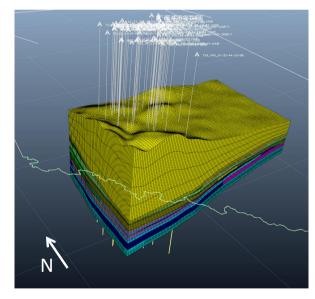


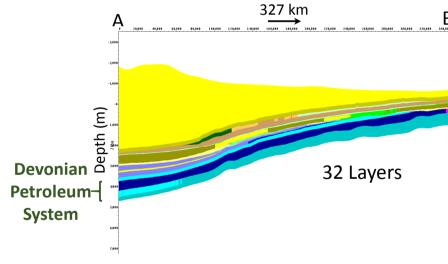
### CASE STUDY – ALBERTA BASIN

3D model of Alberta foreland basin (West of Edmonton city)

Canada : Nisku/Leduc Formation, Devonien Up to  $90\% H_2S$ , T = 125-145°C



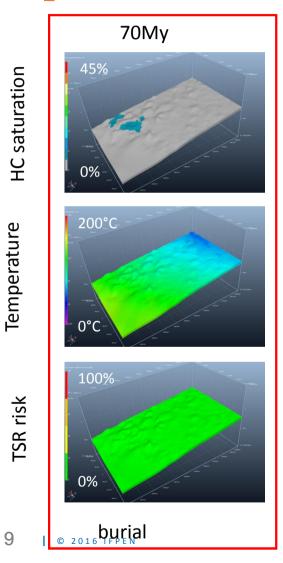


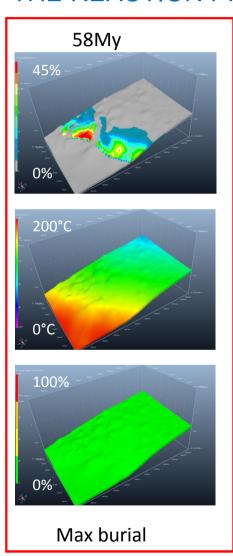


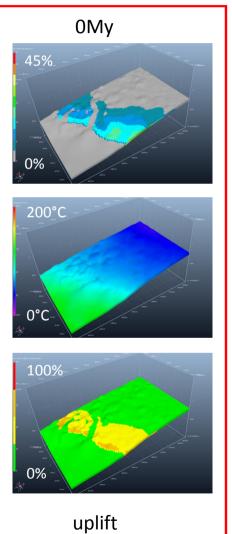


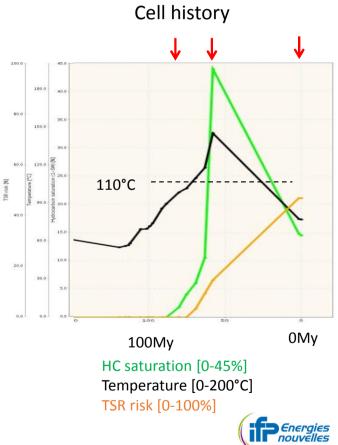
### ASSESSMENT OF THE REACTION PROGRESS AT NISKU FM.

RESPONSIBLE OIL AND GAS







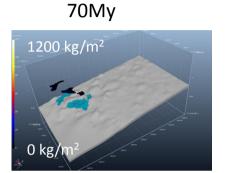


### RESPONSIBLE OIL AND GAS

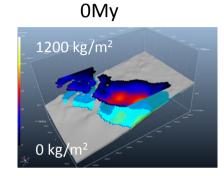
## H<sub>2</sub>S gas mass

## **Temperature**

## ASSESSMENT OF THE H2S MASSES OF THE REACTION PRODUCTS AT NISKU FM.

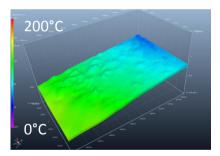


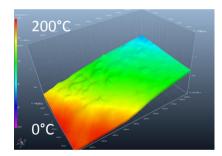
58My 1200 kg/m<sup>2</sup>



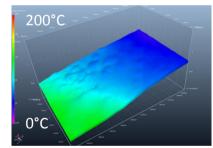


 Post-pro computed by using HC saturation only (without taking into account TSR risk)



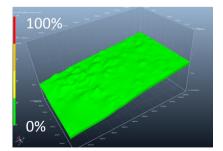


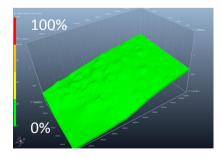
0 kg/m

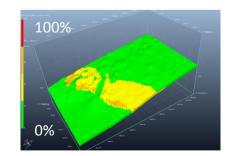


### Conclusion

 H<sub>2</sub>S gas generation does not represent a kinetic reaction





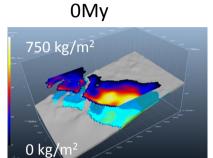


### RESPONSIBLE OIL AND GAS

### ASSESSMENT OF THE H2S MASSES OF THE REACTION PRODUCTS AT NISKU FM.

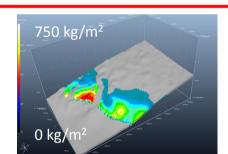
70My 1200 kg/m<sup>2</sup>



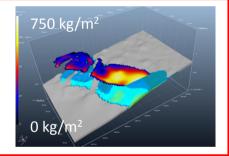


Hypothesis

 Post-pro computed by using HC saturation + starting the reaction when TSR risk is 25%

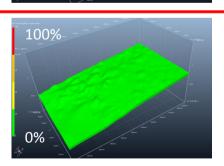


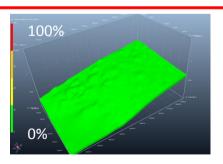
0 kg/m

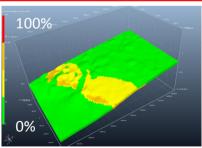


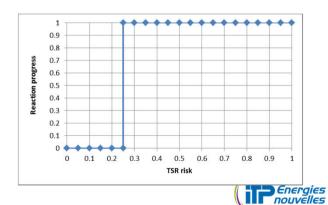
### Conclusion

 H<sub>2</sub>S gas generation better represents a kinetic reaction









H<sub>2</sub>S gas mass

gas mass

H<sub>2</sub>S

0 kg/m

0 kg/m

750 kg/m<sup>2</sup>

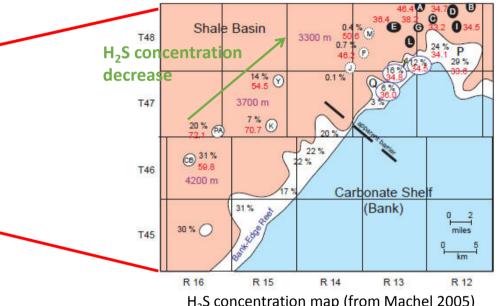
#### RESPONSIBLE OIL AND GAS

### ASSESSMENT OF THE H2S MASSES OF THE REACTION PRODUCTS AT NISKU FM.



# 750 kg/m<sup>2</sup> $0 \text{ kg/m}^2$

### Brazeau Reservoir Map



H<sub>2</sub>S concentration map (from Machel 2005)

- General H<sub>2</sub>S mass trend reproduced
- No migration of generated H2S tends to overestimate of H<sub>2</sub>S quantities

- Average H<sub>2</sub>S Masses from Machel (2005): 300 kg/m<sup>2</sup>
  - $\bullet$  H<sub>2</sub>S gas = 140 kg/m<sup>2</sup>
  - $\bullet$  H<sub>2</sub>S dissolved = 160 kg/m<sup>2</sup>

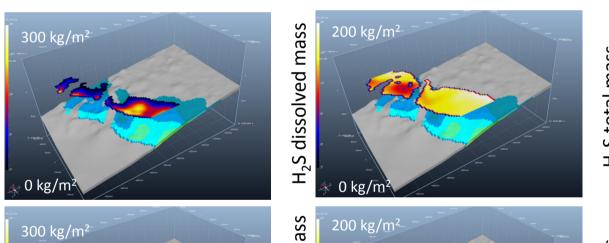


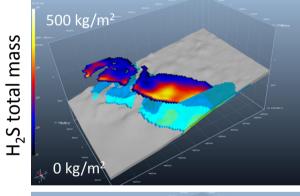
H<sub>2</sub>S gas mass

13

## ASSESSMENT OF THE H2S MASSES OF THE REACTION PRODUCTS AT 0MY

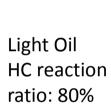
- Hypothesis
  - Post-pro computed by using HC saturation + starting the reaction when TSR risk
     is 25% + ponderating the reaction by the TSR risk
- Conclusion: H<sub>2</sub>S masses in better agreement with measured data





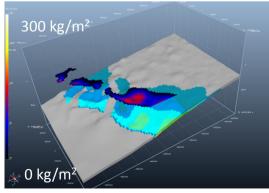
0.9

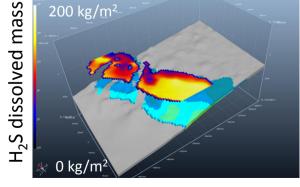
0.5 0.4 0.3

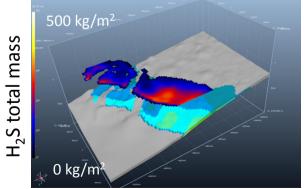


TSR risk

0.7





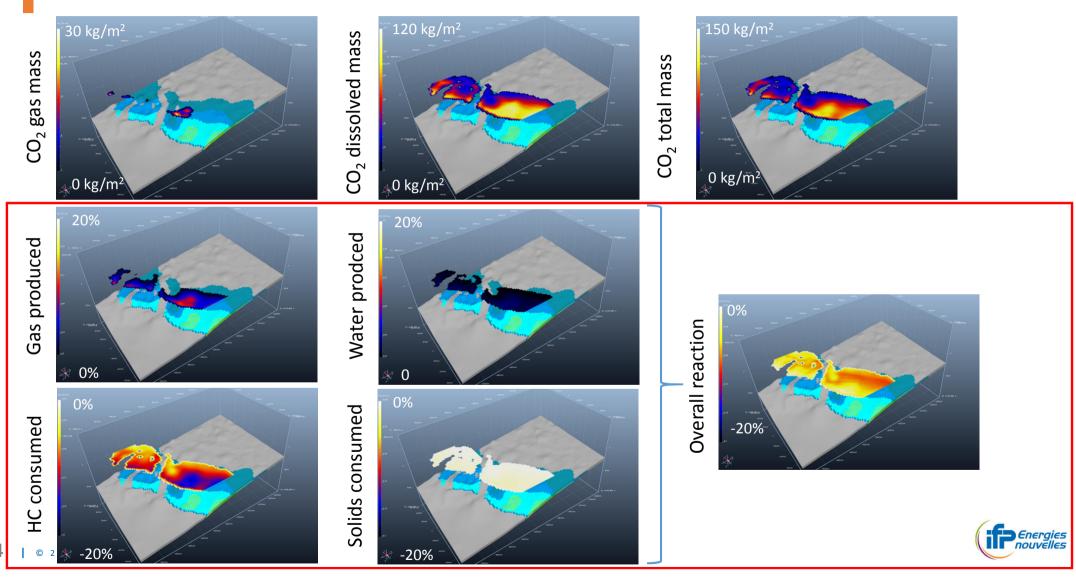


Medium Oil HC reaction ratio: 60%



### OTHER RESULTS AT 0MY

 $8 C_n H_m + (4n+m) CaSO_4 \rightarrow (4n+m) CaCO_3 + (4n+m) H_2 S + (4n-m) CO_2 + (3m - 4n) H_2 O$ 



### CONCLUSION

- 2 types of calculations has been developed within TemisFlow<sup>TM</sup> to assess an H<sub>2</sub>S risk from a TSR reaction
  - A first TSR risk on the commercial version:
    - Assessment of the reaction progress based on HC residence time within the TSR conditions
    - TSR Time Window (My) and TSR Risk assessment (/)
  - A second TSR risk under developpement:
    - Assessment of the masses of the reaction products based on a Stoechiometric equation of sulfates reduction
    - Mass/Volume of fluids (HC, H<sub>2</sub>S, CO<sub>2</sub>) and solids (Sulfate, Carbonate)
    - Strengths
      - The masses of produced H<sub>2</sub>S and CO<sub>2</sub> are distributed between vapor and liquid phases
      - Compositional HC description can be used
      - Fast computation
    - Weaknesses
      - No migration
- Perspectives
  - migration module of TemisFlow<sup>TM</sup> in link the 3 phases flow under developpement
  - Continue the validation process with more quantitative data



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