

# **Experimental and Theoretical Study of Water and Solute Transport Mechanisms in Organic-Rich Carbonate Mudrocks\***

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## **Abstract**

The objective of this research is to determine the physicochemical processes underlying water and solute transport in organic-rich source rocks. Experiments were performed on Eagle Ford shale samples composed of organic-rich, low-clay carbonates using a high-pressure triaxial assembly with novel design. Experimental results were successfully matched with a numerical chemical transport model. The mathematical formulation of this model relies on the chemical osmosis principles driving low-salinity brine into high salinity core samples. The results of this research should be beneficial for design of EOR processes in organic-rich shale.

A custom-designed experimental apparatus was constructed to conduct flow tests. The apparatus is capable of maintaining core samples at reservoir pressure, temperature, and confining stress. In addition, a new mathematical model was formulated to simulate flow into the core as a porous medium rather than as a molecule-selective membrane. This new model is based on the following principles: (1) the solvent (low-salinity water) selectively enters the pores by diffusion mass transport and (2) the dissolved salt molecules (which are ionized) are restrained by internal electrostatic forces from diffusing in the opposite direction of the low-salinity brine molecules entering the pore network.

The mathematical model closely matches the experimental results and, more importantly, only very few assumptions were made in matching experiments. For instance, the critical model input data, such as permeability, porosity, and rock compressibility, were obtained from flow experiments on twin cores, and the diffusion coefficient was chosen by history matching. The strengths of the numerical simulation include the following: (1) the mathematical model is based on the mass transport fundamental principles, (2) the model does not require the use of the ambiguously defined membrane efficiency term, and (3) the chemical potential gradient is the reason for the low-salinity brine entering the high-salinity brine cores to generate osmotic pressure within the cores. The latter implies that osmotic pressure is the consequence of water entering the cores, not the cause.



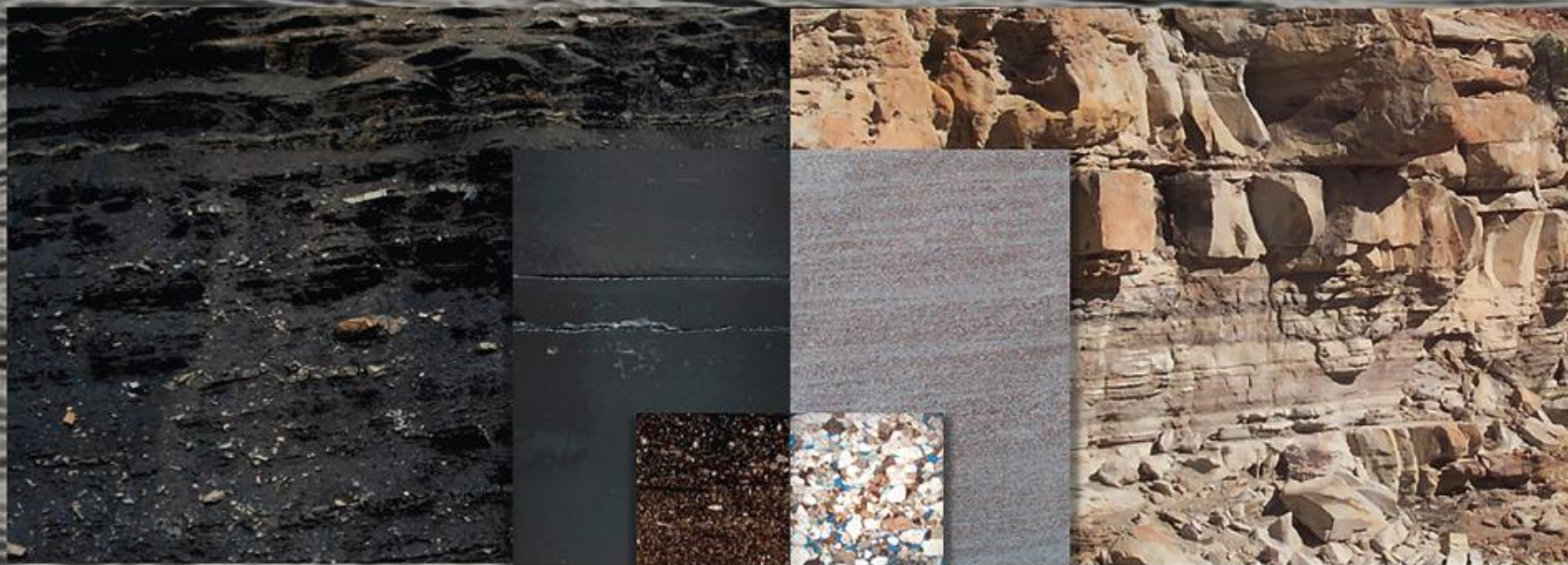
# AAPG

Latin America & Caribbean Region

## ARGENTINA 2016

Geosciences Technology Workshop

Co-hosted by the Argentine Association of Petroleum Geologists and Geophysicists



## Moving toward the Prediction of Unconventional Plays:

### Lessons Learned from Tight and Shale Reservoirs in the Neuquén Basin



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# Experimental and Theoretical Study of Water and Solute Transport Mechanisms in Organic -Rich Carbonate Mudrocks

Anton Padin, PhD

Colorado School of Mines

## Objective

- ❑ Determine the physicochemical processes underlying **water and solute transport** in organic-rich **Eagle Ford and Vaca Muerta** source rock samples
- ❑ Conduct coupled flow/geomechanical experiments on preserved Eagle Ford shale samples using a **novel high pressure triaxial assembly**
- ❑ Include **reservoir conditions**: pressure, temperature and effective stress
- ❑ Conduct **transport modeling** to match experiments

## Impact

- ❑ Use research findings in design of hydraulic fracturing & EOR

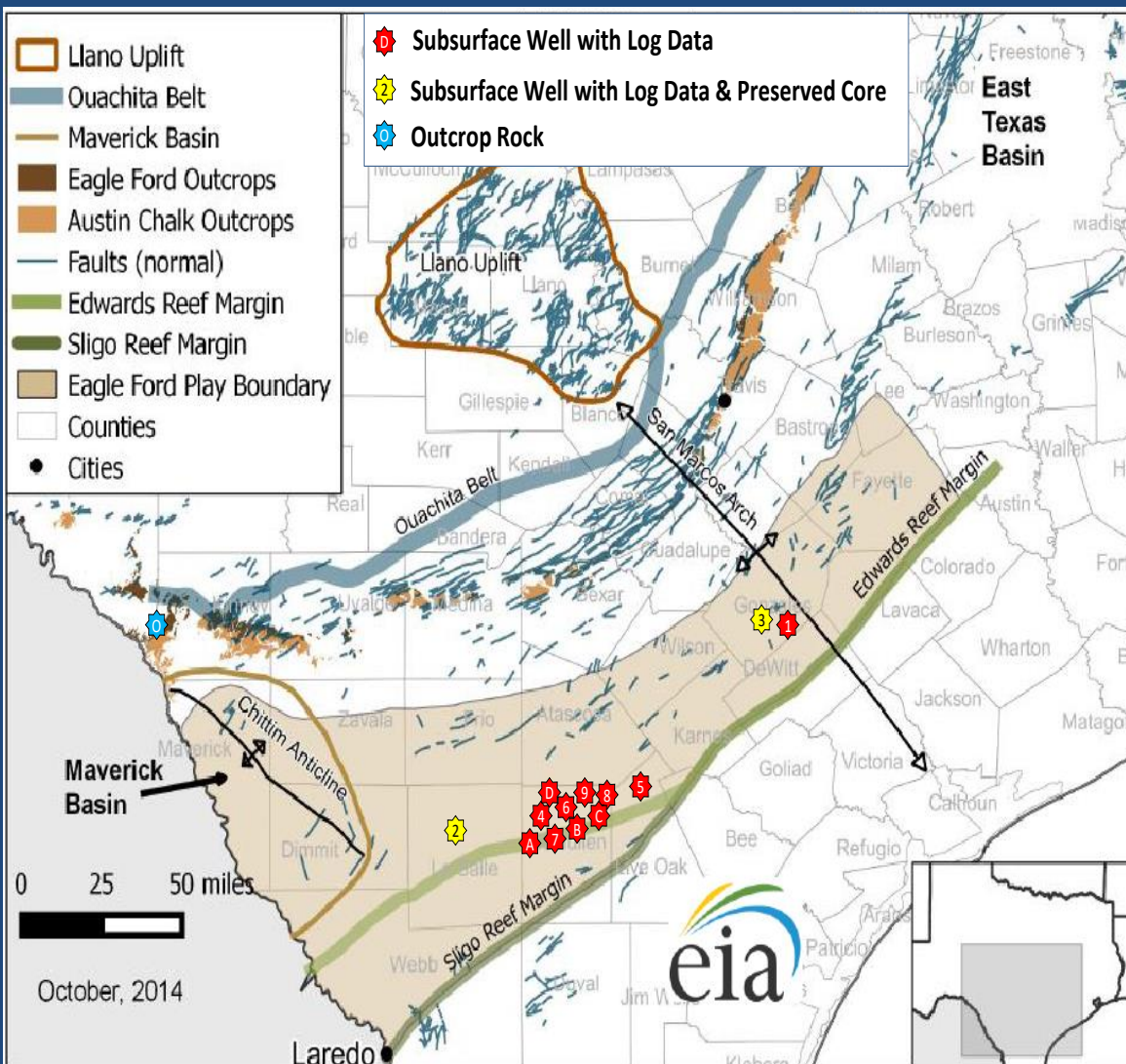


## Observations from Surveillance of Flowback Water after HF

- ❑ Improved production rates after long periods of shut-in
- ❑ Variable flowback-water recovery
- ❑ Time-dependent, gradual increase in flowback water salinity ( $\text{Na}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{K}^+$ ,  $\text{Fe}$ ,  $\text{Sr}^{2+}$  or  $\text{Ba}^{2+}$ )

## Observations from EOR Field Studies

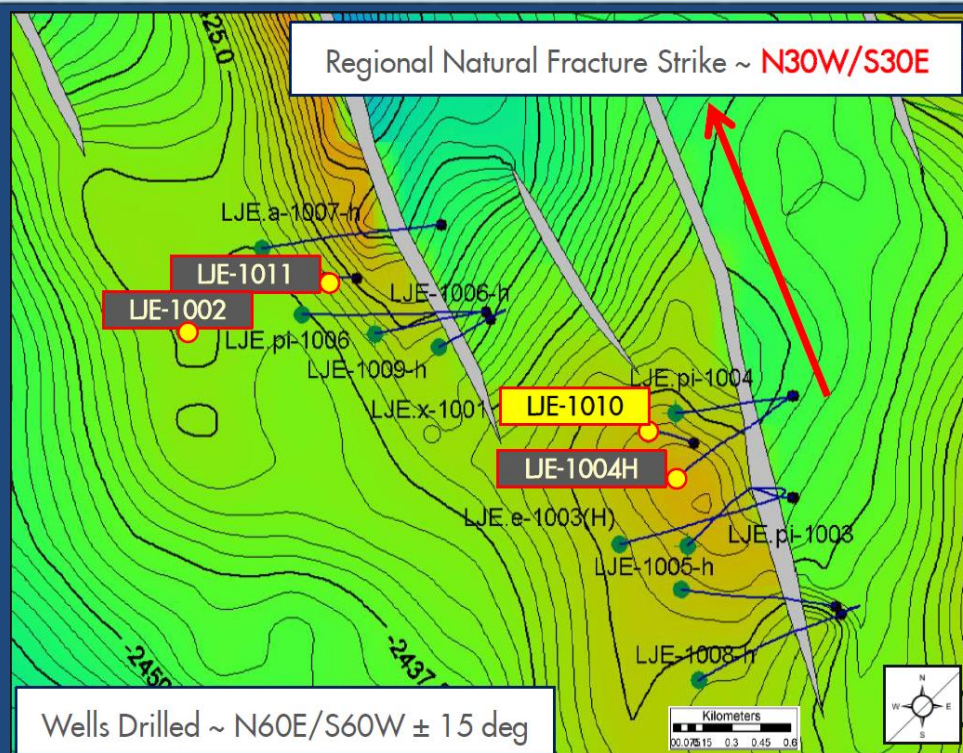
- ❑ Improved oil recovery by: Pressure/temperature increase and salinity decrease
- ❑ Attributed to wettability changes:
  - ❑ Similar to alkaline flooding – interfacial tension reduced
  - ❑ Increased repulsion forces, towards more water-wet



## Source Rock I: Upper Eagle Ford Marl

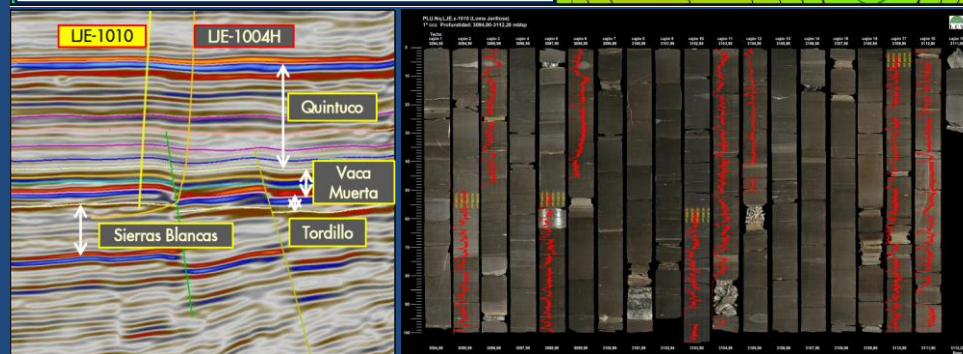
- Upper Cretaceous
- Isolated carbonate platform surrounded by siliciclastics
- Deposited during a sea level transgression.





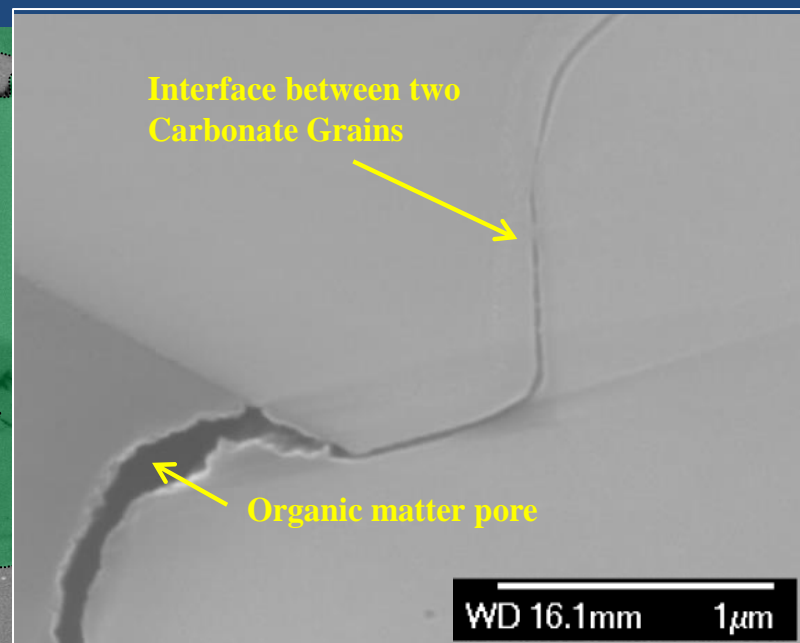
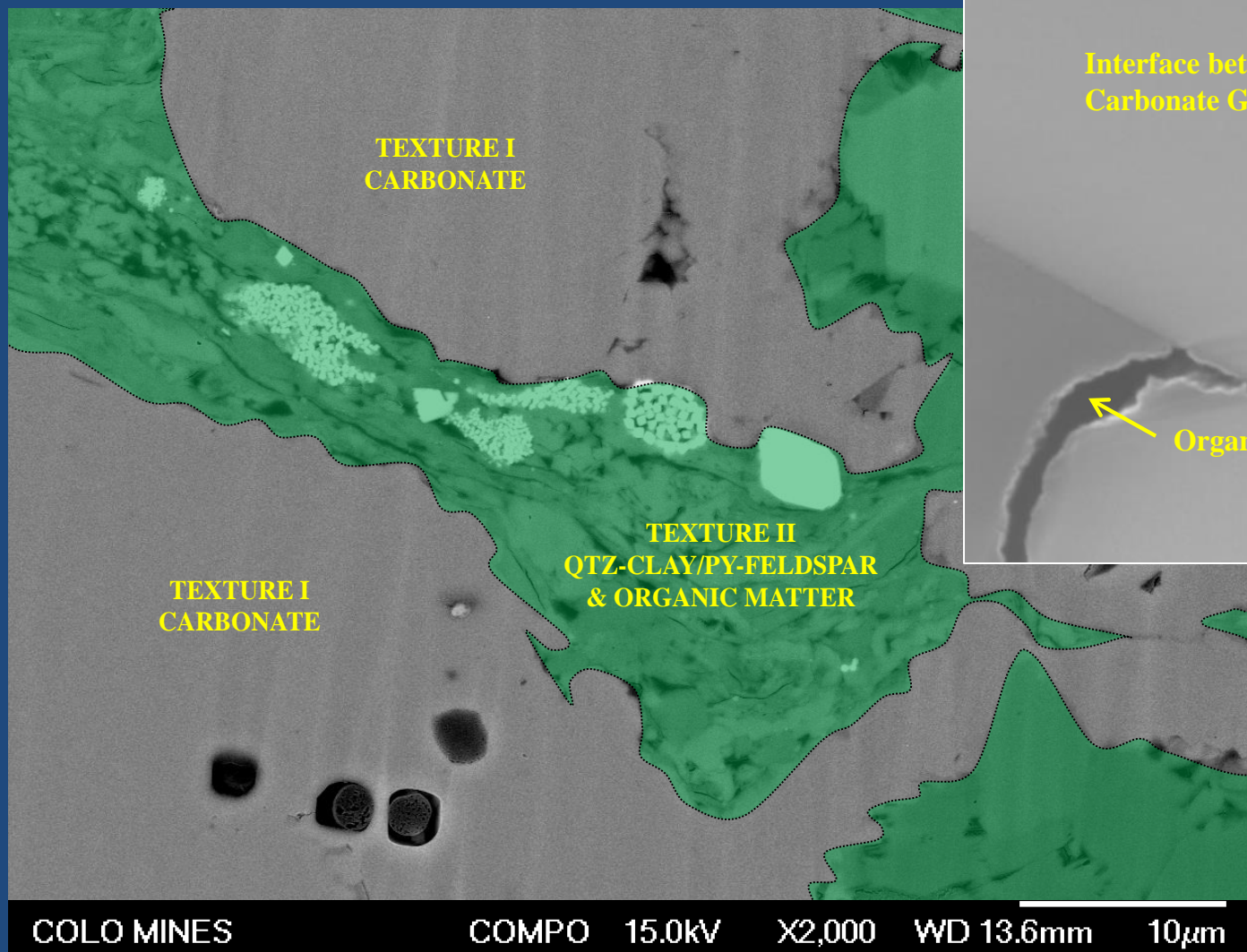
## Source Rock II: Vaca Muerta Marl

- ❑ Marine, black to dark brown organic-rich mudstone
- ❑ High contents of TOC, hydrogen index and anomalous concentrations of molybdenum, vanadium, nickel and chromium
- ❑ Core from the lower Vaca Muerta, well LJE-1010





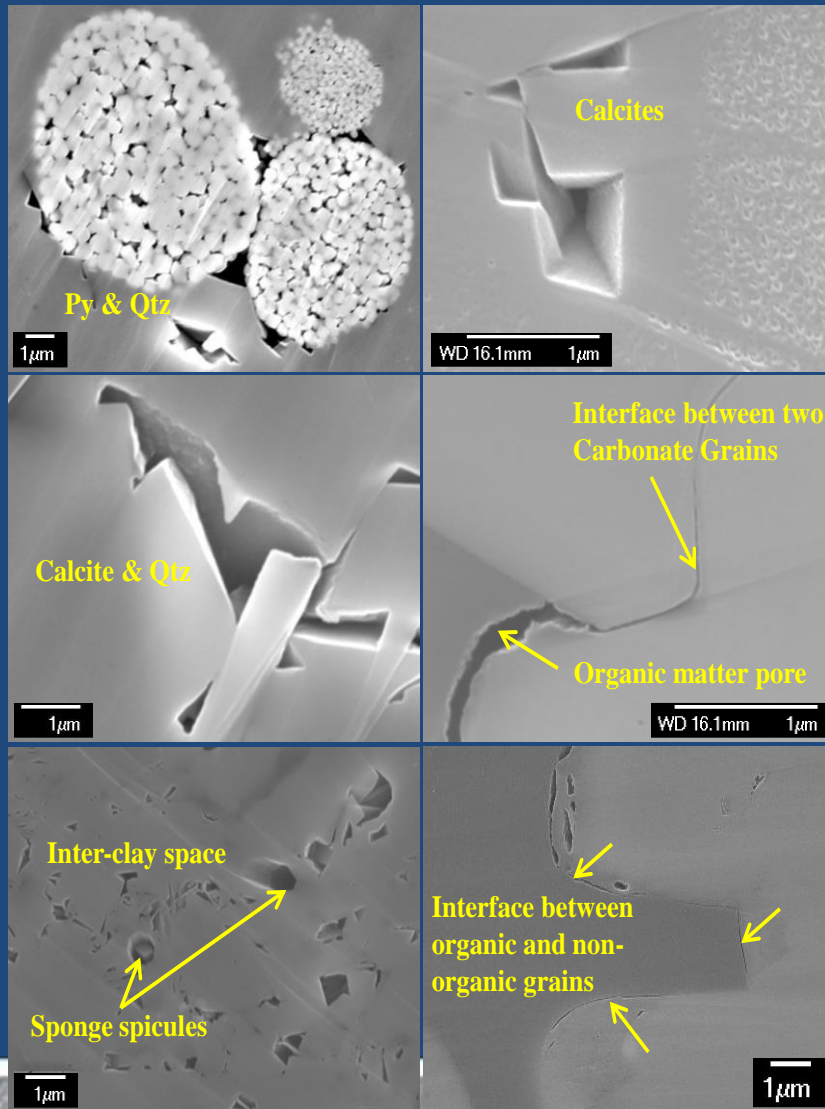
## Sample Core: Texture Interface and Microfractures



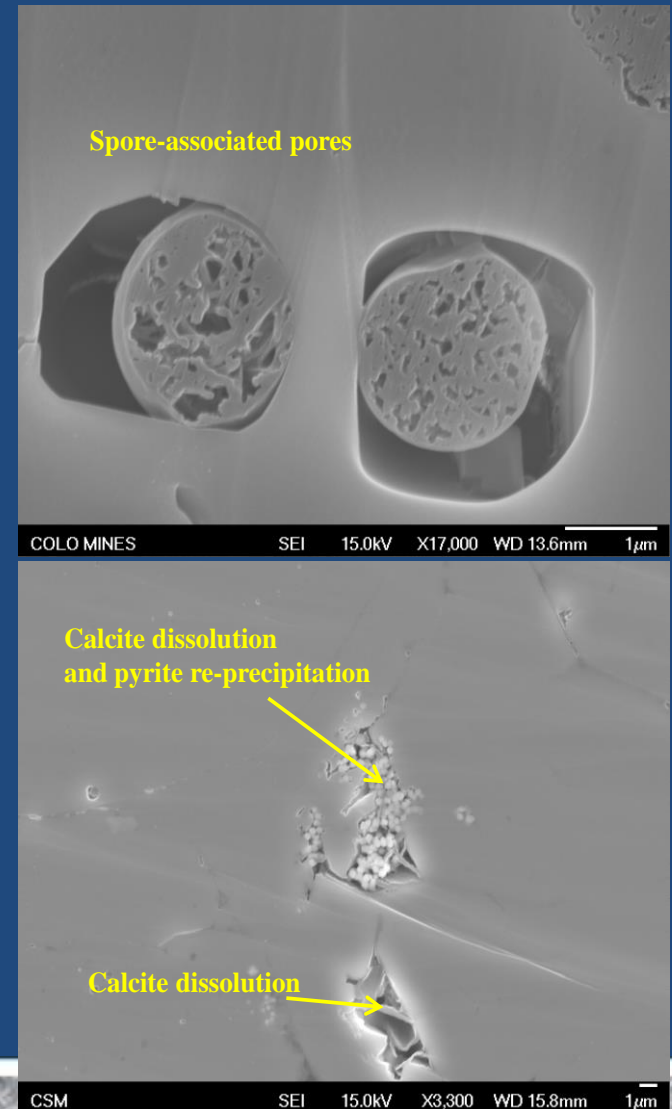


# Inorganic Pore Types

## Interparticle Pores

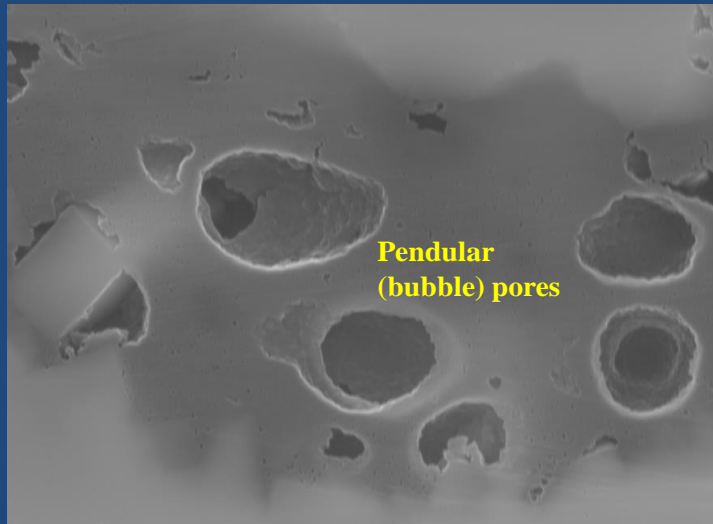


## Intraparticle Pores

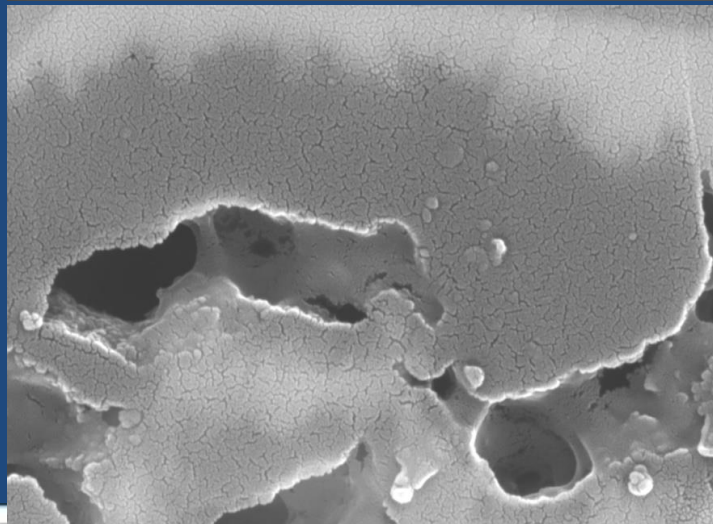


# Organic Pore Types

## Pendular (Bubble) Pores

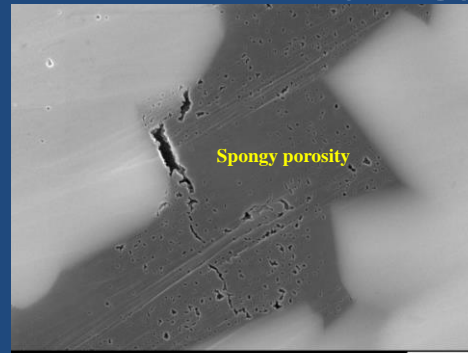


COLO MINES 3 SEM SEI 15.0kV X17,000 WD 17.1mm 1µm

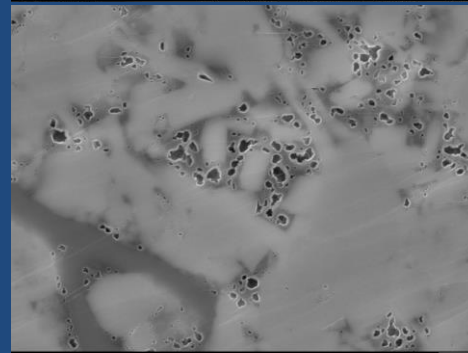


COLO MINES 3 SEM SEI 15.0kV X40,000 WD 7.5mm 100nm

## Spongy Porosity



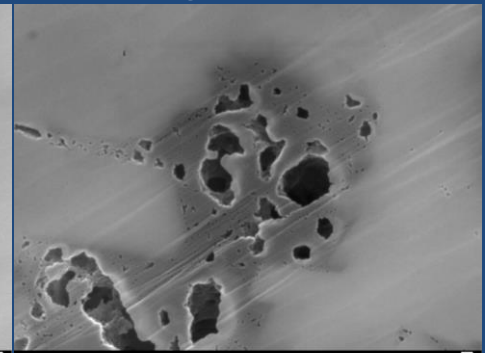
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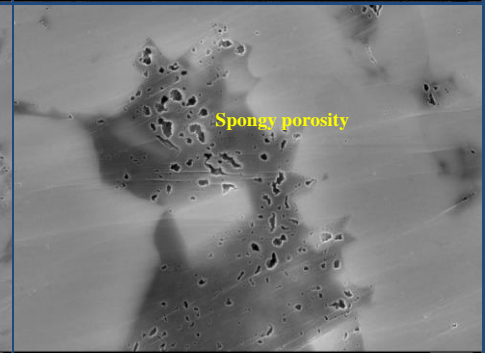
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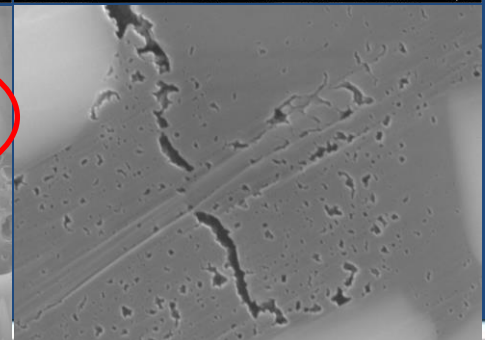
COLO MINES 3 SEM SEI 15.0kV X5,000 WD 16.2mm 1µm



COLO MINES SEI 15.0kV X30,000 WD 18.0mm 100nm

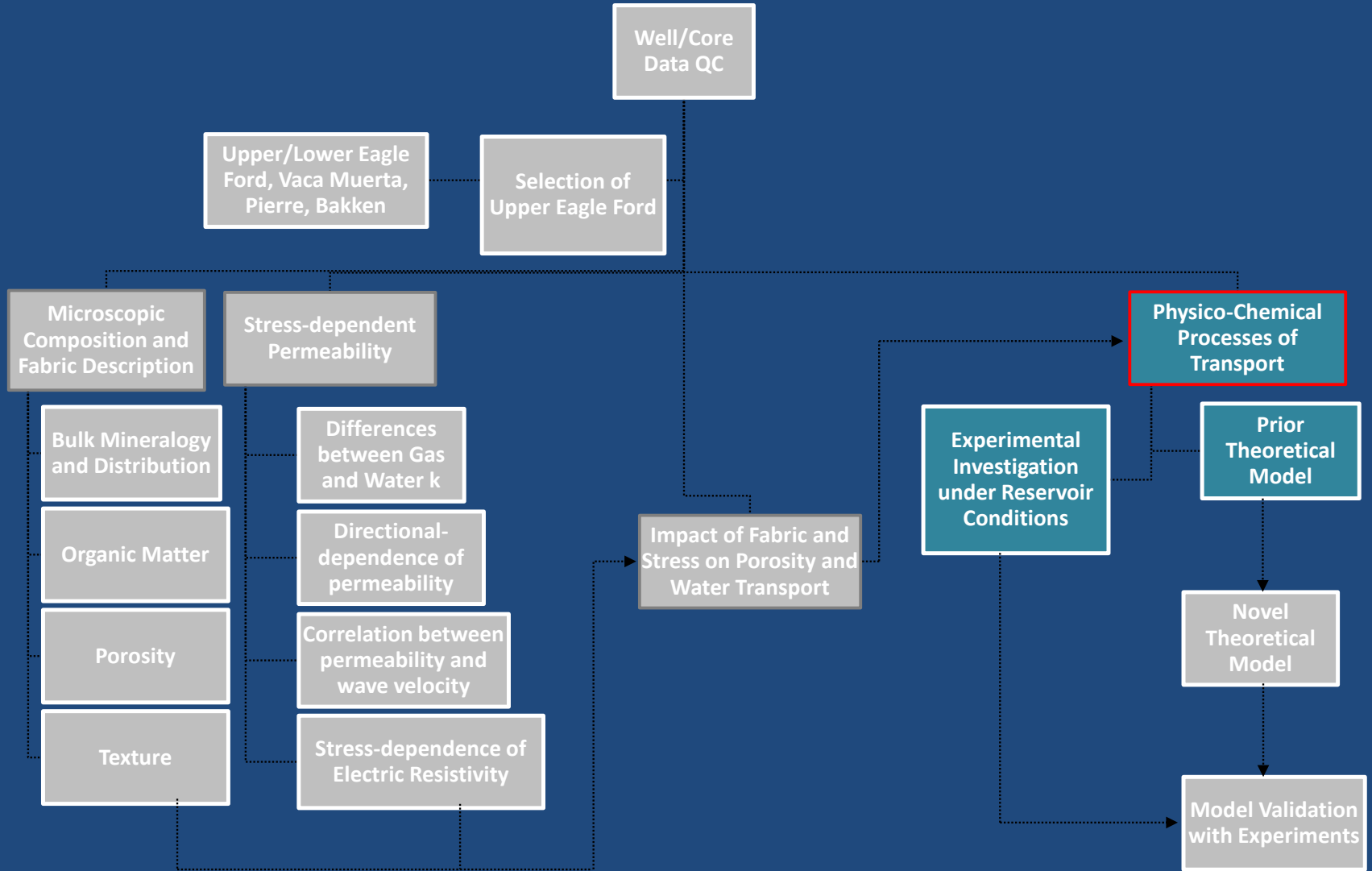


COLO MINES SEI 15.0kV X11,000 WD 18.0mm 1µm



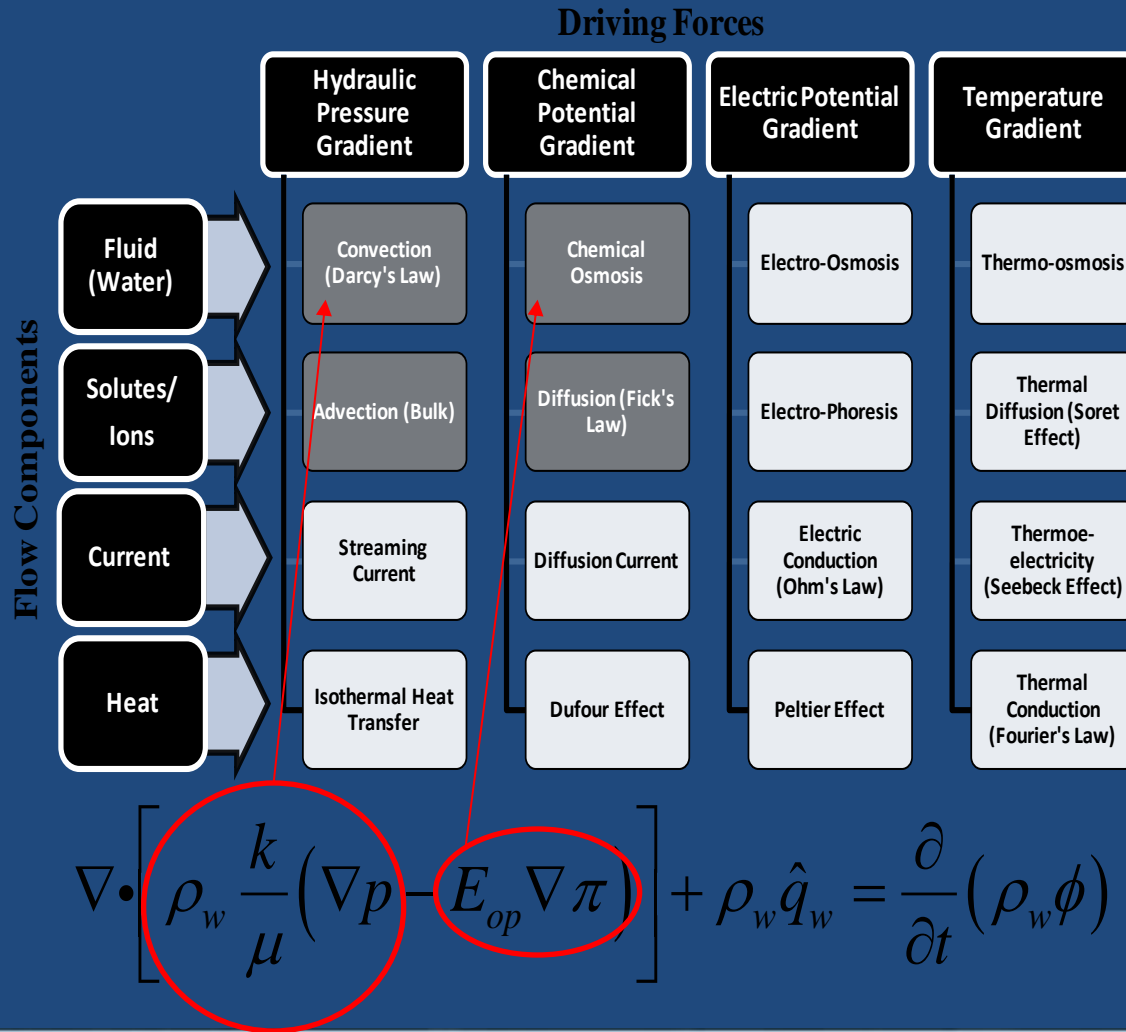
COLO MINES SEI 15.0kV X33,000 WD 18.0mm 100nm

# Experiments on Solute/Water Transport in Mudrocks





# Transport Laws in Mudrocks



□  $E_{op}$  empirical scaling factor termed *membrane efficiency*

- Defines the selectivity of membrane to specific ions
- Not-well-defined physical entity

$$E_{op} = 1 - \frac{a_{solute}}{a_{water}}$$

- $E_{op}$  depends on the ion type:  
KCl < NaCl < CaCl<sub>2</sub> < MgCl<sub>2</sub>
- $E_{op} = 0$  if  $k > 0.2$  nD

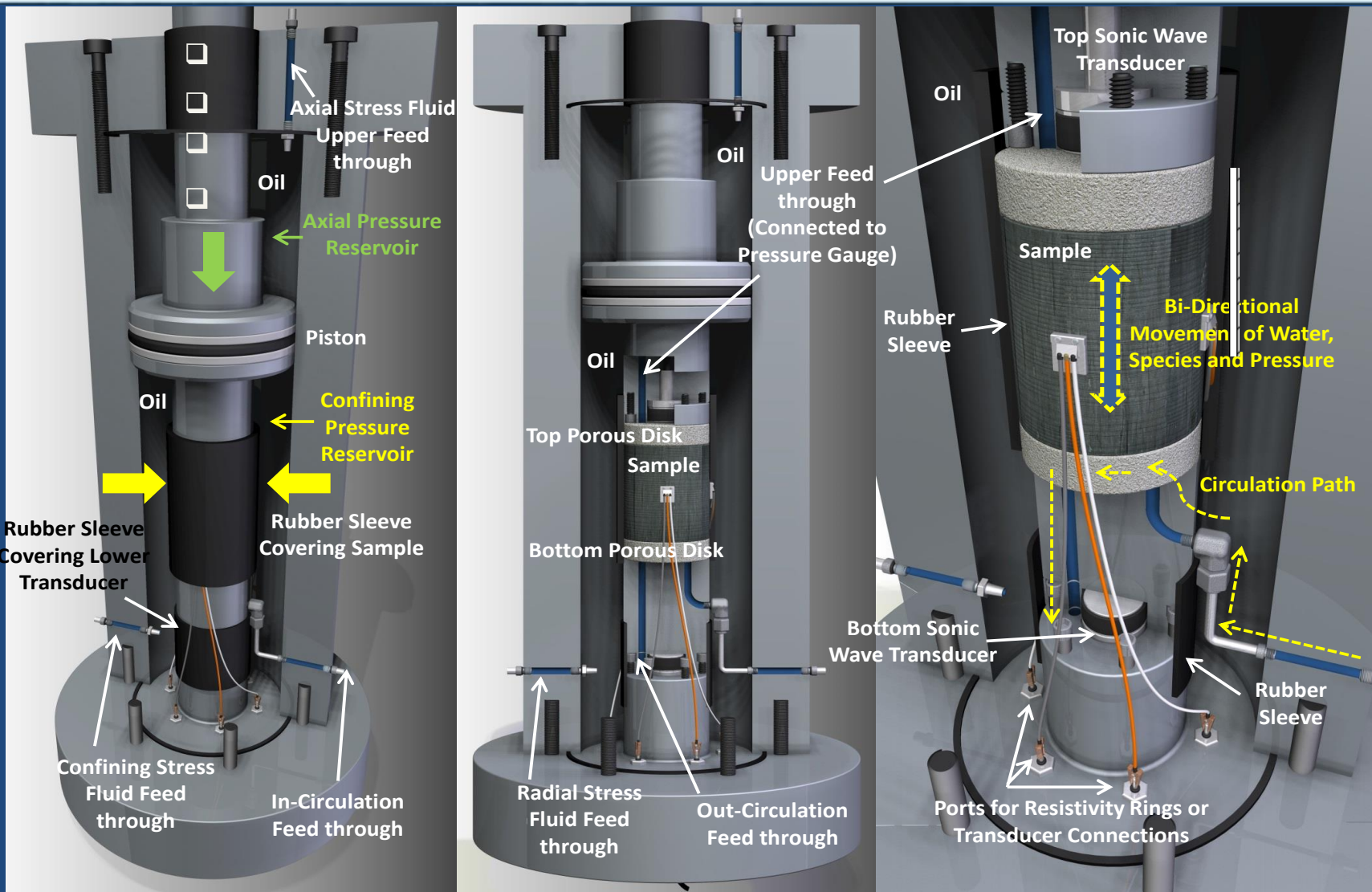
## Gaps from prior research in surface-fluid interaction

- ❑ Most research focused on: clay-rich, non-organic, seal shales
- ❑ In seal shales – interactions clay surface-water-solute are dominant
- ❑ No reservoir conditions (P,T) in experiments

## Our set of tests

- ❑ Conducted at reservoir conditions (6,000 psi conf., 4,000 psi Pp)
- ❑ Studied impact of solute type (monovalent, Na<sup>+</sup> and K<sup>+</sup>, and divalent, Ca<sup>2+</sup>) on surface-fluid interaction
- ❑ Impact of initial saturation, effective stress and solute concentration

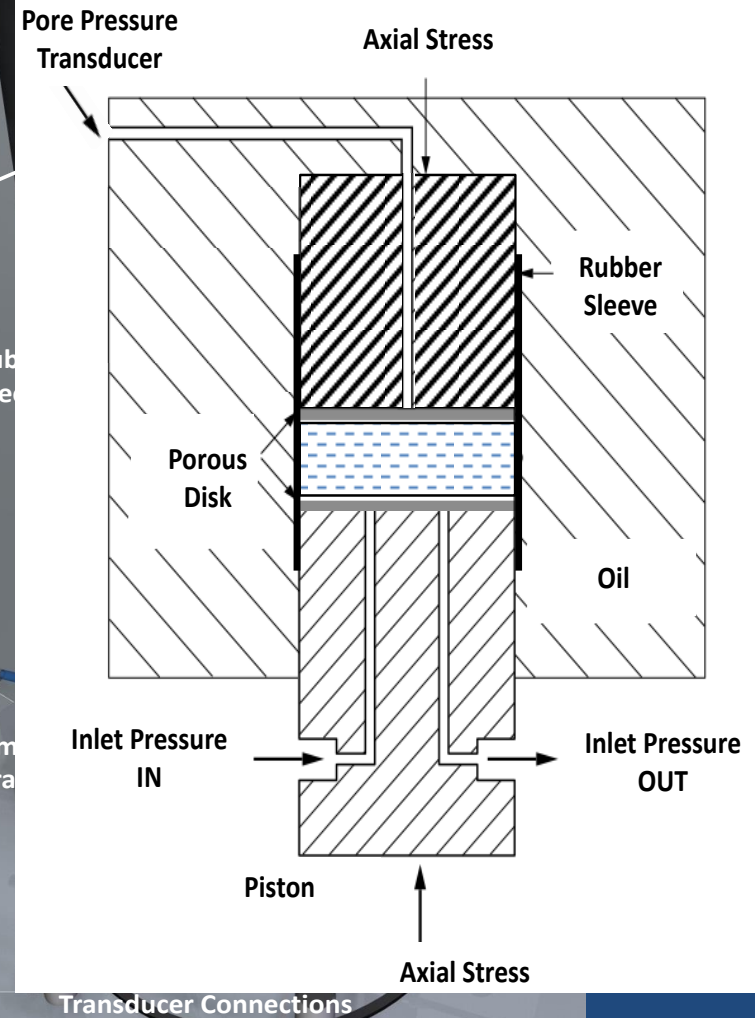
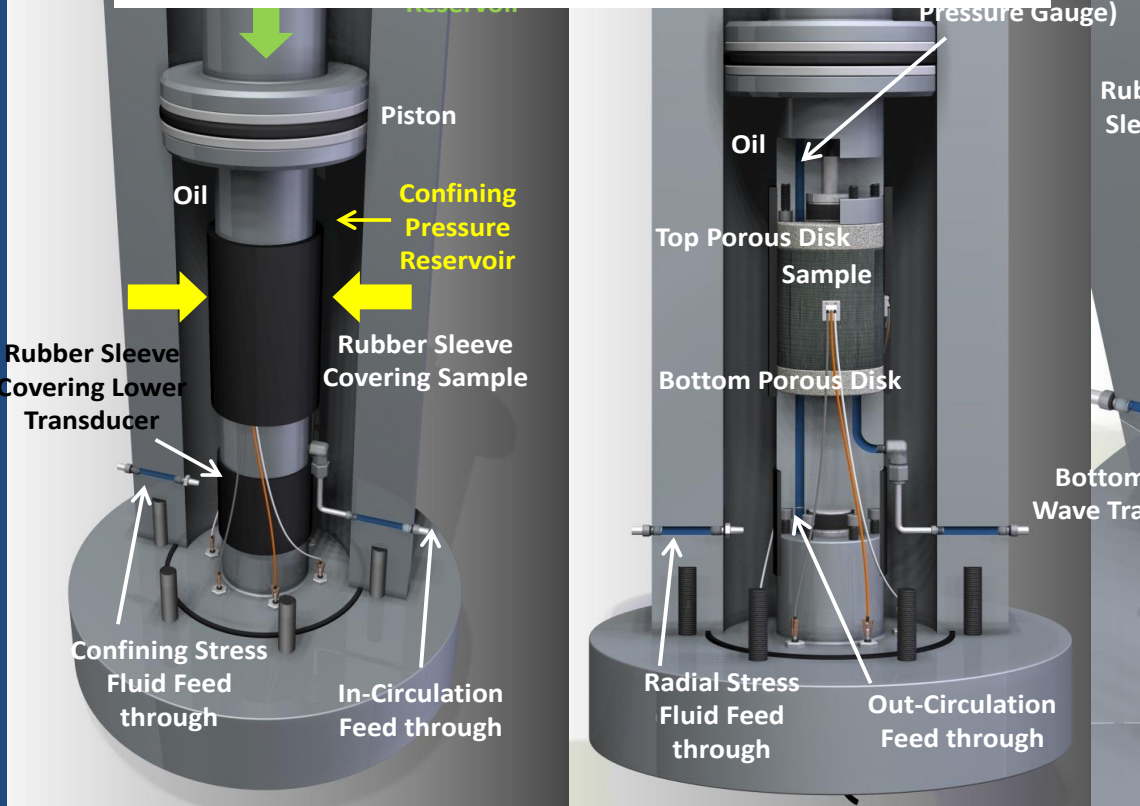
## Permeability-Osmosis Apparatus – Reservoir Conditions



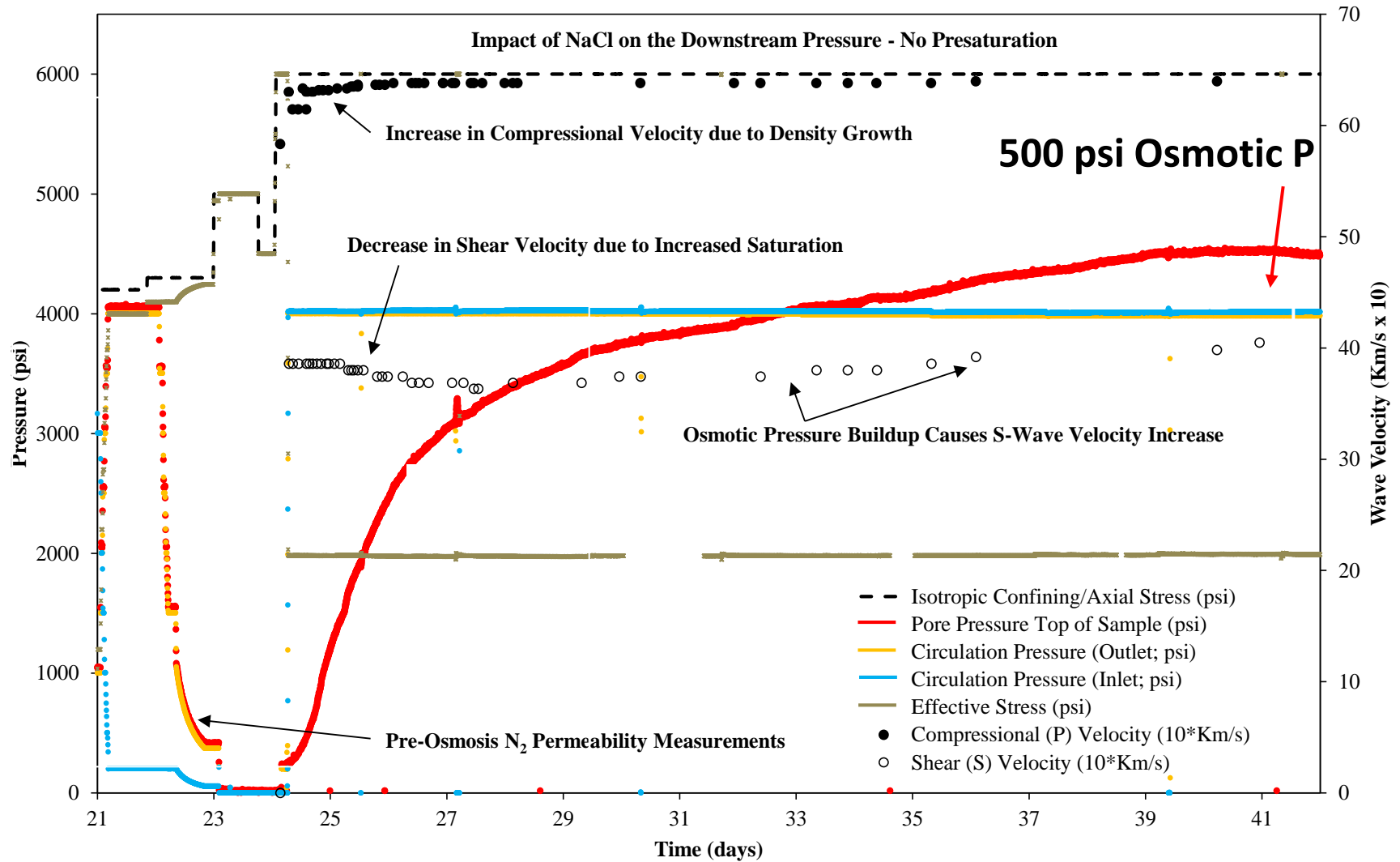


## Permeability-Osmosis Apparatus – Reservoir Conditions

- Pore Pressure (10,000 psi max.)
- Temperature ( $40^{\circ}\text{C} \pm 0.3^{\circ}\text{C}$ )
- P and S wave velocities (1 MHz)
- Displacement, Stress and Resistivity



## Impact of Solute Type - NaCl 1,000 ppm



## Impact of Solute Type - NaCl 1,000 ppm

4,500 psi

Pore Pressure Transducer

Axial Stress

Rubber Sleeve

Porous Disk

Oil

Inlet Pressure IN

Inlet Pressure OUT

Piston

Axial Stress

4,000 psi

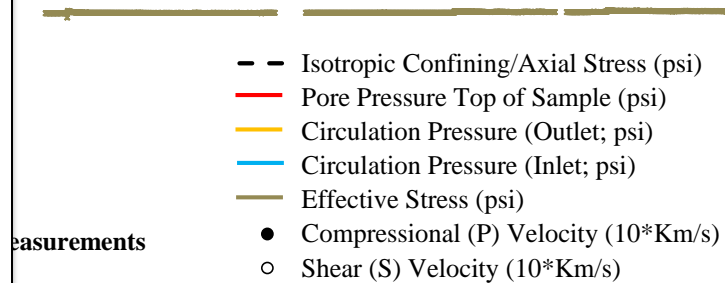
Downstream Pressure - No Presaturation

ity due to Density Growth

500 psi Osmotic P

Increased Saturation

Osmotic Pressure Buildup Causes S-Wave Velocity Increase

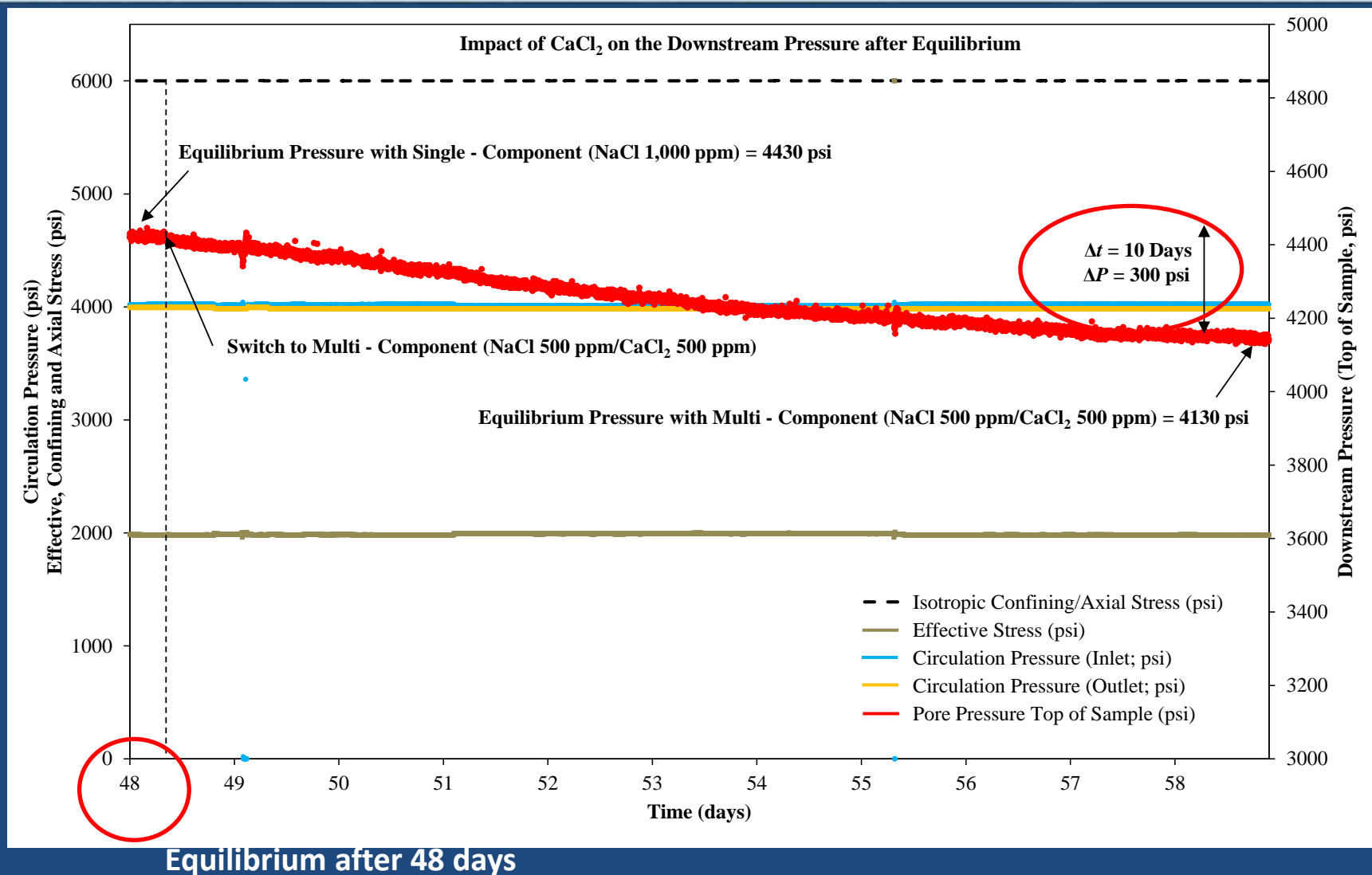


Measurements

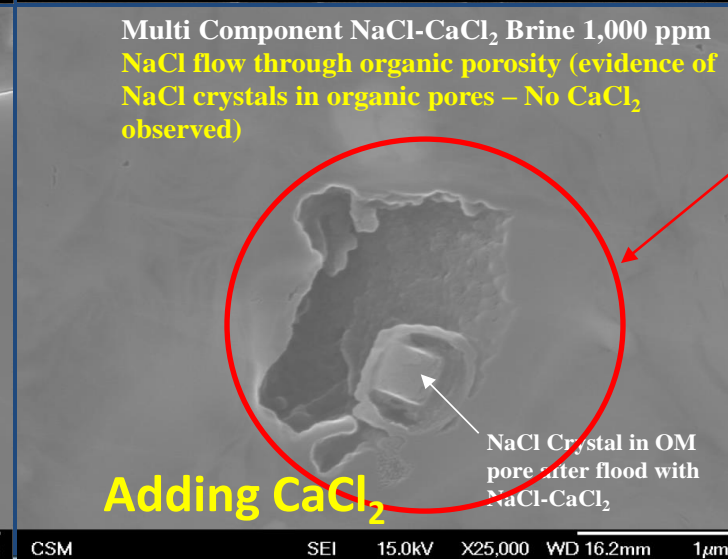
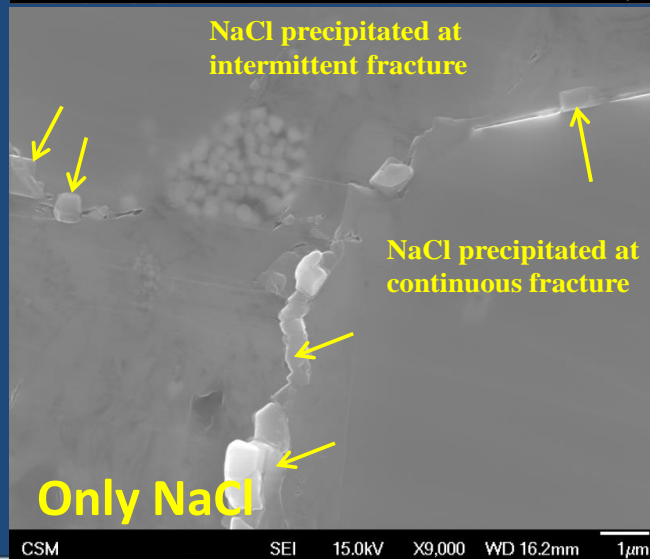
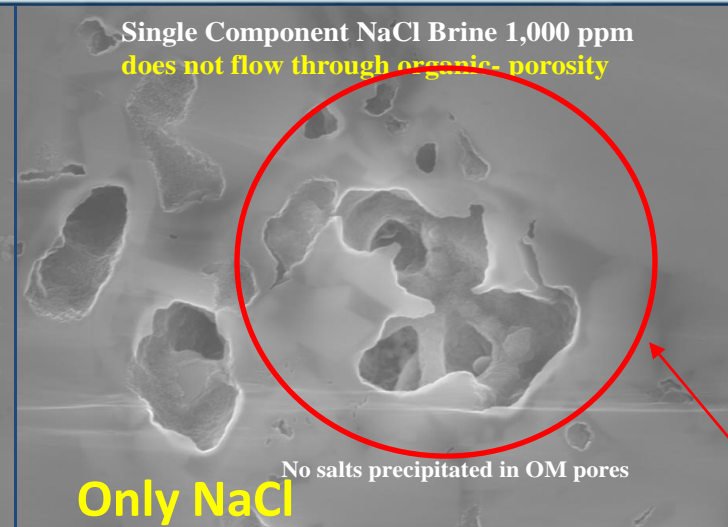
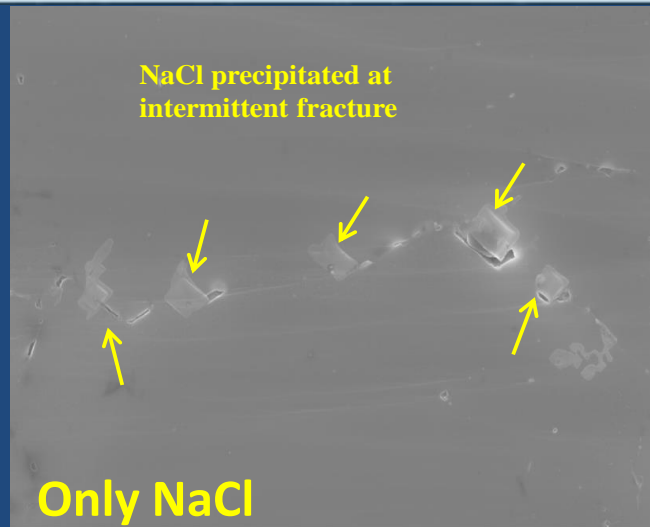
Time (days)



## Impact of Solute Type – Replacing low salinity NaCl by CaCl<sub>2</sub>

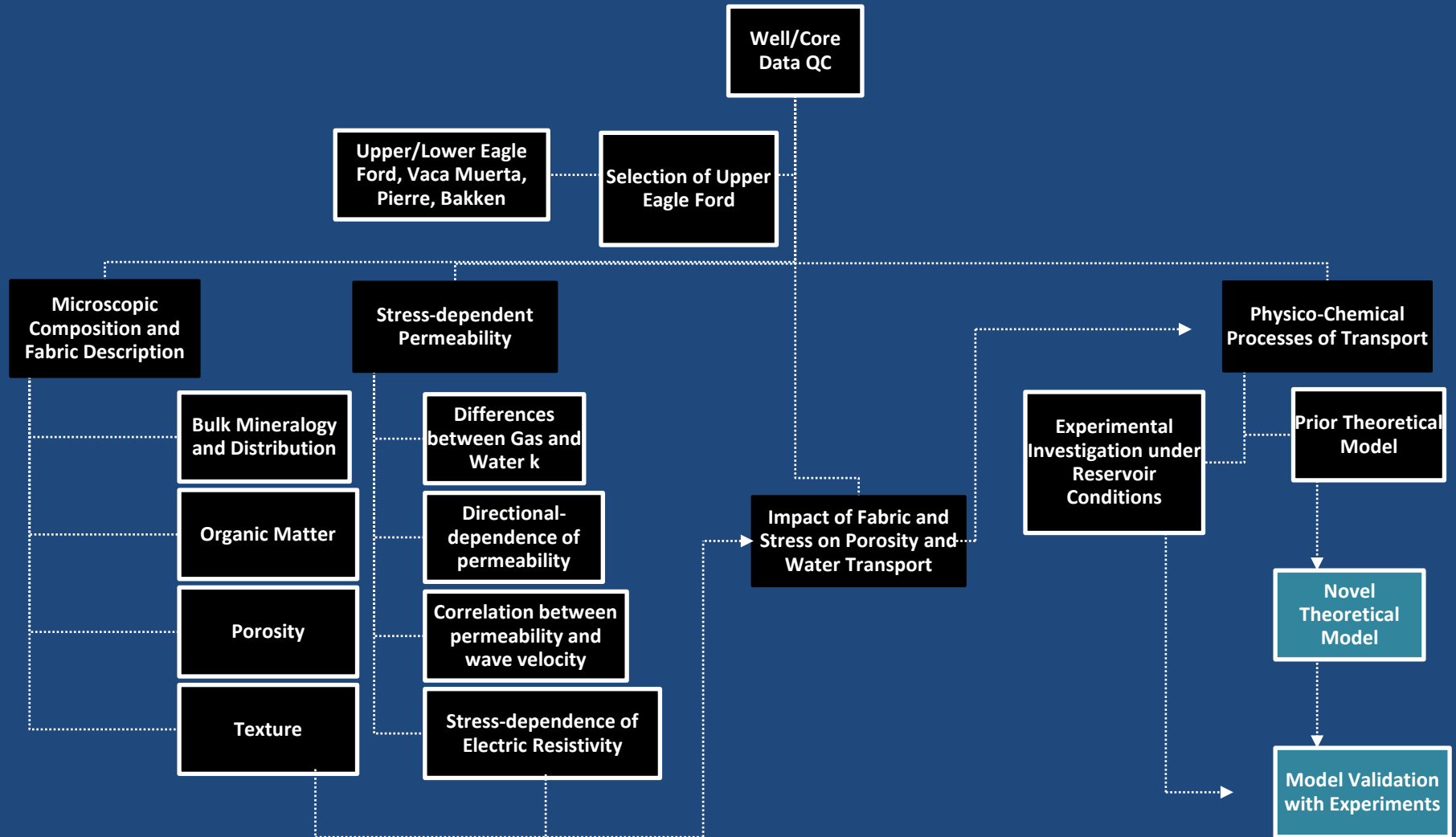


# When we add $\text{CaCl}_2$ , $\text{NaCl}$ diffuses through organic porosity



Vs.

# Novel Conceptual Approach to Transport Mechanisms



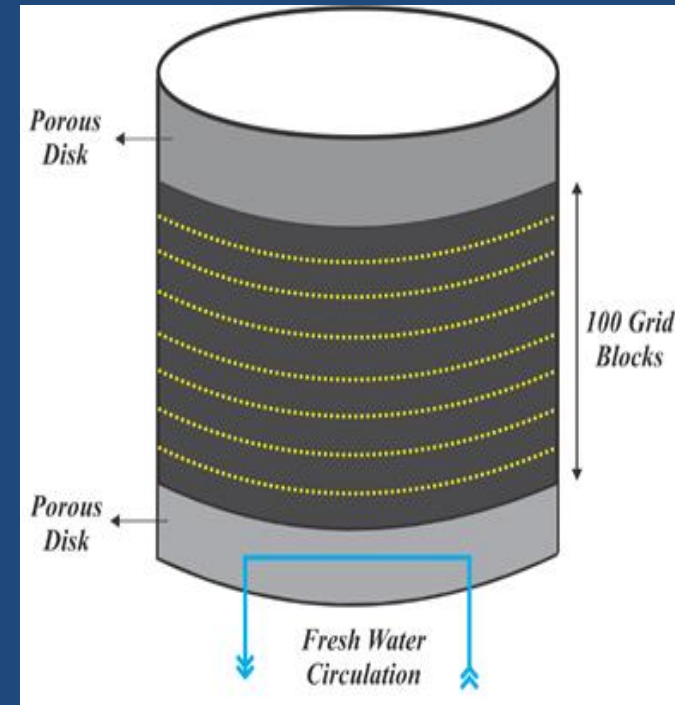


## Existing Mathematical Model has Critical Limitations

- ❑ Rock assumed a semi-permeable membrane, but thickness much larger than a membrane
- ❑ Osmotic pressure considered the imbibing force

## We treat porous media as nano-tubes rather than a membrane

- ❑ **Osmotic pressure** is the **consequence** of the selective molecular transport by the solvent, **not the imbibing force**
- ❑ Only H<sub>2</sub>O allowed to enter the pore space
- ❑ Salt molecules are restrained by internal forces to move against water molecule flow
- ❑ Water and solvent flow inside core both by advective flow and molecular diffusion



## Fundamental equations:

### □ Component 1 (solute)

$$\frac{\partial}{\partial x} \left[ \rho D_{1,2}^{eff} \frac{\partial C_1}{\partial x} + \rho C_1 \frac{k}{\mu} \frac{\partial p}{\partial x} \right] = \frac{\partial}{\partial t} (\phi \rho C_1)$$

*Solute diffusion*

*Bulk solute advection*

□ System of three equations with three primary variables

□ Solved for pore pressure  $p$ , water and solute concentrations ( $C_2$  and  $C_1$ )

### □ Component 2 (water)

$$\frac{\partial}{\partial x} \left[ \rho D_{2,1}^{eff} \frac{\partial C_2}{\partial x} + \rho C_2 \frac{k}{\mu} \frac{\partial p}{\partial x} \right] + \left\{ \begin{array}{l} \left[ \frac{\rho D_{eff} (C_2^* - C_{2,1})}{(\Delta x)^2} \right] \delta(x - x_1) \\ - \left[ \frac{\rho \frac{k}{\mu} C_2 (p_1^{n+1} - p_{in}^*)}{(\Delta x)^2} \right] \delta(x - x_1) \end{array} \right\} = \frac{\partial}{\partial t} (\phi \rho C_2)$$

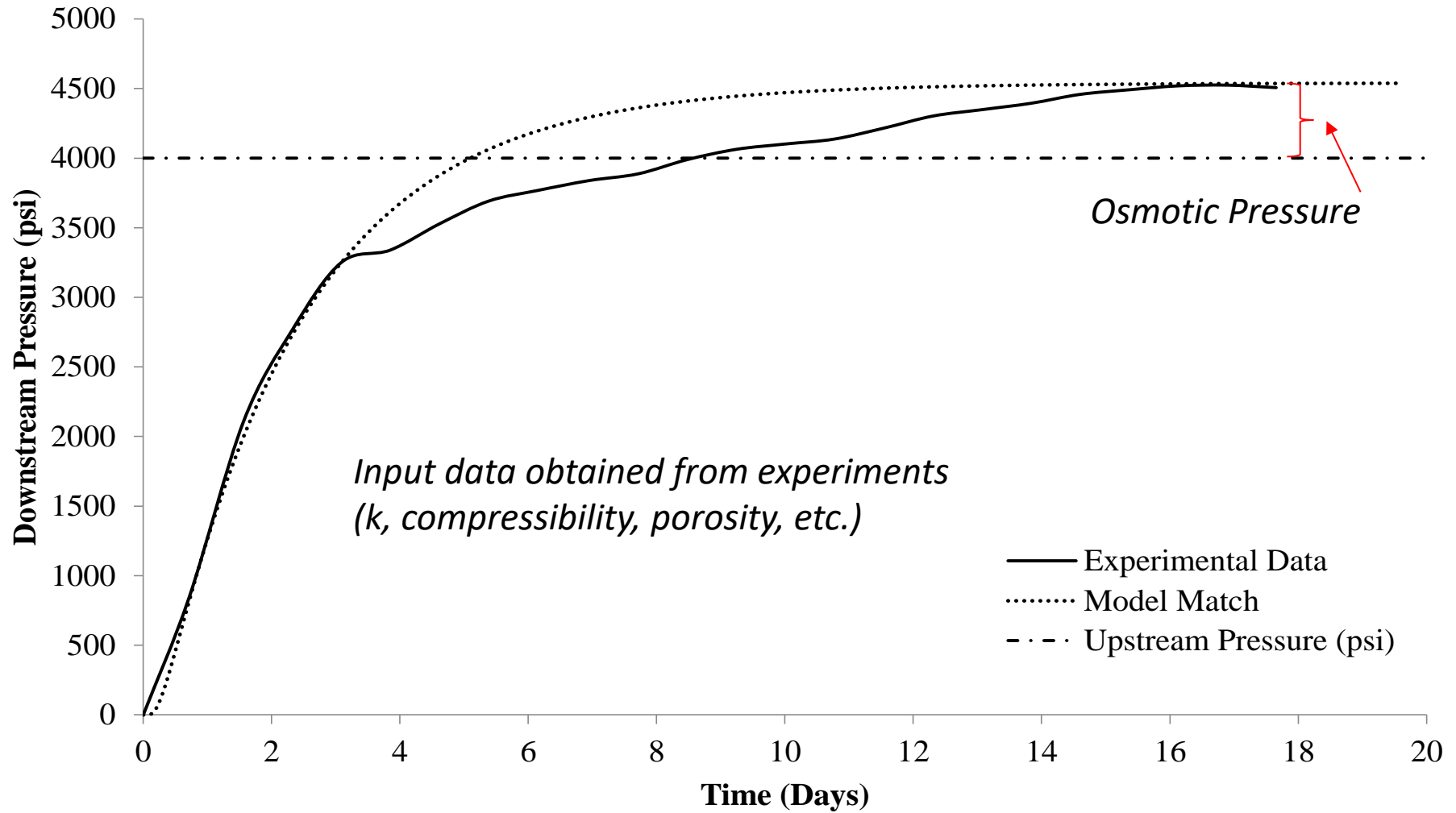
*Water diffusion due to chemical osmosis*

*Water advection*

*Boundary conditions*

$$C_1 + C_2 = 1$$

## Model vs. Experimental Data for NaCl 1,000 ppm Circulation





## Advantages over Prior Models

- ❑ Simpler formulation based on transport phenomena
- ❑ No empirical scaling factor
- ❑ Water imbibes because of selective molecular transport by the solvent
- ❑ No thermodynamic **activity** is needed for transport equations
- ❑ Diffusion coefficient is a more fundamental parameter than membrane efficiency
- ❑ Impact of ions other than  $\text{Na}^+$  and  $\text{Cl}^-$  can be modeled using additional components

## Limitations

- ❑ Not capturing electro-osmosis (important for high (>50%)-clay content shales)
- ❑ Not capturing impact of organic-matter surface forces