Hierarchical Evaluation of Geologic Carbon Storage Resource Estimates: Cambrian-Ordovician Units within the MRCSP Region*

Cristian R. Medina¹, John A. Rupp², Kevin Ellett², David A. Barnes³, Matthew J. Rine³, Matthew S. Erenpreiss⁴, and Stephen F. Greb⁵

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Abstract

The Midwest Regional Carbon Sequestration Partnership (MRCSP) aims to study the regional distribution and geologic storage suitability of units within the Cambrian-Ordovician sequences, including the Knox Supergroup, St. Peter Sandstone, Trenton and Lexington Limestones, and equivalent units across the MRCSP region.

To date, we have compiled a comprehensive data set of wireline logs and petrophysical information that include core analysis for porosity and permeability and mercury injection capillary pressure (MICP) analyses. Using these data, carbon storage resource estimates (SRE) are evaluated using a hierarchical approach that addresses uncertainty in the estimates by incorporating different models of formation porosity based on a series of increasingly complex portrayals of the pore system. The simplest analysis follows the USDOE methodology whereby a SRE is calculated using a single value for porosity in the assessed formation. Additional estimates follow the same general methodology but employ increasingly precise spatially variable porosity models based on formation diagenesis (depth-dependent function), reservoir suitability (effective porosity), distinct petrofacies (advanced reservoir characterization), and multiple realizations of porosity using data-driven geostatistical methods.

Results from this hierarchical approach help illuminate the magnitude of uncertainty that should be expected in SREs as a function of data availability and the level of reservoir characterization that is achievable for a given formation. A semi-probabilistic SRE calculation methodology using Monte Carlo simulations to create models for porosity generally tends to underestimate the range of uncertainty in storage resource. Conceivably, the higher the order model, the lower the uncertainty in the SRE. Ongoing research is investigating whether improved precision implicit in higher orders of the hierarchy are generating more accurate estimates of storage volumes.

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Selected References

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Outline

- Purpose
- Midwest Regional Carbon Sequestration Partnership (MRCSP)
- Stratigraphy
- Reservoir characterization
- Methods
- Results
- Conclusions

Purpose

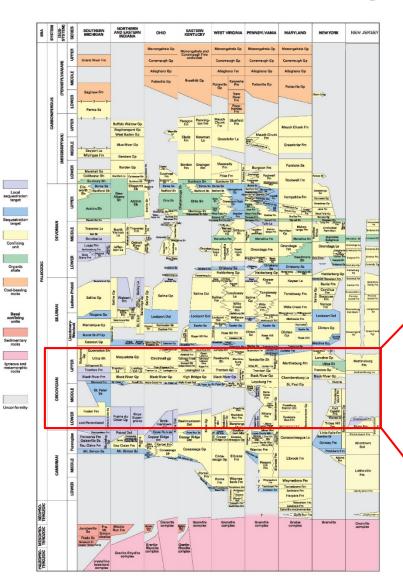
- To evaluate the CO₂ storage potential in saline aquifers of Cambrian-Ordovician strata underlying portions of the MRCSP states
- To explore the use of five different methodologies to independently generate storage resource estimates (SRE)
 - The methods differ fundamentally in how they estimate values for porosity (Ø)
- To compare the various results and assess how each of the different methods yield SREs with various magnitudes and explore the reasons for "inter-method" variability

Midwest Regional Carbon Sequestration partnership (MRCSP)



- One of the seven partnerships in US and Canada
- 10 states
- This work focuses on saline aquifers in Indiana, Michigan, Ohio, Kentucky, West Virginia, and Pennsylvania

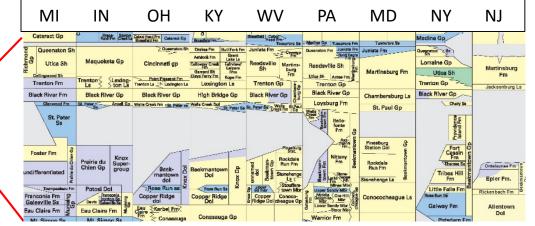
Stratigraphy / Units



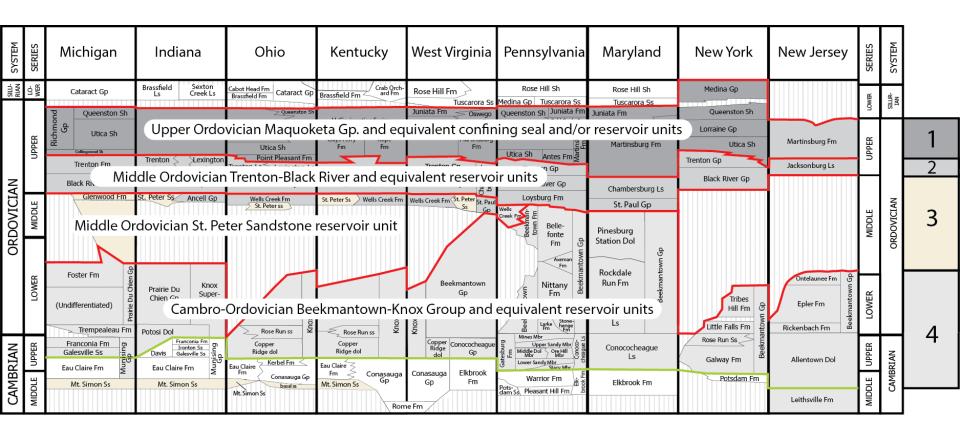
Seal vs. Reservoir (Knox Supergroup)



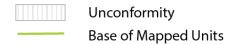




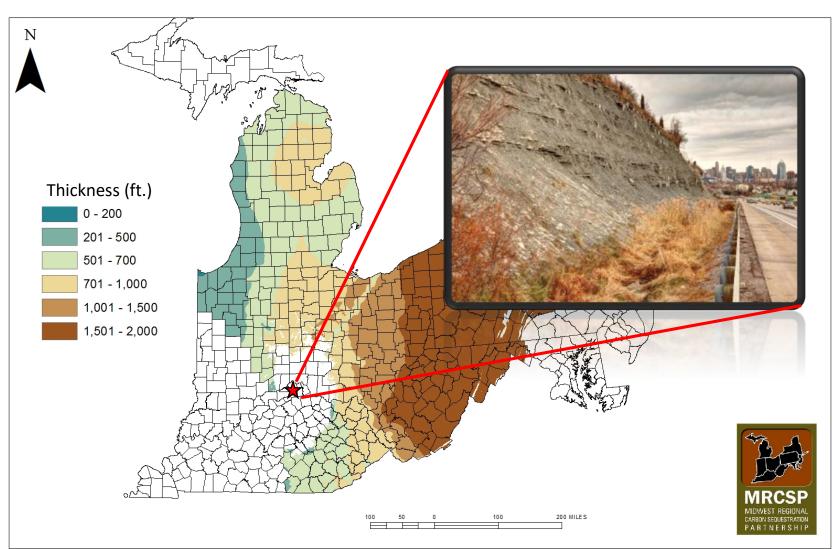
Stratigraphy / Units



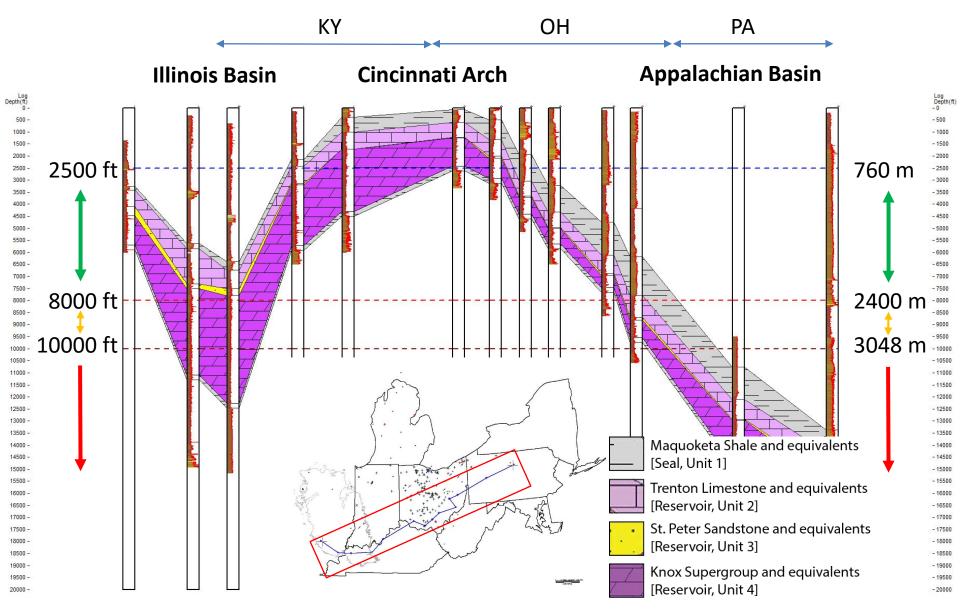
- 1 Upper Ordovician Maquoketa Gp. and equivalent confining seal and/or reservoir units
- 2 Middle Ordovician Trenton-Black River and equivalent reservoir units
- 3 Middle Ordovician St. Peter Sandstone reservoir unit
- 4 Cambro-Ordovician Beekmantown-Knox Group and equivalent reservoir units



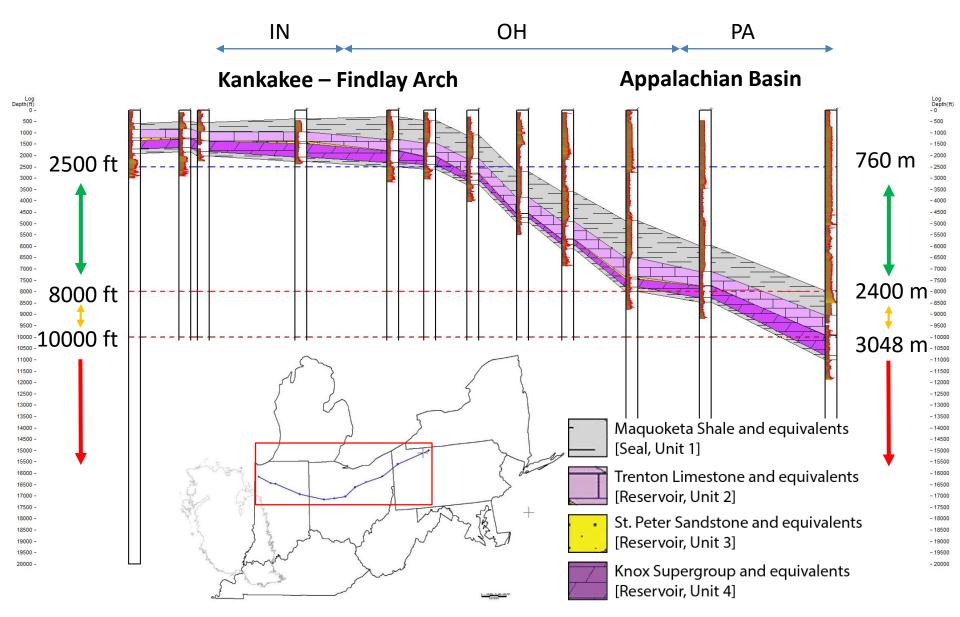
Isopach of Primary Reservoir Seal: Maquoketa Group and Equivalents



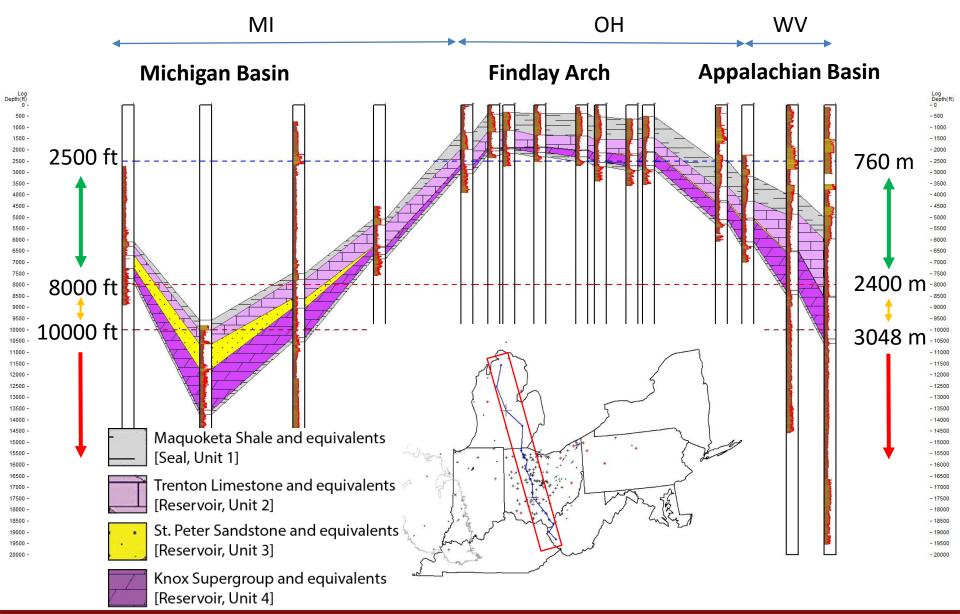
Cross Section I (SEE-NEE)



Cross Section II (W-E)



Cross Section III (N-S)



DOE Methodology

"The volumetric methods require the area of the target formation or horizon along with the formation's thickness and porosity..."

Source: DOE Carbon Storage Atlas, Fifth Edition (2015)

- Designed to be reconnaissance or highest level estimation of potential storage volumes
- Uses a single value for all basic parameters

Storage Resource Estimate (SRE):

 $SRE_{CO_2} = Area * Thickness * Porosity * Density_{CO_2} * E_{saline}$

Efficiency Factor

Employs an "efficiency factor" (E_{saline}) to account for the lack of accuracy caused by variability in factors

Efficiency factor uses "widely accepted assumptions about in-situ fluid distributions in porous formations and fluid displacement processes commonly applied in the petroleum and groundwater science fields"

In saline aquifers, because of the high degree of uncertainty in estimates (96 to 99 %), the resultant volumes are highly discounted (4 to 1% of the calculated values)

* However, when any of the factors in the basic volumetric equation are "enhanced" with more accurate, less uncertain data, the efficiency factors need to be modified (increased) to account for these changes.

$$SRE_{CO_2} = Area * Thickness * Porosity * Density_{CO_2} * E_{saline}$$

where

$$E_{\text{saline}} = E_{\text{An/At}} E_{\text{hn/hg}} E_{\phi e/\phi \text{tot}} E_{\text{v}} E_{\text{d}}$$

This Work's Methodology

Increasing in sophistication/complexity of porosity data

Method I	Method II	Method III	Method IV	Method V
Assumes average porosity in all units ($\phi = 10\%$)	Uses average porosity from core analysis	Uses porosity from wireline logs	Uses a diagenetic model that assumes an exponential	Uses MICP data on pore size distribution patterns to
Similar to DOE methodology		Logs used include neutron, sonic, and density	decrease of porosity as a function of depth	define 'petrofacies' models
Robust dataset	Limited data	Robust dataset	Robust dataset	Limited data

- To facilitate comparison of results among methods, the efficiency factor was held constant
- Results also reported in tonnes of CO₂ /km²
- Number of data points varies depending on methodology.

Method I

- Assumes average porosity in all units (φ_{tot}= 10%)
- Follows a volumetric equation (ie, methodology published in Atlas by DOE-NETL, 2010)

$$SRE_{CO_2} = A_t * h_g * \mathbf{0}_{tot} * \rho_{CO_2} * E_{saline}$$

$$SRE_{CO_2} = A_t * h_g * \mathbf{0.10} * 0.73 * [0.01, 0.04]$$

Where:

 A_t is the area of a given county h_g is the average thickness, in the county, of unit under assessment \emptyset_{tot} is the average porosity (10%) ρ_{CO_2} is CO_2 density at reservoir conditions (0.73 tonnes/ m^3) E_{saline} is the efficiency factor (1% and 4% used, respectively)

Method II

- Uses average porosity from core analysis (φ_{core})
- Follows volumetric equation (DOE-NETL, 2010)

$$SRE_{CO_2} = A_t * h_g * \mathbf{ore} * \rho_{CO_2} * E_{saline}$$

Where:

 A_t is the area of a given county h_g is the average thickness, in the county, of unit under assessment \emptyset_{core} is the average porosity from core analysis ρ_{CO_2} is CO_2 density at reservoir conditions (0.73 tonnes/ m^3) E_{saline} is the efficiency factor (1% and 4% used, respectively)

Method III

 Consists of the processing of wireline-derived porosity (such as neutron, sonic, or density logs) in Petra Software to estimate SRE.

$$SRE_{CO_2} = A_t * h_g * \mathbf{0}_{log} * \rho_{CO_2} * E_{saline}$$

Where:

 A_t is the area of a given county h_g is the average thickness, in the county, of unit under assessment \emptyset_{log} is the wireline-derived porosity ρ_{CO_2} is CO_2 density at reservoir conditions (0.73 tonnes/ m^3) E_{saline} is the efficiency factor (1% and 4% used, respectively)

Method IV

• Uses depth-dependent porosity model based on the previous studies that suggest that porosity decreases with depth $(\phi(d)=A^*e^{-depth^*B})$

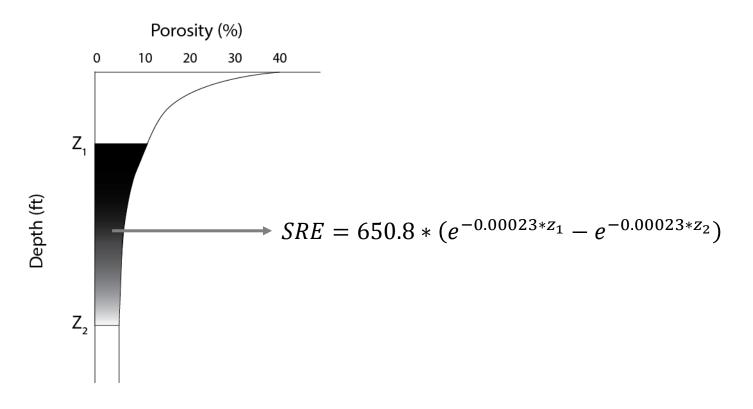
$$SRE_{CO_2} = A_t * h_g * \emptyset(d) * \rho_{CO_2} * E_{saline}$$

Where:

 A_t is the area of a given county h_g is the average thickness, in the county, of unit under assessment \emptyset (d) is porosity as a function of depth ρ_{CO_2} is CO_2 density at reservoir conditions (0.73 tonnes/ m^3) E_{saline} is the efficiency factor (1% and 4% used, respectively)

Method IV

$$SRE_{well} = \int_{z_{top}}^{z_{bottom}} \emptyset(z) dz = \int_{z_{top}}^{z_{bottom}} 0.1497 * e^{-0.00023*z} dz$$



Method V

Uses data from Mercury Injection Capillary Pressure (MICP) to define petrofacies.
 These petrofacies have characteristics values of porosity (and permeability).

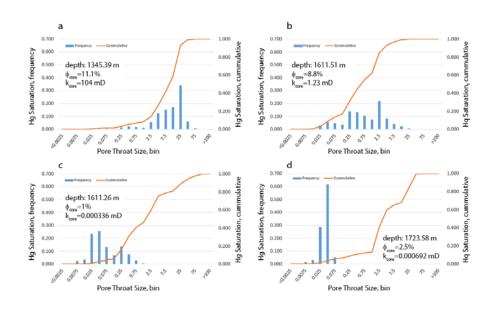
$$SRE_{CO_2} = A_t * h_g * \emptyset(petrofacies) * \rho_{CO_2} * E_{saline}$$

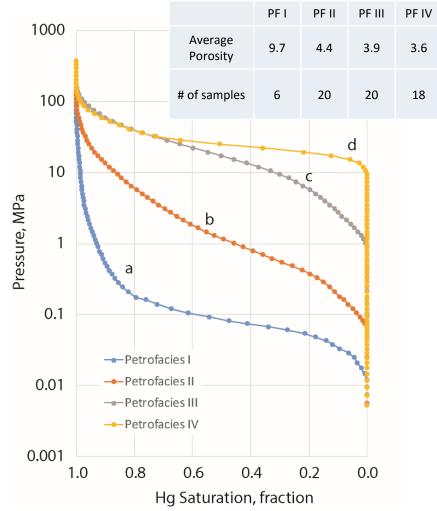
Where:

 A_t is the area of a given county h_g is the average thickness, in the county, of unit under assessment \emptyset (petrofacies) is porosity associated to petrofacies ρ_{CO_2} is CO_2 density at reservoir conditions (0.73 tonnes/ m^3) E_{saline} is the efficiency factor (1% and 4% used, respectively)

Method V

Uses data from Mercury Injection
 Capillary Pressure (MICP) to define
 characteristic pore size distribution curve.
 An average porosity is derived from each
 type petrofacies.





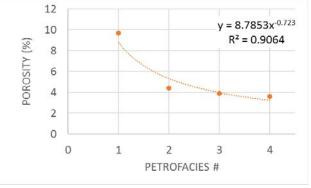
Petrofacies in Cores







	PF I	PF II	PF III	PF IV
Average Porosity	9.7	4.4	3.9	3.6
# of samples	6	20	20	18

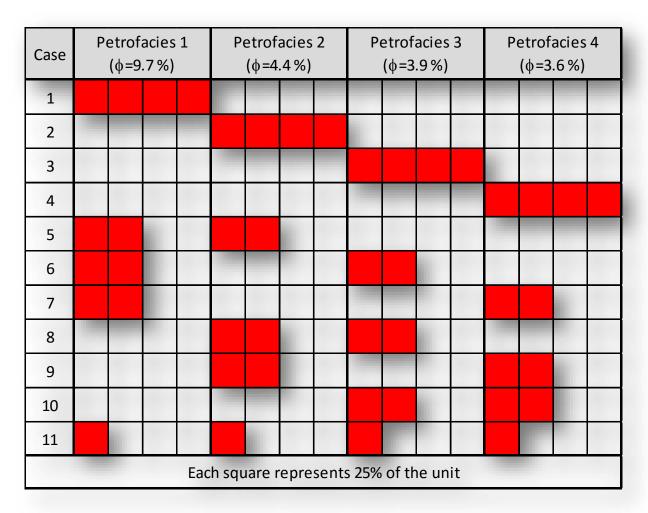






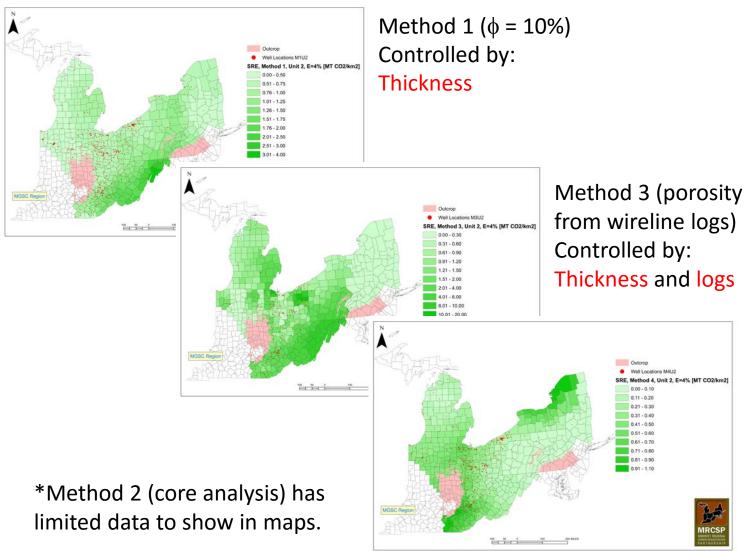
Method V

Each well is assumed a different scenario of abundance of petrofacies (porosity based on current study)



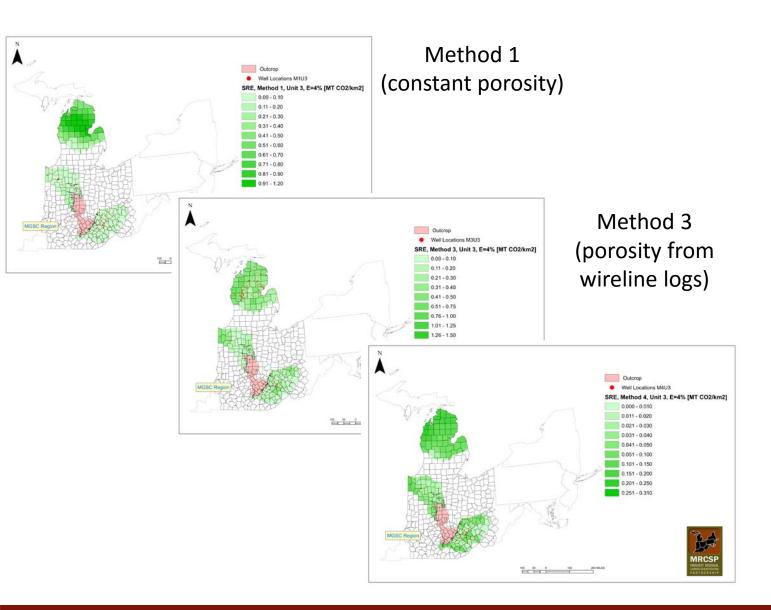
Results

Unit II (Trenton/Black River): Results* (E = 4%)



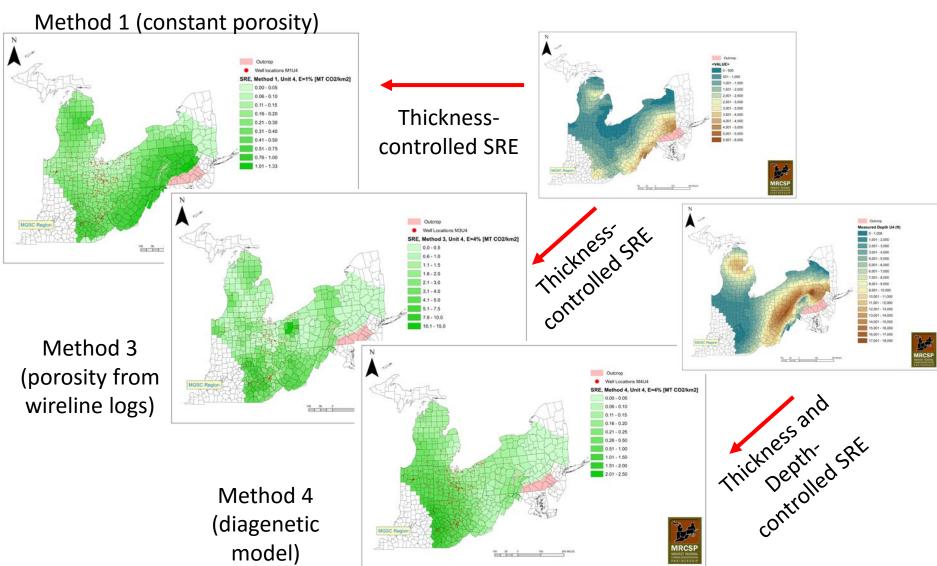
Method 4
(diagenetic model).
Controlled by:
Depth and
Thickness

Unit III (St. Peter SS): Results (E = 4%)

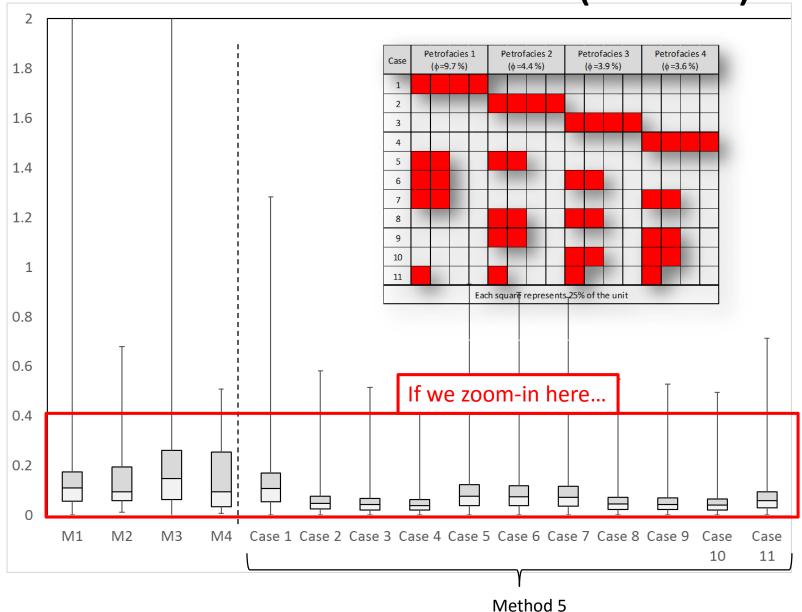


Method 4 (diagenetic model)

Unit IV (Knox): Results (E = 4%)

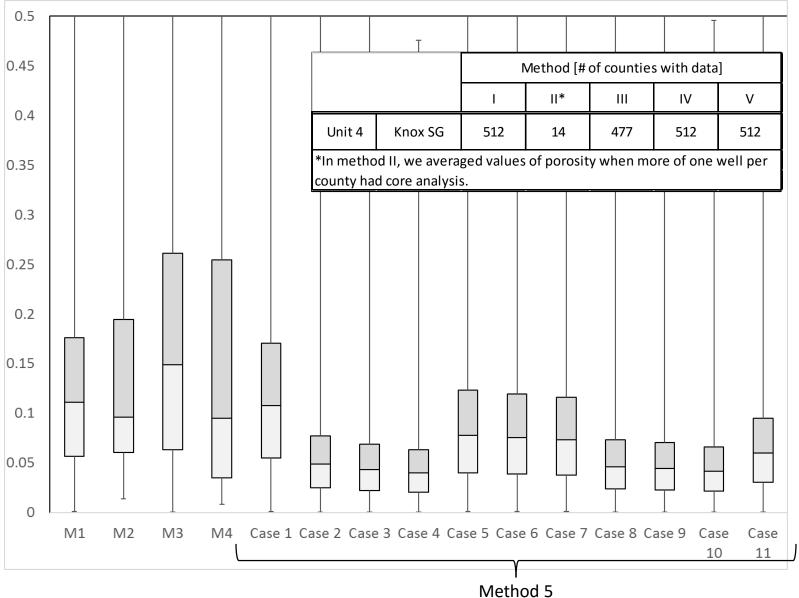


Results: All Methods (Unit 4)

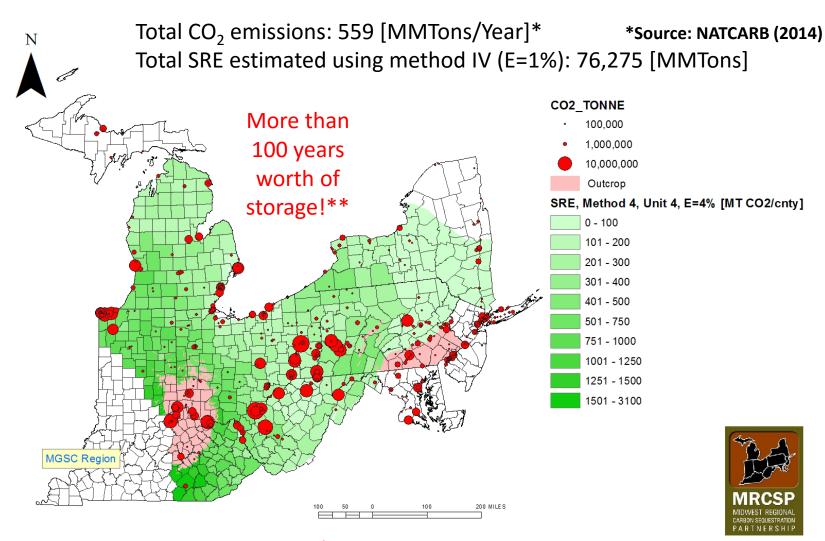


MM Tons CO₂/Km²

Results: All Methods (Unit 4)



How do these SREs compare with Emissions from Point Sources?

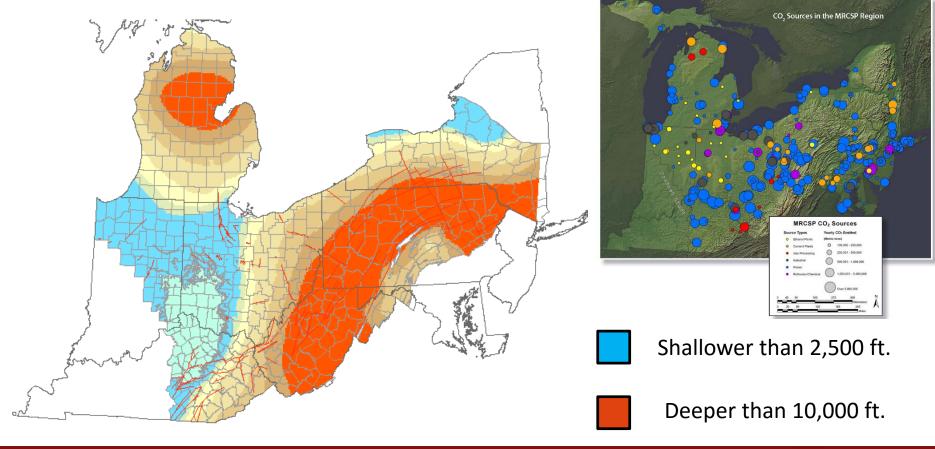


^{**} Further screening is necessary, such as min/max depth considerations, distance to source (pipeline), etc.

Reservoir Characterization: Isopach and Structure (Unit 4: Knox Supergroup and Equivalents)

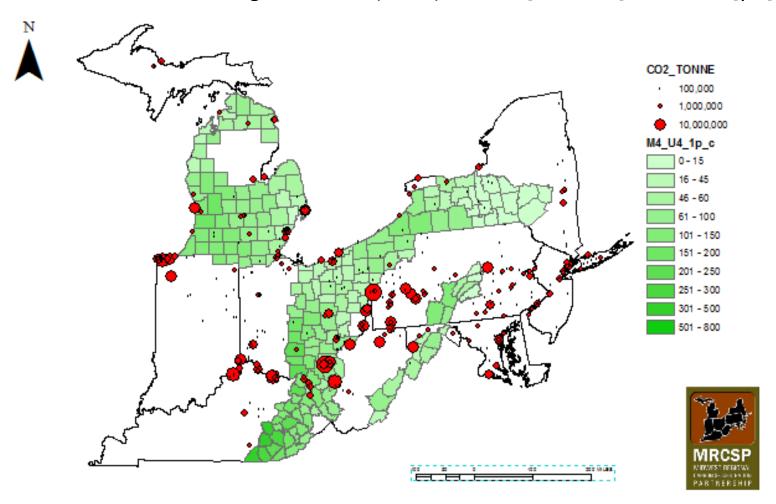
But...

...Portions of the region do not meet the basic criteria (i.e. too shallow). A second analysis excluding those areas resulted in SRE for unit 4 (Know and equivalents) using method IV is:



Reservoir Characterization: Isopach and Structure (Unit 4: Knox Supergroup and Equivalents)

Total CO₂ emissions: 559 [MMTons/Year]* *Source: NATCARB (2014) Total SRE estimated using method IV (E=1%): 14,935 [MMTons] or 26-100 [yrs] [E=1-4%]



Conclusions [1/2]

- SRE in the MRCSP region suggest that, there is sufficient storage capacity in the carbonate reservoirs of the Cambrian-Ordovician to deploy CCUS in the Midwestern region. Considering CO₂ emissions from stationary sources in the region result in +100 years of storage.
- Methodologies suggest that using a single value for porosity of 10% (Method 1) or average porosity from wireline logs (Method 3) results in overestimation of SRE.
- Regional scale SREs could possibly benefit from the use of efficiency factors that incorporate increased accuracy in factors (A, h, Ø). These "intermediate" efficiency factors will increase to reflect the decrease in uncertainty (e.g. Peck et al, 2014).

Conclusions [2/2]

- These estimates do not include local factors that should be included in site-scale analysis (i.e., details of the local geology).
- Future work should incorporate dynamic aspects of reservoir performance during and after injection.
- This study is exploratory in nature and does not intend to determine which method is "better" or "worse than", but rather, sets the stage for future consideration of integration of different methods based on robustness and availability. This is a good time, for example, to start considering the Variable Grid Method (VGM) introduced by NETL.



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Thank you!

Questions?









