

# **Predicting Subseismic Fracture Density and Orientation in the Gorm Field, Danish North Sea: An Approach Using Elastic Dislocation Models\***

**Brett Freeman<sup>1</sup>, David Quinn<sup>1</sup>, Cathal G. Dillon<sup>1</sup>, Michael Arnhold<sup>2</sup>, and Bastiaan Jaarsma<sup>3</sup>**

Search and Discovery Article #20321 (2015)\*\*

Posted September 21, 2015

\*Adapted from oral presentation given at AAPG 2015 Annual Convention and Exhibition, Denver, Colorado, May 31 – June 3, 2015

\*\*Datapages © 2015 Serial rights given by author. For all other rights contact author directly.

<sup>1</sup>Badley Geoscience Ltd, Hundleby, United Kingdom ([Brett@badleys.co.uk](mailto:Brett@badleys.co.uk))

<sup>2</sup>Maersk Oil Norway AS, Stavanger, Norway

<sup>3</sup>EBN, Utrecht, Netherlands

## **Abstract**

The chalk reservoir of the Gorm field, southern North Sea is dome shaped and faulted due to a combination of salt diapirism and regional E-W extension. Fractures developed in the structure considerably enhance permeability. The dataset discussed here records fractures in horizontal wells from more than 10km of image logs and provides a special opportunity to test theoretical models of fracture development with quantitative observations. In an effort to forecast fracture density and fracture orientation we have estimated the strains in the structure using an elastic dislocation model that incorporates mechanical boundaries in the form of the tectono-stratigraphic interface with salt and tectonic faults. More than 50% of the angular differences between poles to the planes of simulated and observed fractures are less than 30 degrees, 75% are less than 45 degrees. Relative strain magnitude appears to be a useful indicator of fracture density. At the field scale, small strain magnitudes correspond with small non-zero fracture densities and relatively large strain magnitudes correspond with high fracture densities.

## **Reference Cited**

Esmerode, E.V., H. Lykke-Andersen, and F. Surlyk, 2008, Interaction between bottom currents and slope failure in the Late Cretaceous of the southern Danish Central Graben, North Sea: *Journal of the Geological Society*, v. 165, p. 55–72.

# Predicting subseismic fracture density and orientation in the Gorm Field, Danish North Sea: an approach using elastic dislocation models

Brett Freeman, David Quinn, Cathal Dillon (Badleys)

Michael Arnhild (Maersk)

Bastiaan Jaarsma (EBN)

Acknowledgements



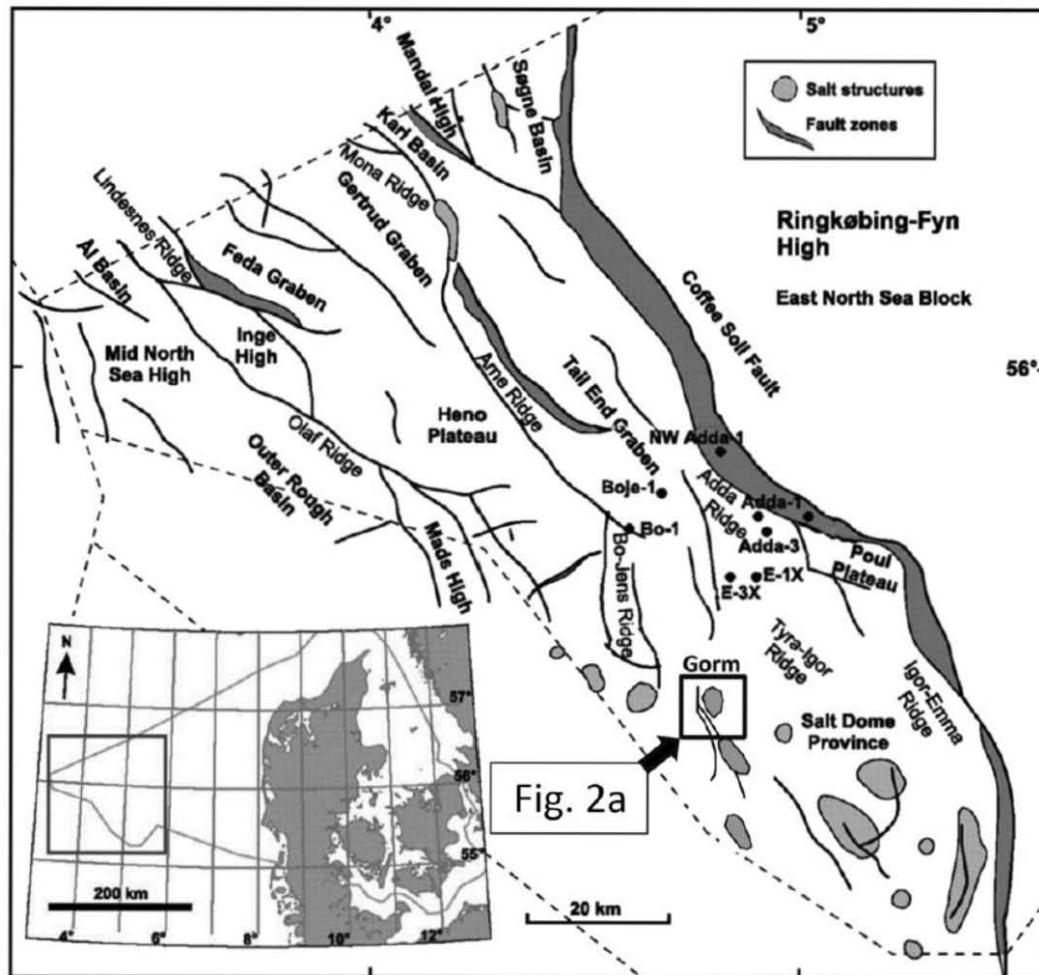


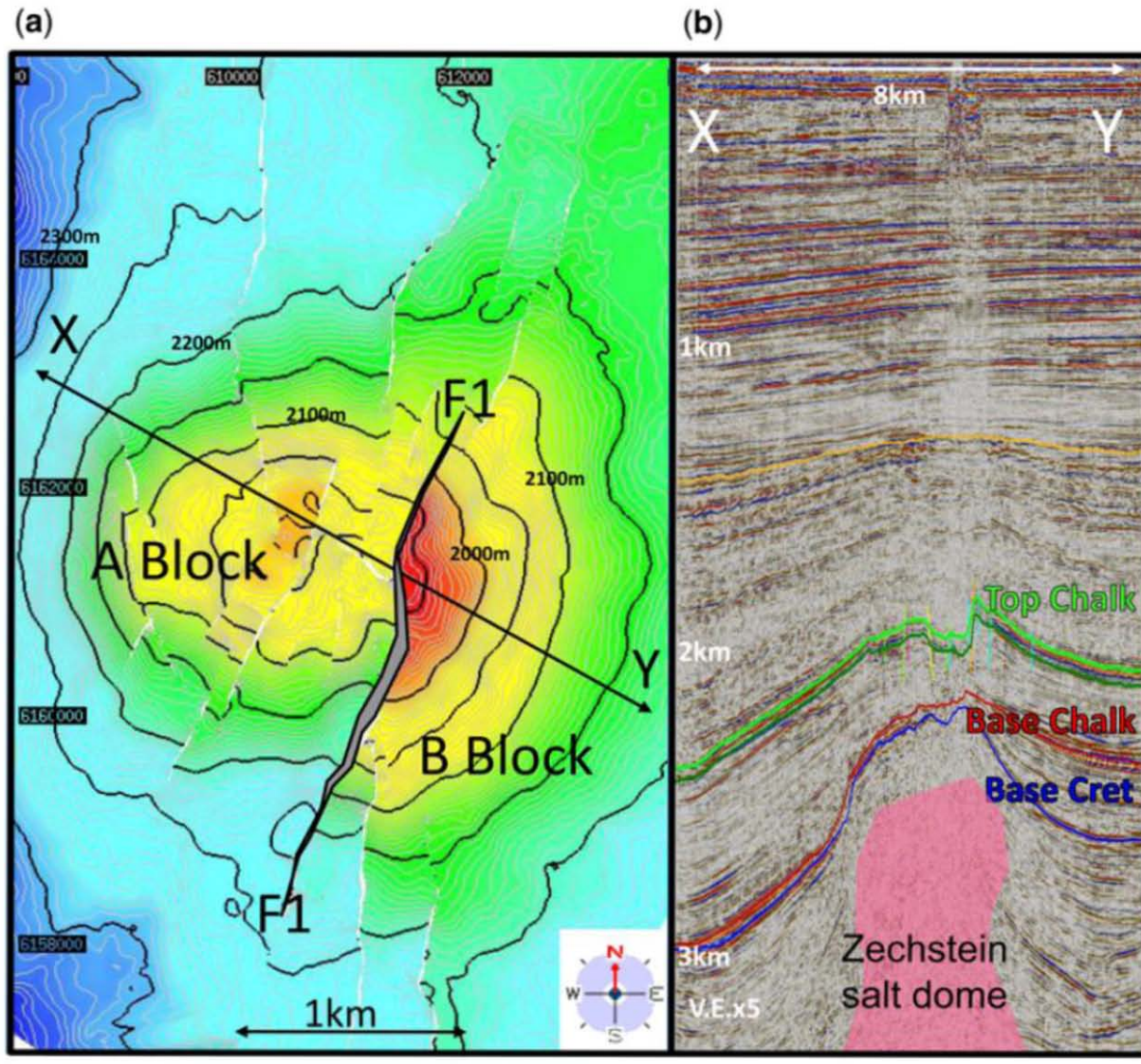
Fig. 1. Jurassic elements of the Danish Central Graben after Esmerode *et al.* (2008). The bold square marked 'Fig. 2a' indicates the location of the Gorm Field.

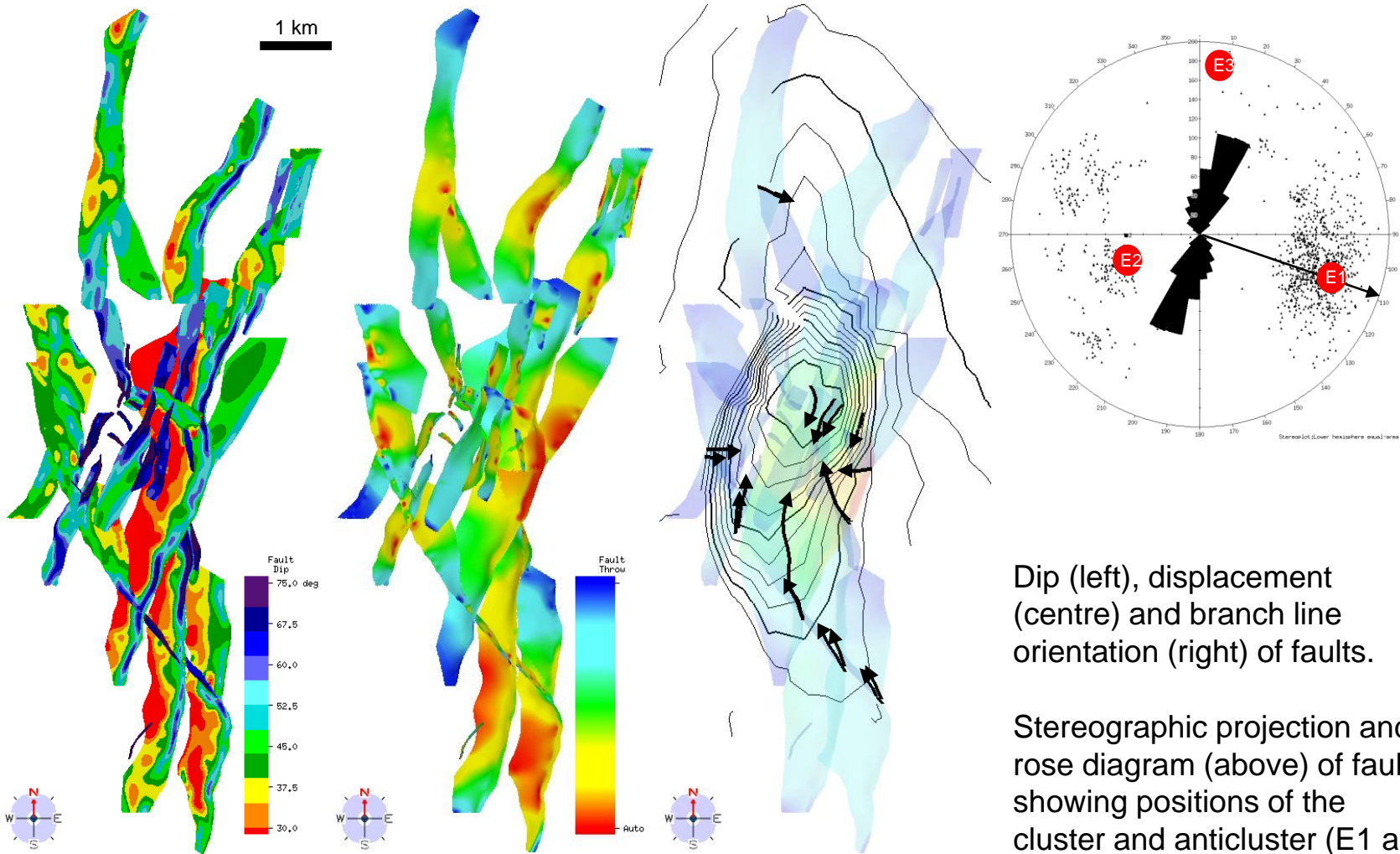
- Chalk field, operated by Maersk, Producing since 1981, 327 mb oil, 580 bscf gas
- Zechstein salt (seated at 5500 m - 7500 m) penetrates Jurassic rocks, present day top at 2750 m, 250 m beneath the base of the Chalk
- The Chalk thickness is approx. 500 m but is thinned on the crest in the form of a dome, present day top of the dome at approx. 1800 m
- Matrix permeability 0.5 mD - 8 mD, matrix porosity 15% - 45%
- Production is known to depend on fracture permeability

- More than 111 wells, 13 of which have in total more than 10 km image logs
- More than 16,000 logged fractures
- 433 fractures are considered to be large, sub-seismic shear fractures (i.e. faults) with observed offsets
- Density of these fractures up to 0.22 per m (approx. 1 every 5 m)
- 3D seismic data from 1998 and 2005 (time migrated and depth converted)
- Interpretation of seismically resolved faults (down to a min offset of about 20m)
- Interpretation of chalk reservoir boundaries, salt top and underlying basement

- In any situation we run an ED model but we don't often get the opportunity to test the results so completely. Given the relative abundance of structural and fracture data, the Gorm field would appear to be an excellent natural laboratory.
- Using routinely available (depth converted) seismic interpretation and an Elastic Dislocation (ED) based continuum model which embodies deformation associated with the mechanical boundary between salt and overburden and mechanical interaction of coeval faults, can we make reasonable estimates of
  - (a) sub-seismic fracture density
  - (b) orientations of those fractures

# Summary map and section

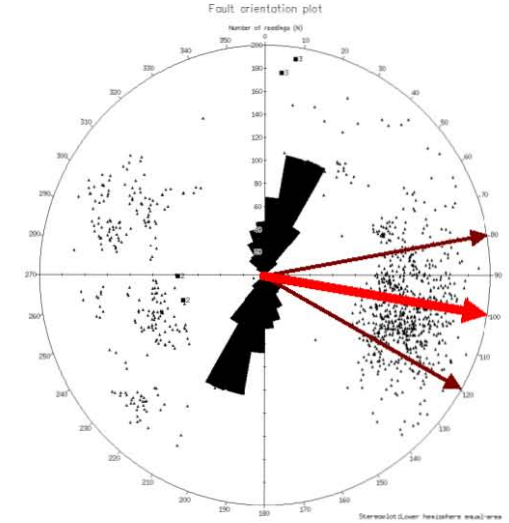
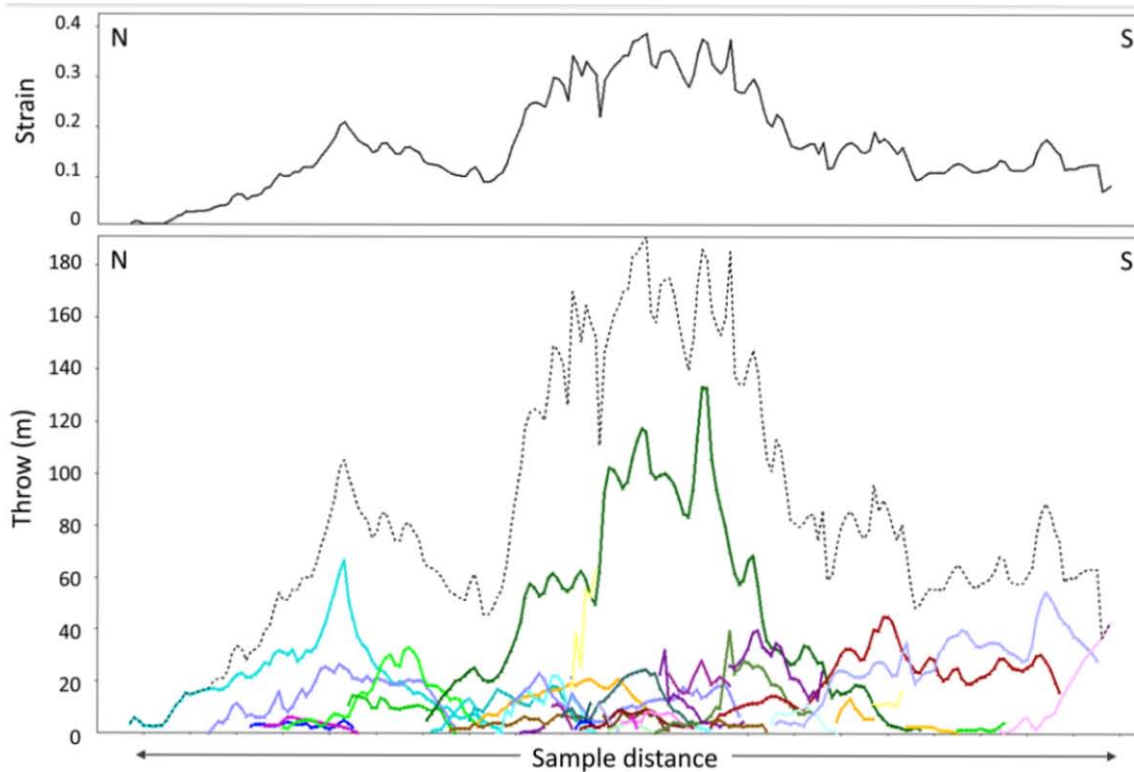




Dip (left), displacement (centre) and branch line orientation (right) of faults.

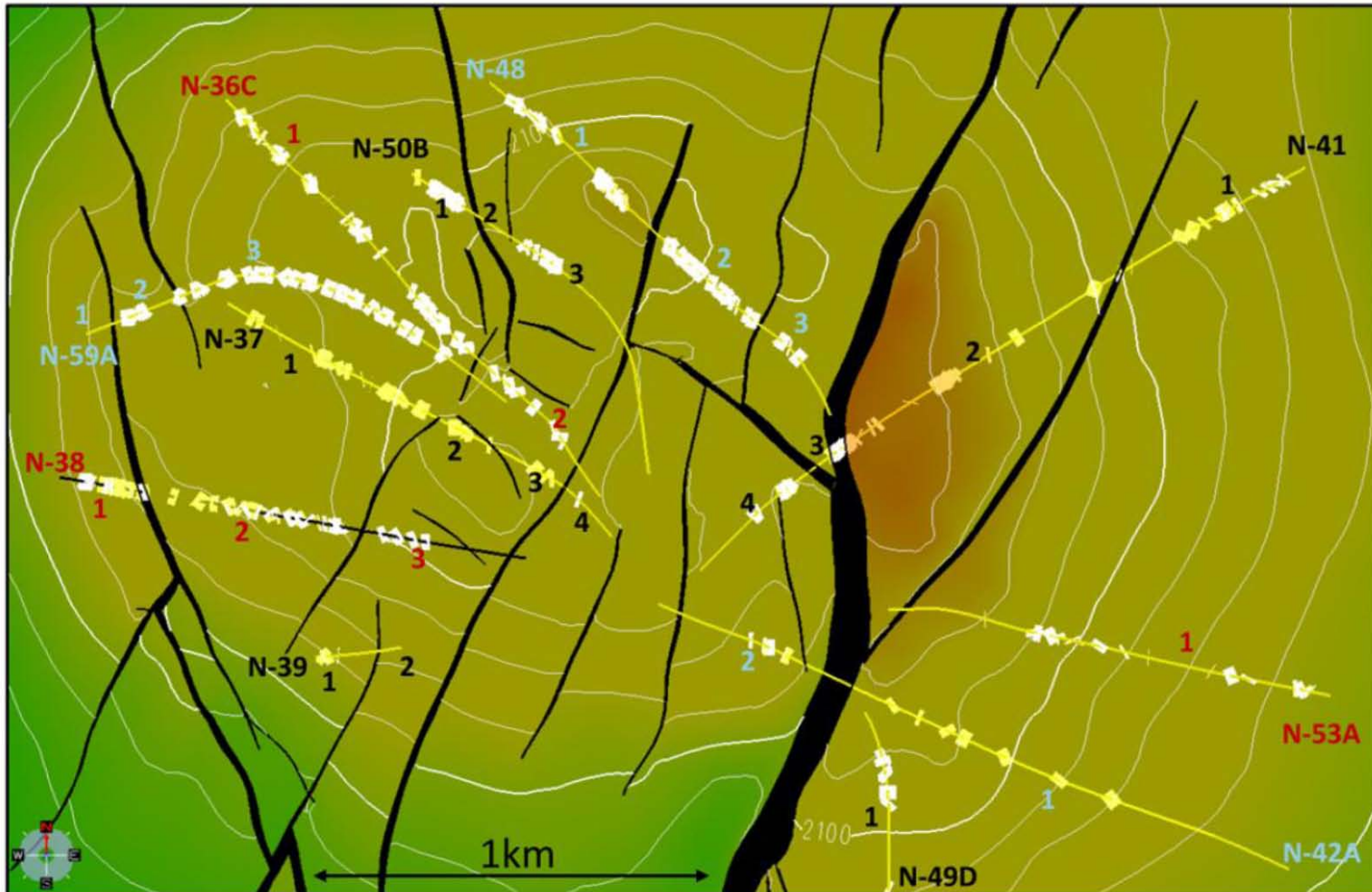
Stereographic projection and rose diagram (above) of faults showing positions of the cluster and anticluster (E1 and E3)





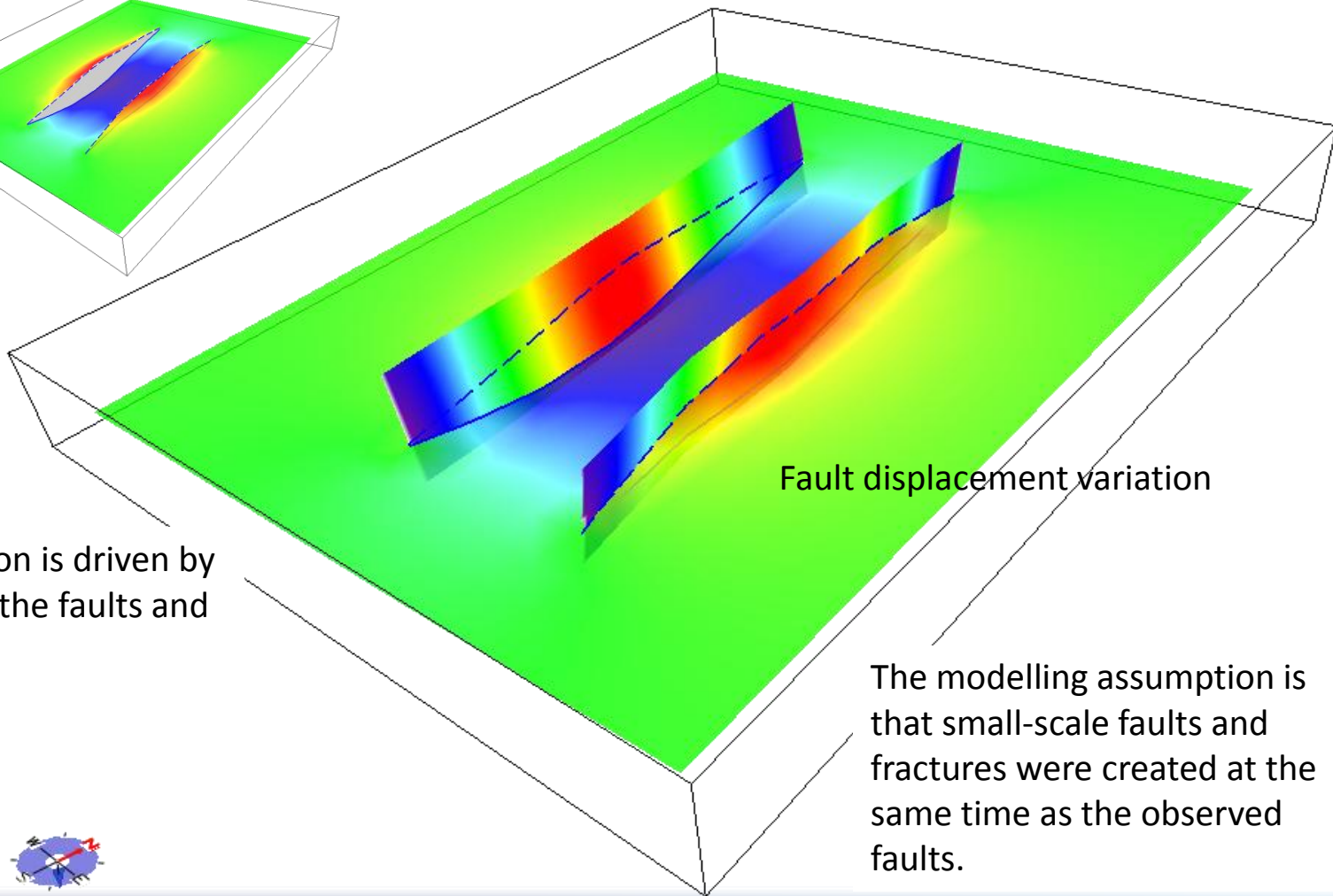
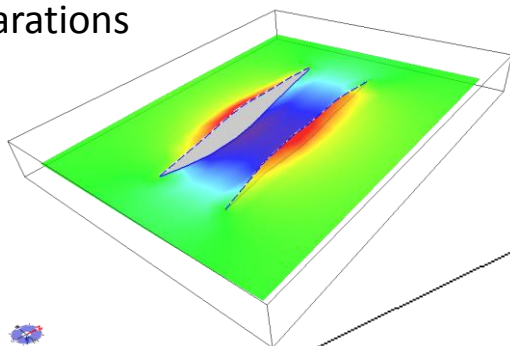
$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
-0.03	0.00	0.03
-0.06	0.00	0.06

**Fig. 5.** The lower figure shows the heave profiles of all the framework faults (each individual fault has a unique colour, e.g. Fault F1 is the large green profile in the centre) measured at an azimuth 100°. The summed heaves are represented by the black dotted line. In the upper figure the summed heave is scaled to regional extensional strain (0.4 = 4% extension).



**Fig. 3.** Structure map of the Top M2 horizon showing wells and major fractures as interpreted from image logs. Labels indicate the structural domains that have been used to compartmentalize the fracture densities.

Fault separations



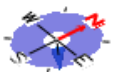
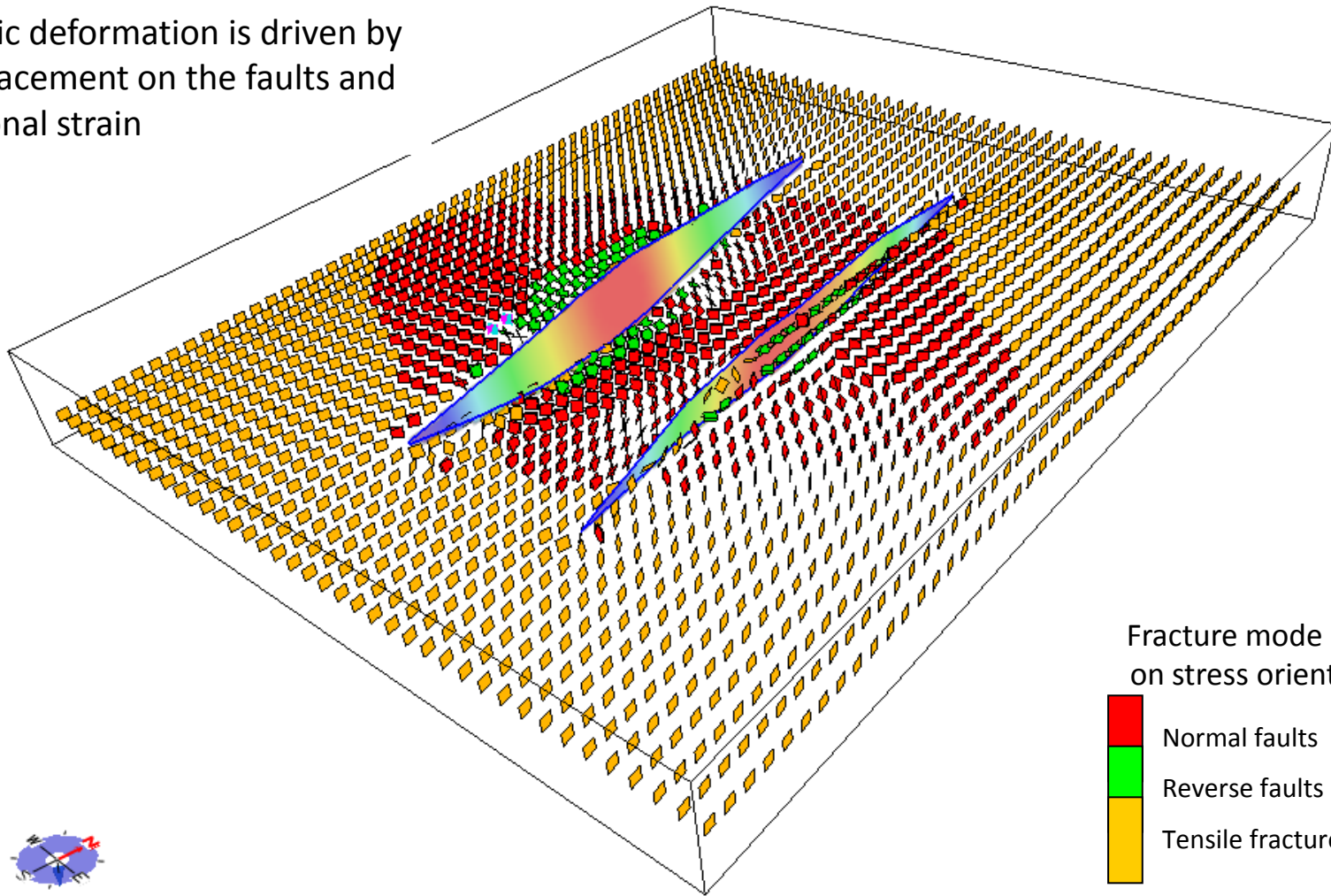
Fault displacement variation

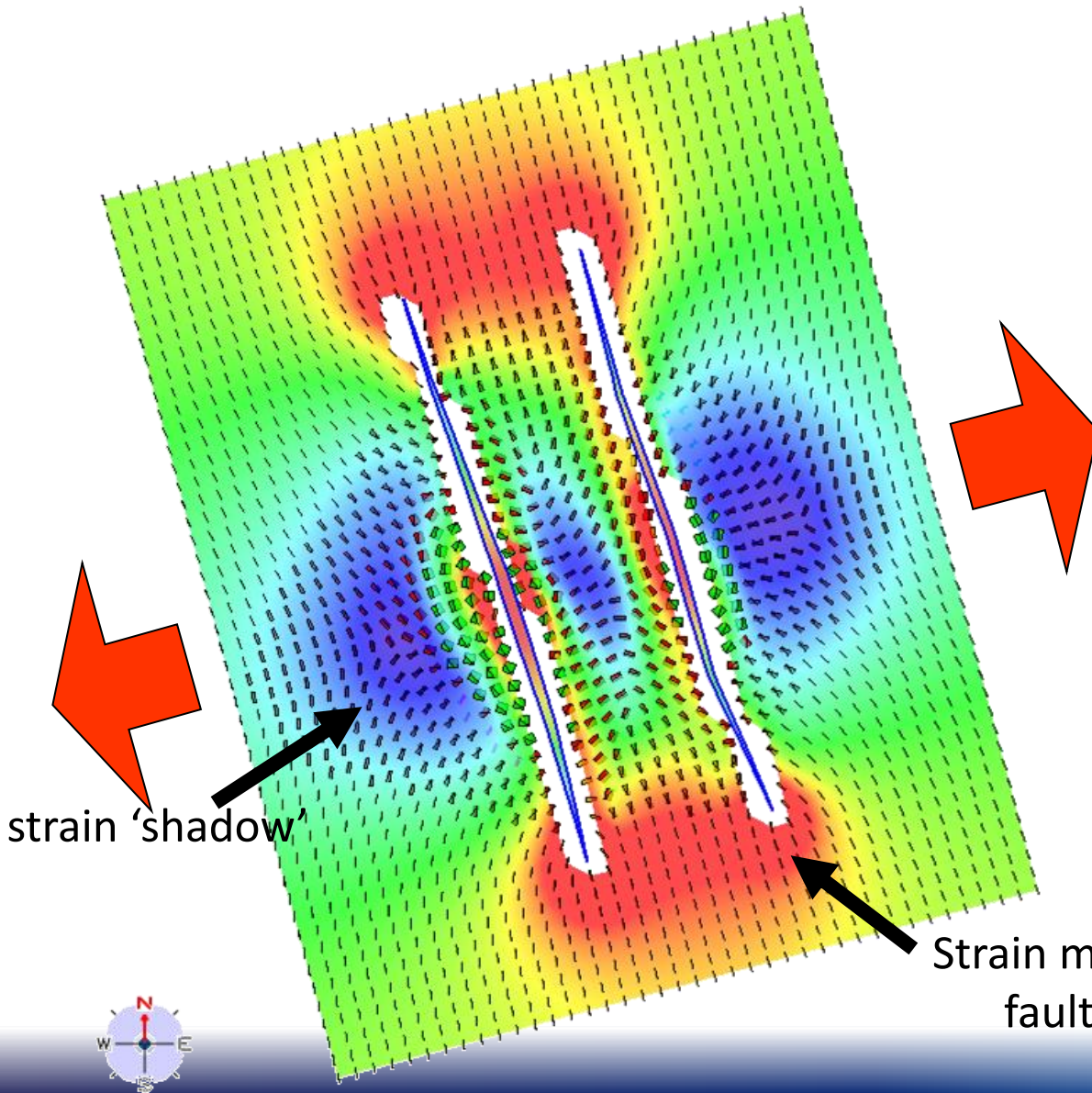
Elastic deformation is driven by displacement on the faults and regional strain



The modelling assumption is that small-scale faults and fractures were created at the same time as the observed faults.

Elastic deformation is driven by displacement on the faults and regional strain





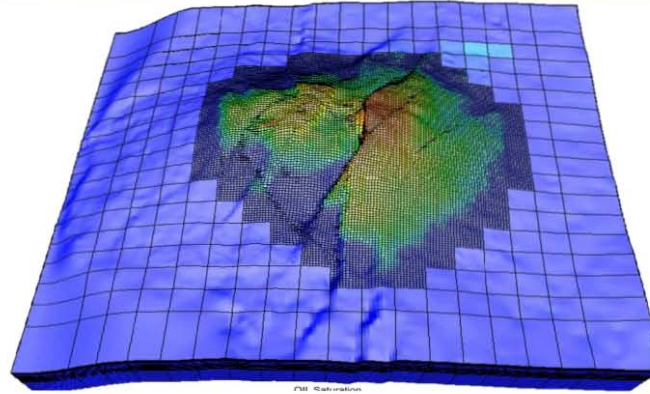
It's assumed that fracture intensity will scale in some way with strain intensity.

There are many ways to represent this but here we use strain magnitude

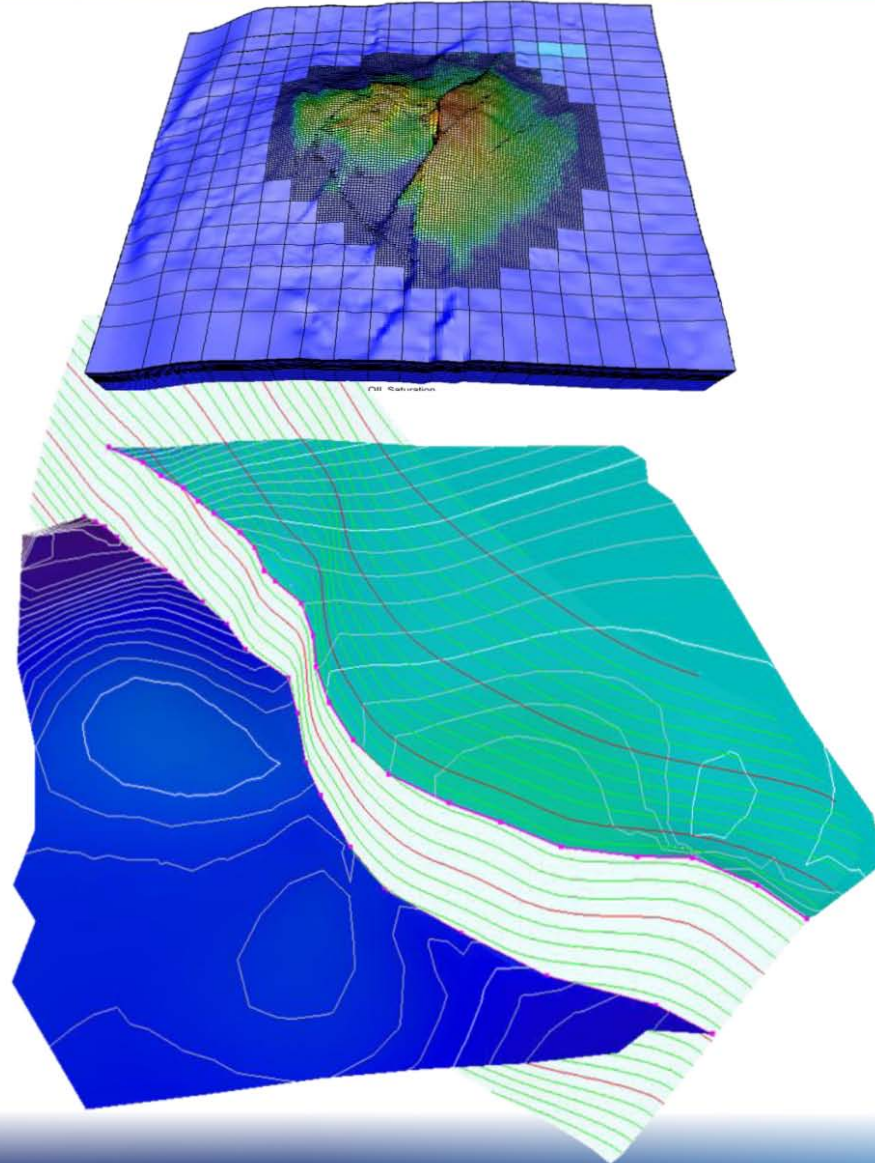
$$\epsilon_m = \sqrt{\epsilon_1^2 + \epsilon_2^2 + \epsilon_3^2}$$

Strain magnitude concentration at fault tips – more fractures?

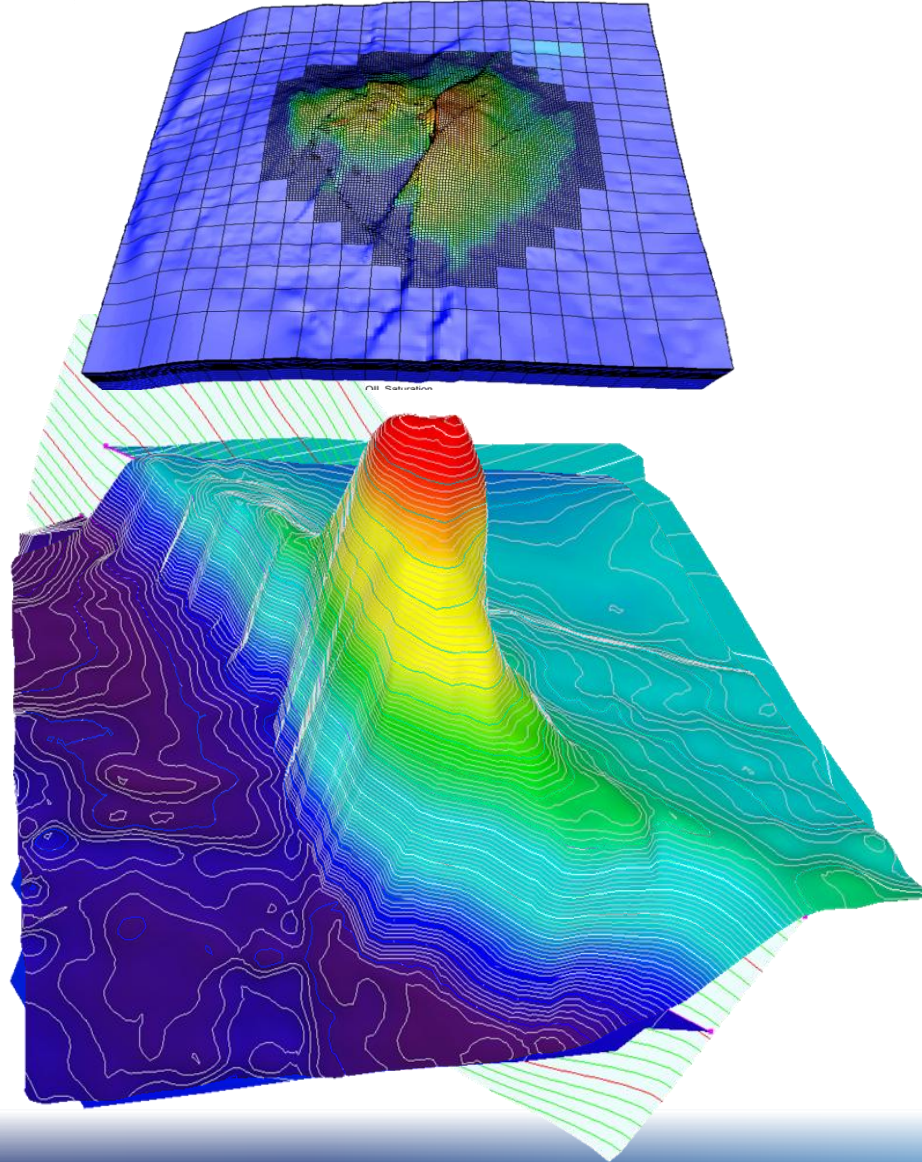
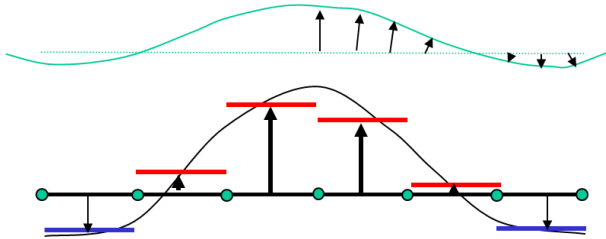
# Application to the Gorm structure



# Application to the Gorm structure



Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

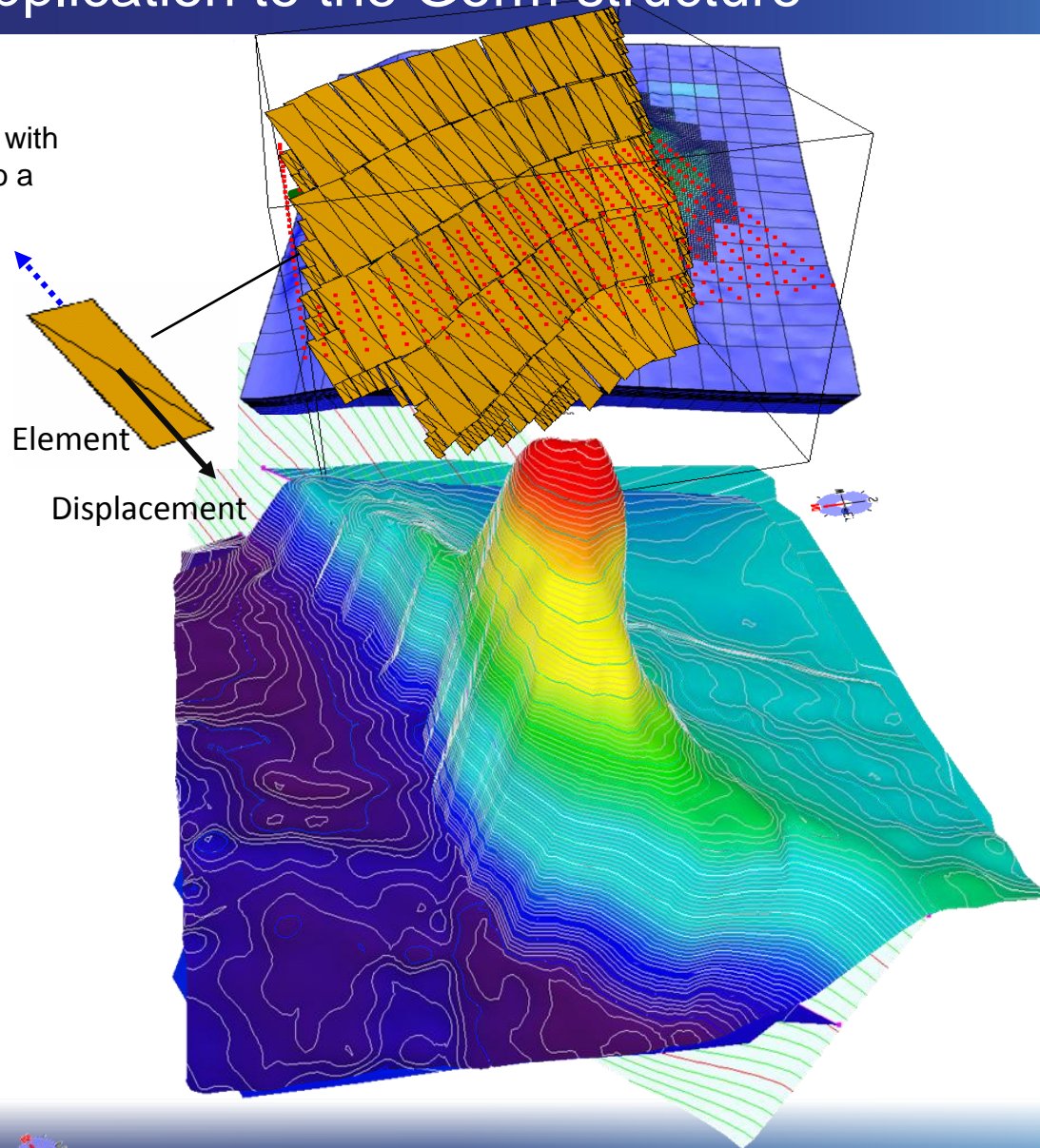




# Application to the Gorm structure

Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

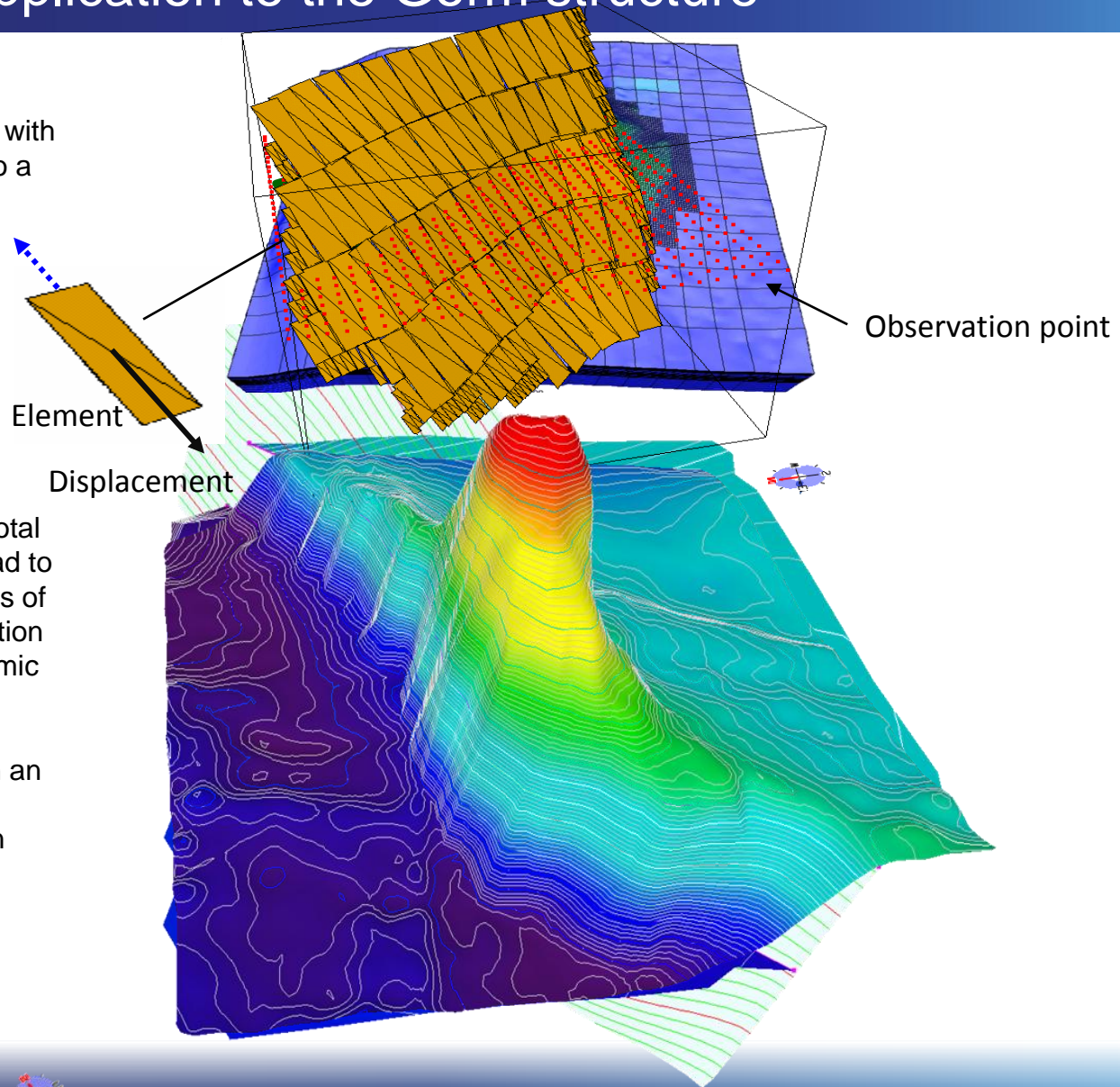


Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

At each observation point the total strains are calculated which lead to the orientations and magnitudes of the principal stress, the orientation and mode of failure for sub-seismic fractures

An observation point can be on an horizon surface, a grid or importantly at the location of an observed fracture in a well

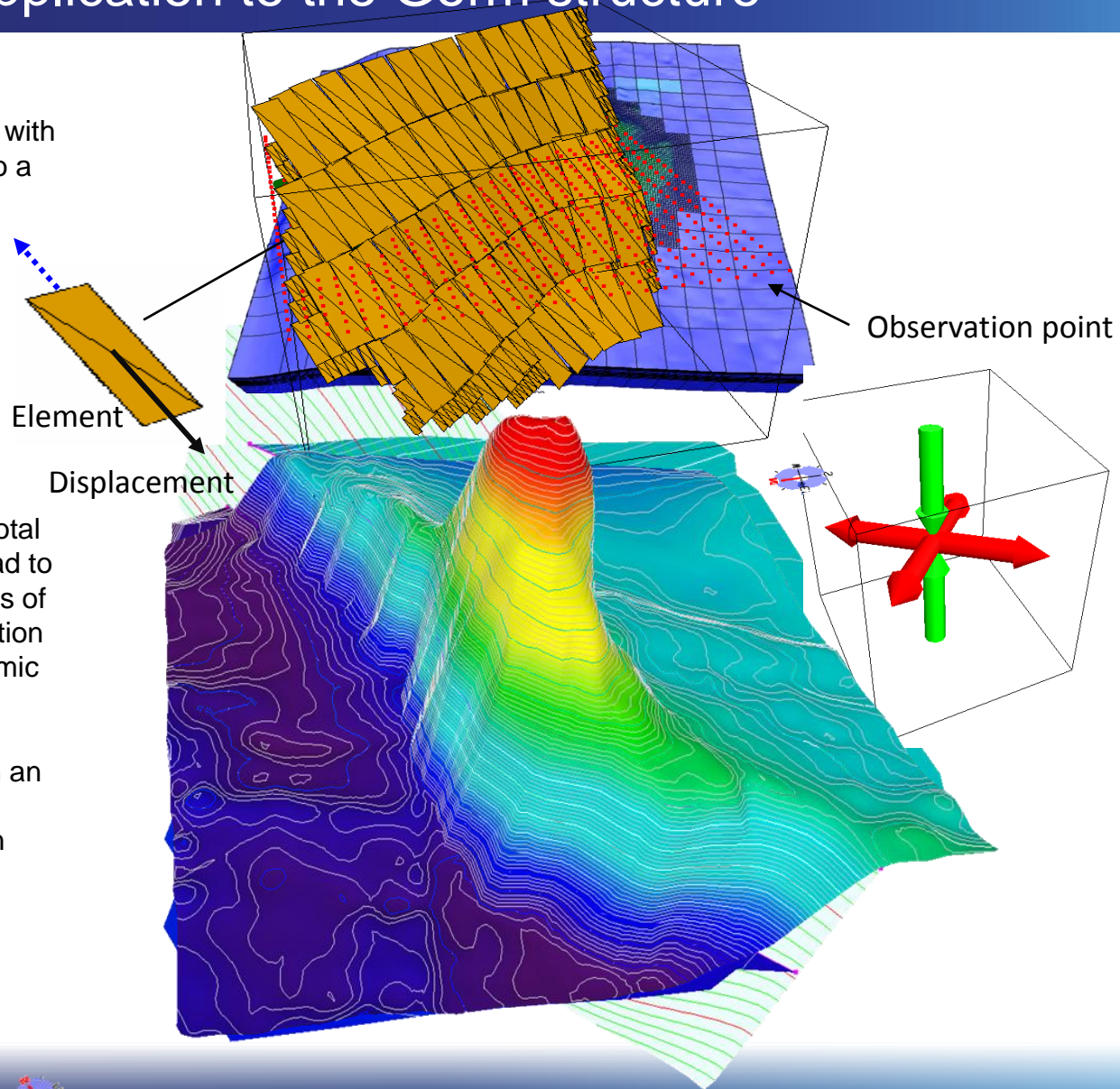


Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

At each observation point the total strains are calculated which lead to the orientations and magnitudes of the principal stress, the orientation and mode of failure for sub-seismic fractures

An observation point can be on an horizon surface, a grid or importantly at the location of an observed fracture in a well

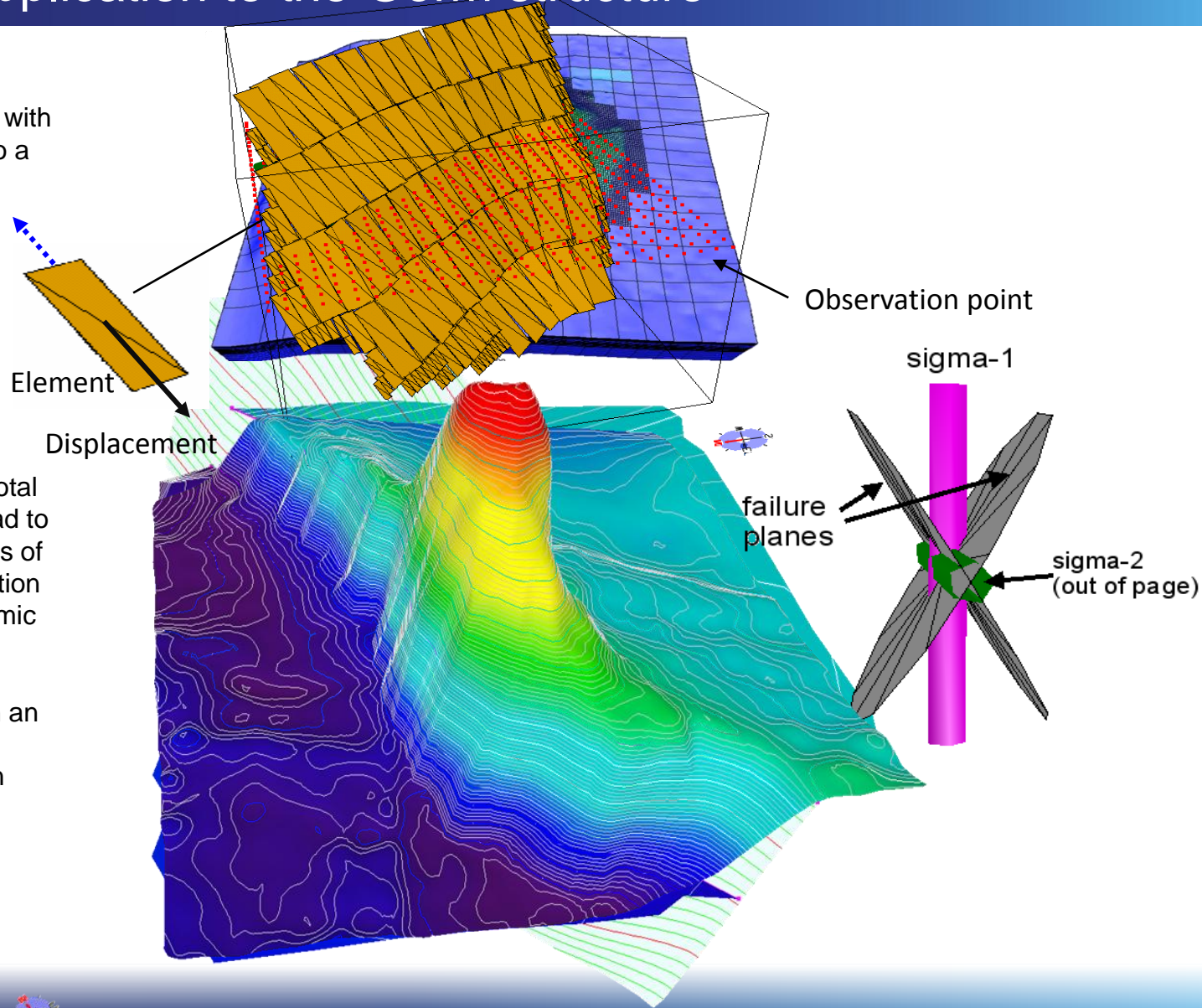


Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

At each observation point the total strains are calculated which lead to the orientations and magnitudes of the principal stress, the orientation and mode of failure for sub-seismic fractures

An observation point can be on an horizon surface, a grid or importantly at the location of an observed fracture in a well



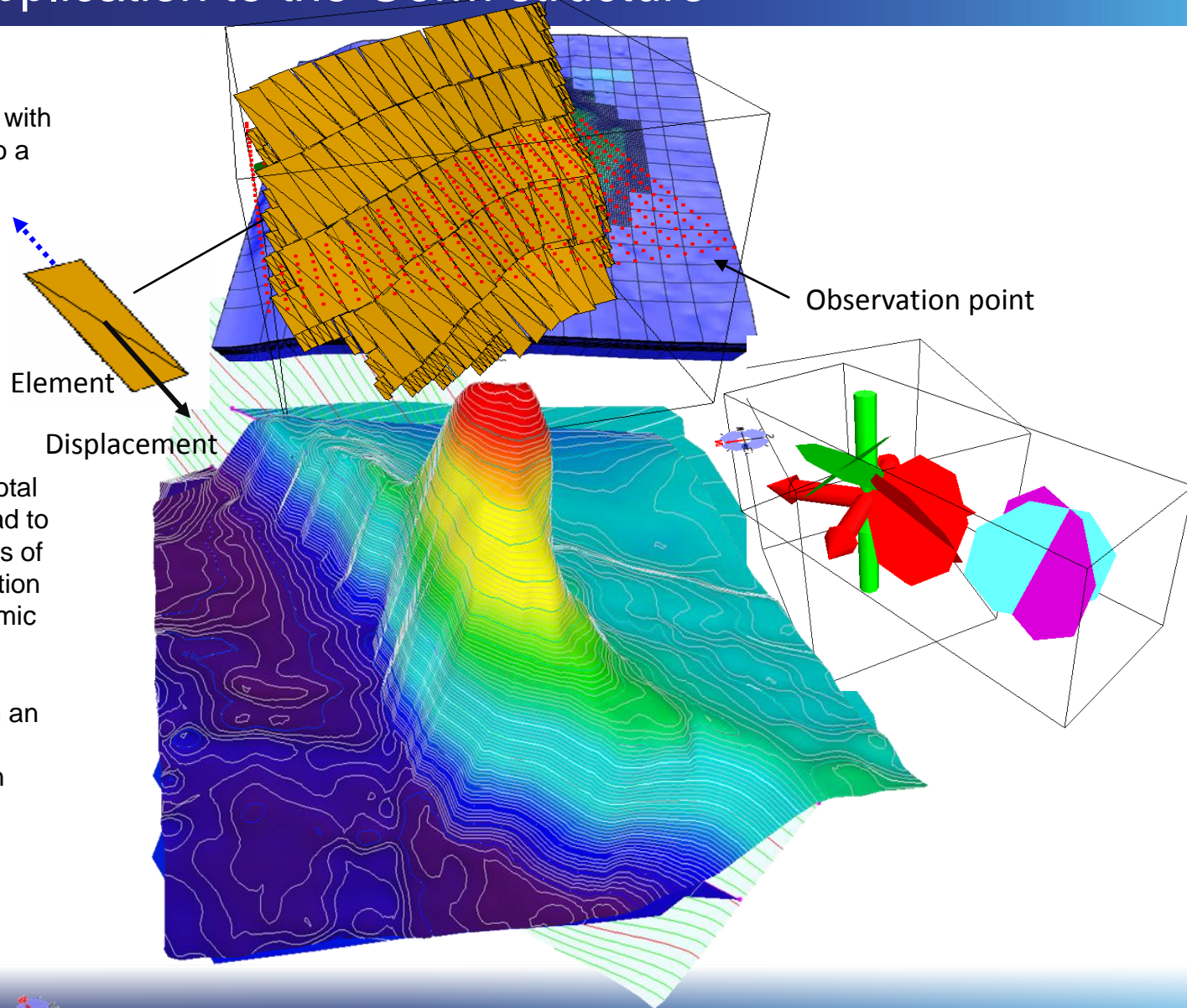
# Application to the Gorm structure

Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

At each observation point the total strains are calculated which lead to the orientations and magnitudes of the principal stress, the orientation and mode of failure for sub-seismic fractures

An observation point can be on an horizon surface, a grid or importantly at the location of an observed fracture in a well

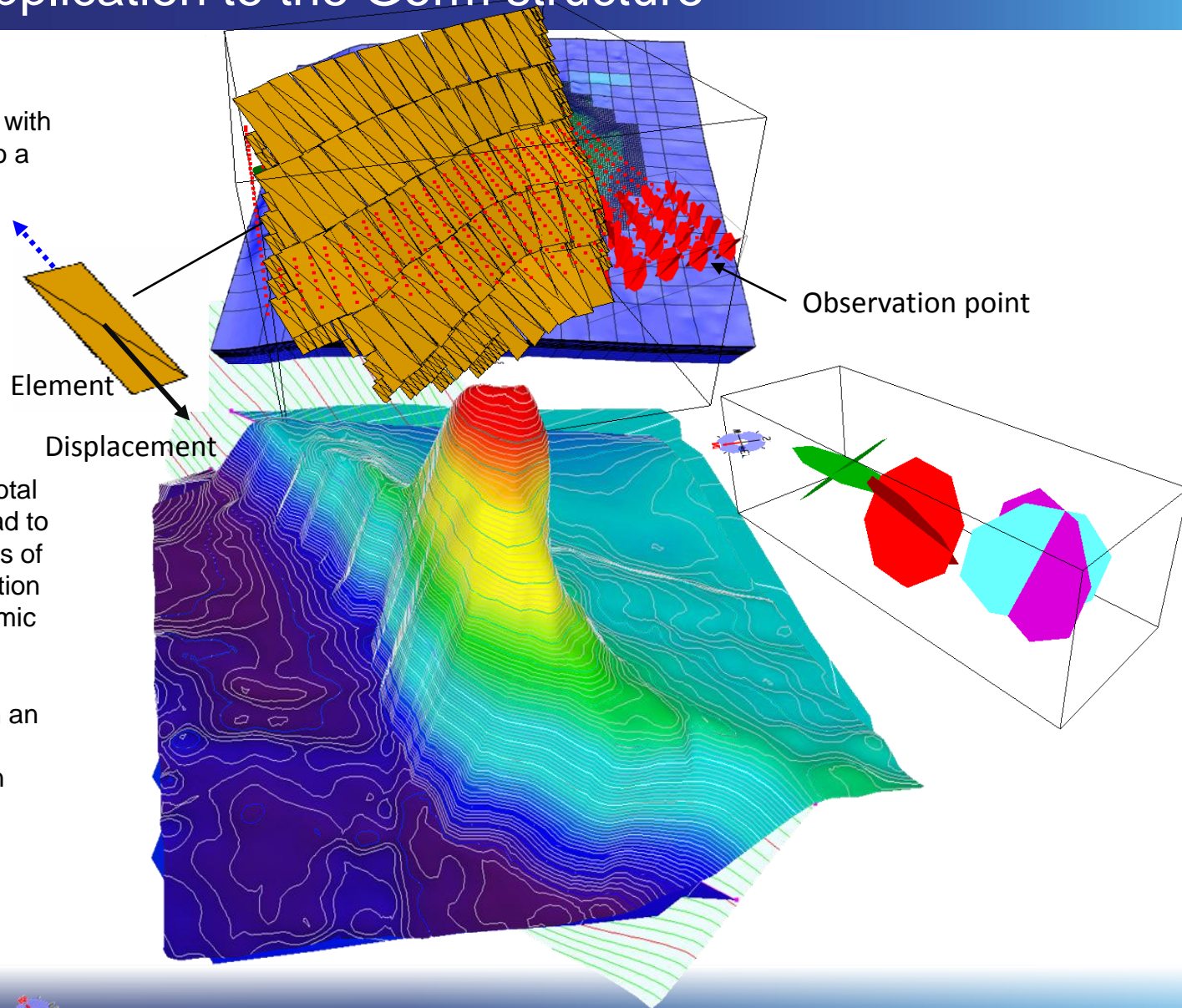


Salt intrusion is modelled with triangular, dilation, dislocations with uplift and subsidence relative to a pre-mobile top salt layer

The faults in the reservoir are modelled as sets of shear dislocations in a broadly E-W extensional regime

At each observation point the total strains are calculated which lead to the orientations and magnitudes of the principal stress, the orientation and mode of failure for sub-seismic fractures

An observation point can be on an horizon surface, a grid or importantly at the location of an observed fracture in a well



**Table 1.** Summary table of mnemonics of mechanical boundary configurations

	Allochthonous salt (uplift only)			Autochthonous salt		
Scale factor for influence of salt	0	0.5	1	0	0.5	1
Exclude faults	–	SAF0S0	SBF0S0	–	SAF0S1	SBF0S1
Include faults	S0F1	SAF1S0	SBF1S0	–	SAF1S1	SBF1S1

The prefixes S0, SA and SB refer to the influence of the salt used in a run: S0 = none; SA = half; SB = full influence. The middle acronyms refer to the influence of the fault: F0 for no influence and F1 for full. The suffixes S0 and S1 refer to no subsidence and subsidence, respectively.

**Table 2.** Three sets of values of remote boundary strains used during the tests on each model-run

$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
–0.03	0.00	0.03
–0.06	0.00	0.06

We also investigated the sensitivity of these models to

- (a) variation in orientation of tectonic extension
- (b) Variation in coefficient of internal friction between 0.2 and 1.0 (0.55 being preferred)

**Table 1.** Summary table of mnemonics of mechanical boundary configurations

	Allochthonous salt (uplift only)			Autochthonous salt		
Scale factor for influence of salt	0	0.5	1	0	0.5	1
Exclude faults				-	SAF0S1	SBF0S1
Include faults				-	SAF1S1	SBF1S1

The prefixes S0, SA and SB refer to the influence of salt, respectively. The middle acronym refers to the influence of subsidence, respectively.

half; SB = full influence. The middle acronym refers to no subsidence and

**Continuous in-flow of salt: no withdrawal or subsidence**

**Table 2.** Three sets of values of remote boundary strains used during the tests on each model-run

$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
-0.03	0.00	0.03
-0.06	0.00	0.06

We also investigated the sensitivity of these models to

- (a) variation in orientation of tectonic extension
- (b) Variation in coefficient of internal friction between 0.2 and 1.0 (0.55 being preferred)



**Table 1.** Summary table of mnemonics of mechanical boundary configurations

	Allochthonous salt (uplift only)			Autochthonous salt		
Scale factor for influence of salt	0	0.5	1	0	0.5	1
Exclude faults	–	SAF0S0	SBF0S0	SAF0S1	SAF0S0	SAF0S1
Include faults	S0F1	SAF1S0	SBF1S0	S0F1	SAF1S0	SBF1S0

**Local salt: uplift and subsidence**

The prefixes S0, SA and SB refer to the influence of the salt used in a run: S0 = no influence, SA = uplift, SB = subsidence. The suffixes F0 and F1 refer to the influence of the fault: F0 for no influence and F1 for full subsidence, respectively.

**Table 2.** Three sets of values of remote boundary strains used during the tests on each model-run

$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
-0.03	0.00	0.03
-0.06	0.00	0.06

We also investigated the sensitivity of these models to

- (a) variation in orientation of tectonic extension
- (b) Variation in coefficient of internal friction between 0.2 and 1.0 (0.55 being preferred)

**Table 1.** Summary table of mnemonics of mechanical boundary configurations

	Allochthonous salt (uplift only)			Autochthonous salt		
Scale factor for influence of salt	0	0.5	1	0	0.5	1
Exclude faults	–	SAF0S0	SBF0S0	–	SAF0S1	SBF0S1
Include faults	S0F1	SAF1S0	SBF1S0	–	SAF1S1	SBF1S1

The prefixes S0, SA and SB refer to the influence of the salt used in a run: S0 = none; SA = half; SB = full influence. The middle acronyms refer to the influence of the fault: F0 for no influence and F1 for full. The suffixes S0 and S1 refer to no subsidence and subsidence, respectively.

**Table 2.** Three sets of values of remote boundary strains used during the tests on each model-run

$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
–0.03	0.00	0.03
–0.06	0.00	0.06

We also investigated the sensitivity of these models to

- variation in orientation of tectonic extension
- Variation in coefficient of internal friction between 0.2 and 1.0 (0.55 being preferred)

**Table 1.** Summary table of mnemonics of mechanical boundary configurations

	Allochthonous salt (uplift only)			Autochthonous salt		
Scale factor for influence of salt	0	0.5	1	0	0.5	1
Exclude faults					SAF0S1	SBF0S1
Include faults					SAF1S1	SBF1S1

The prefixes S0, SA and SB refer to the influence of tectonic extension, respectively.

**Vary the impact of salt:  
No effect, half effect, full effect**

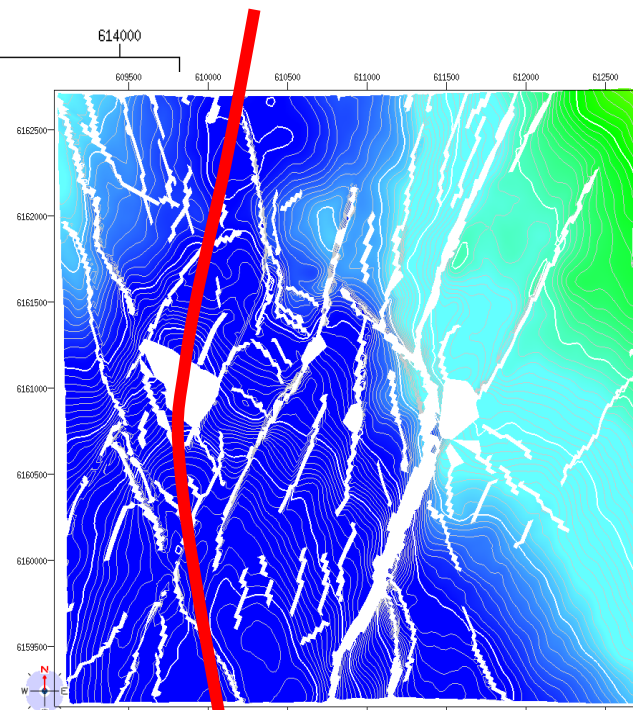
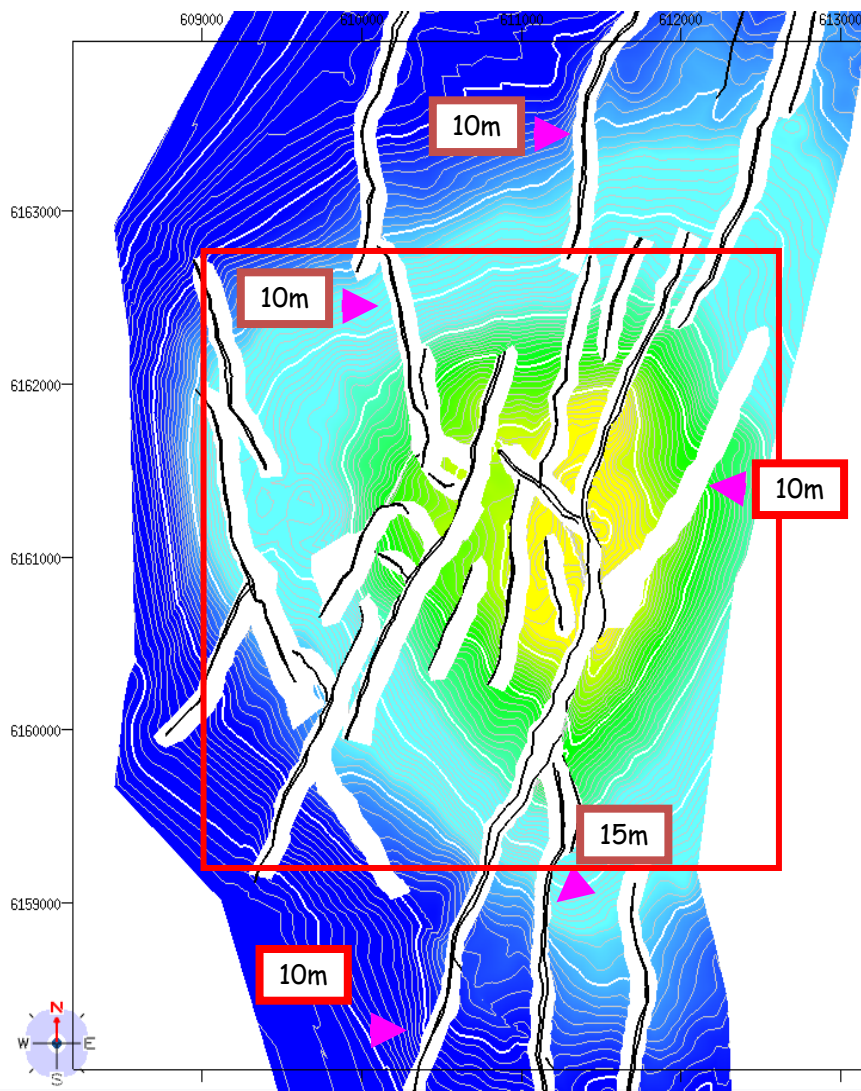
= full influence. The middle and S1 refer to no subsidence and

**Table 2.** Three sets of values of remote boundary strains used during the tests on each model-run

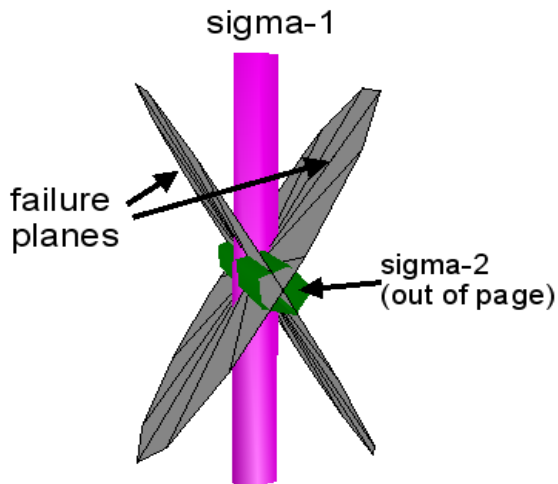
$\epsilon_v$	$\epsilon_{hmin}$	$\epsilon_{hmax}$
0.00	0.00	0.00
-0.03	0.00	0.03
-0.06	0.00	0.06

We also investigated the sensitivity of these models to

- variation in orientation of tectonic extension
- Variation in coefficient of internal friction between 0.2 and 1.0 (0.55 being preferred)



Residual "basin" after restoration.  
 This could be improved (removed) by  
 modifying the salt and pre-salt  
 interpretation

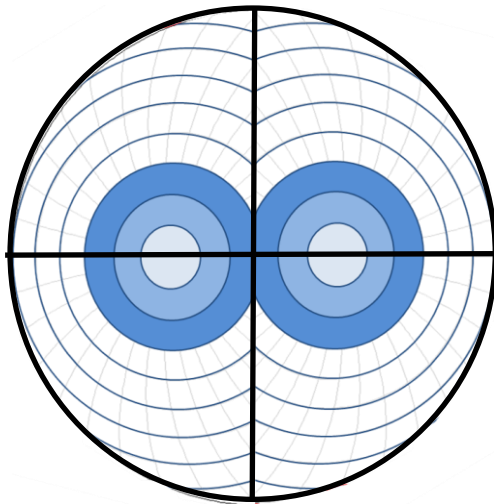


We observe a single fracture

We MODEL a conjugate pair at the same location (our models created very few tensile fractures)

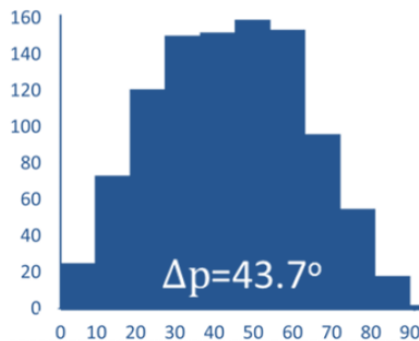
We MEASURE the smallest difference in angle between the poles of the modelled and observed fractures ( $\Delta p$ )

Our null hypothesis states that the orientations of natural fractures is random



The distribution of  $\Delta p$  for the null hypothesis is not uniform

(a) Base case (random distribution)



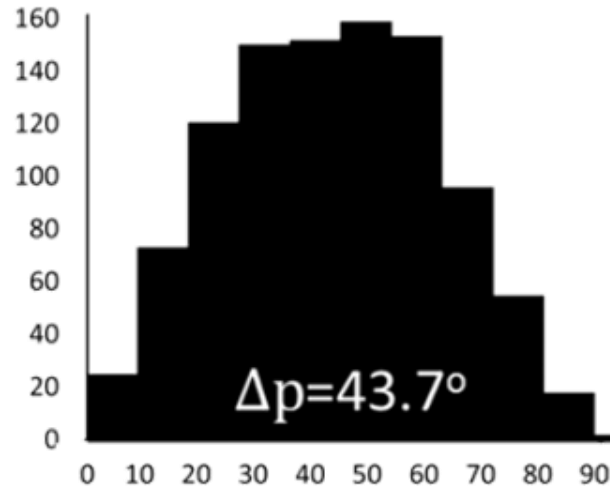
We test the null hypothesis using the Kolmogorov-Smirnov statistic at the 5% level of confidence

All models configurations produce  $\Delta p$  distributions that allow us to reject the null hypothesis at 5% confidence level

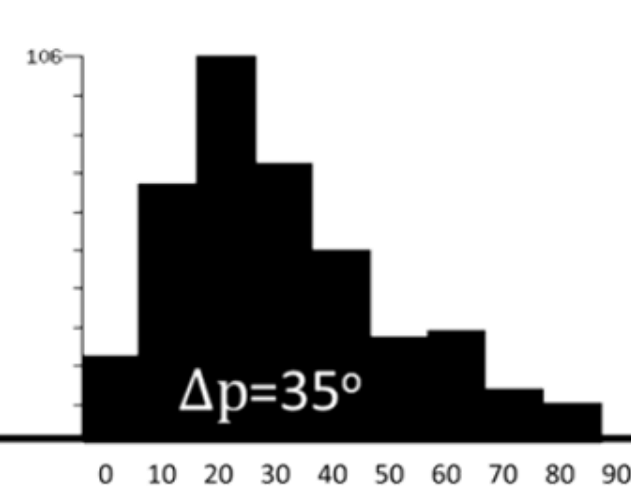
However, orientation mismatch is greatest when salt is excluded and least with full-effect of local salt with uplift and subsidence



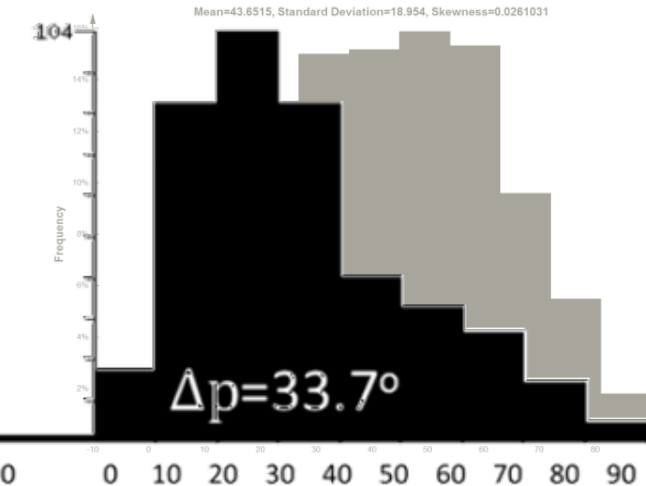
(a) Base case (random distribution)



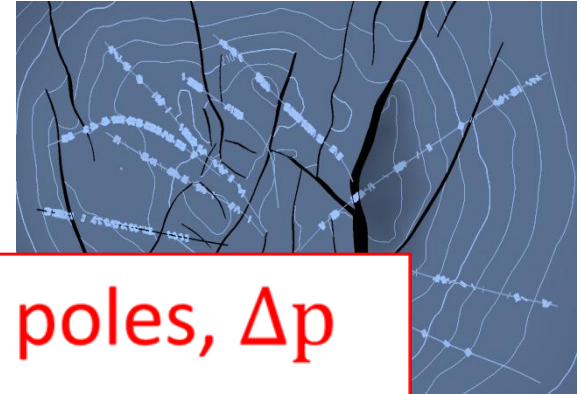
(b) Faults only



(c) Best case (salt included)



All models configurations produce  $\Delta p$  distributions that allow us to reject the null hypothesis at 5% confidence level

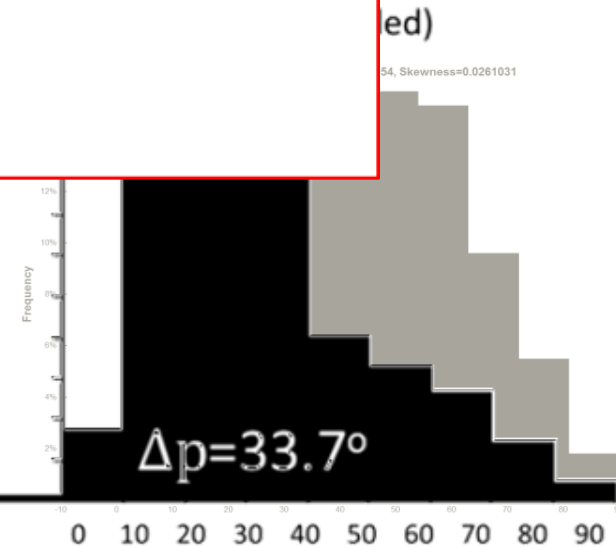
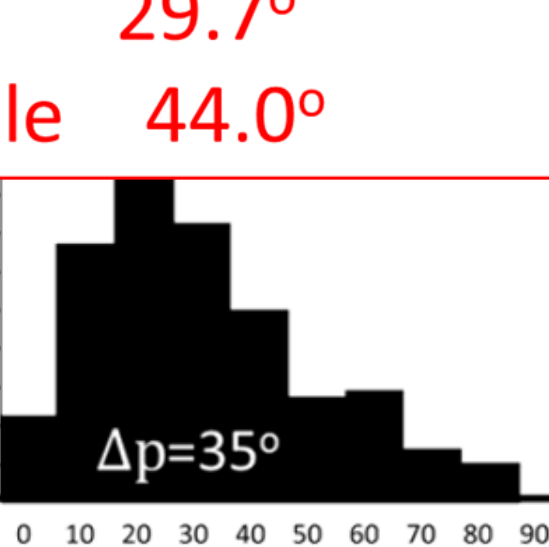
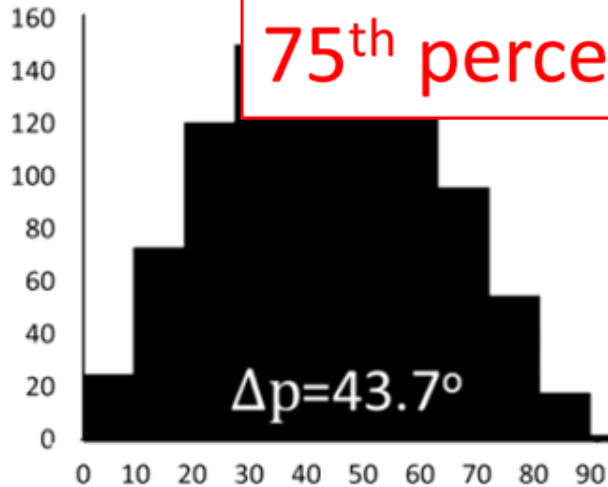


However, salt is excluded with uplift

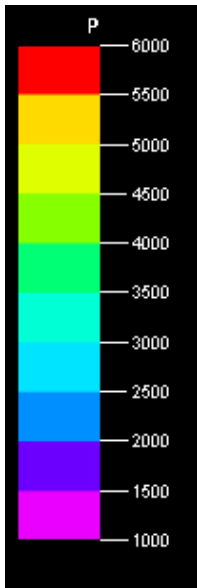
**Angular difference between poles,  $\Delta p$**

mean	33.7°
median	29.7°
75 <sup>th</sup> percentile	44.0°

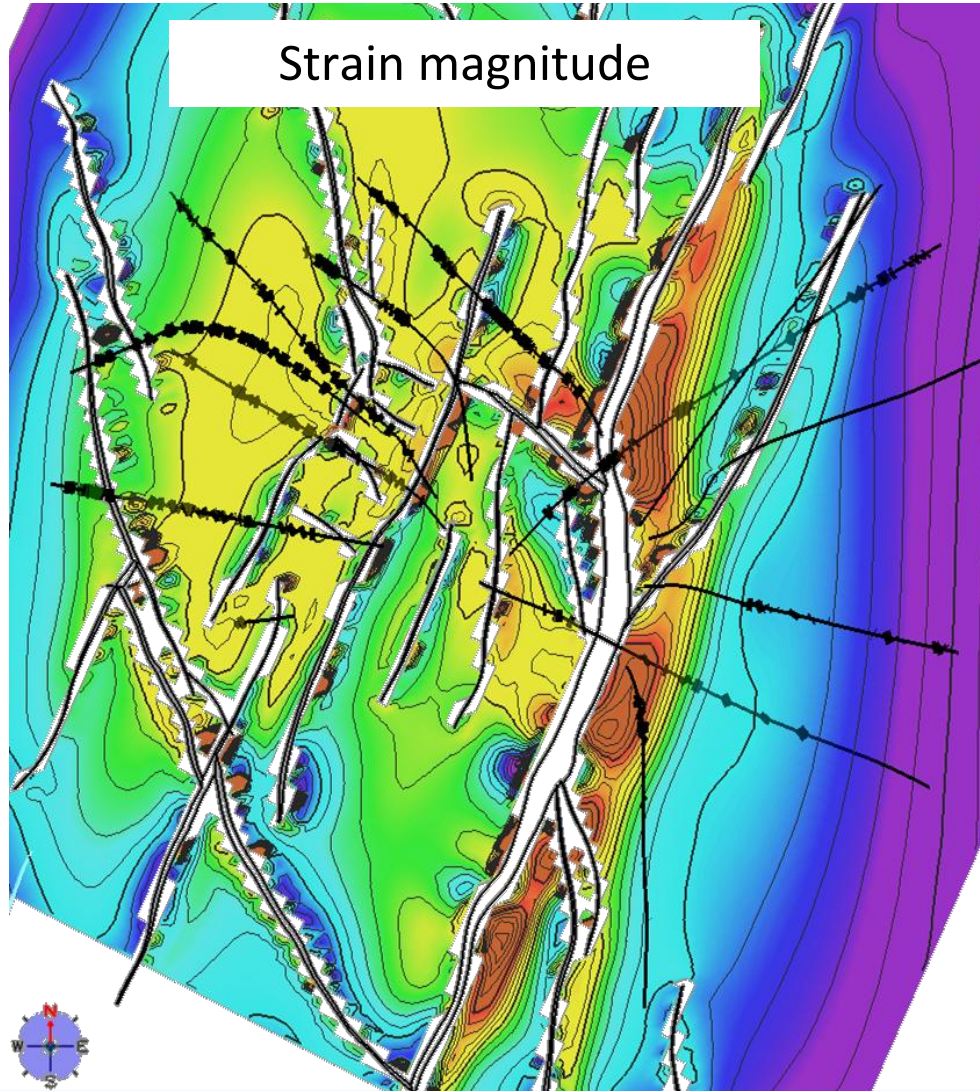
(a) Base case



Densely fractured hot areas,  
sparsely fractured cold



Pore fluid pressure (psi). Virgin pressures between 4000 psi and 4500 psi

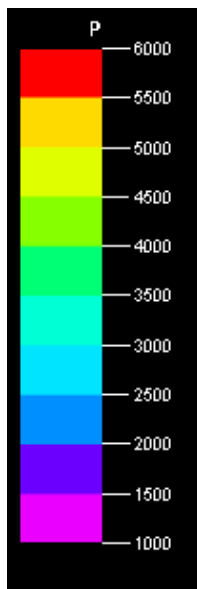


Well tracks with logged major faults/fractures

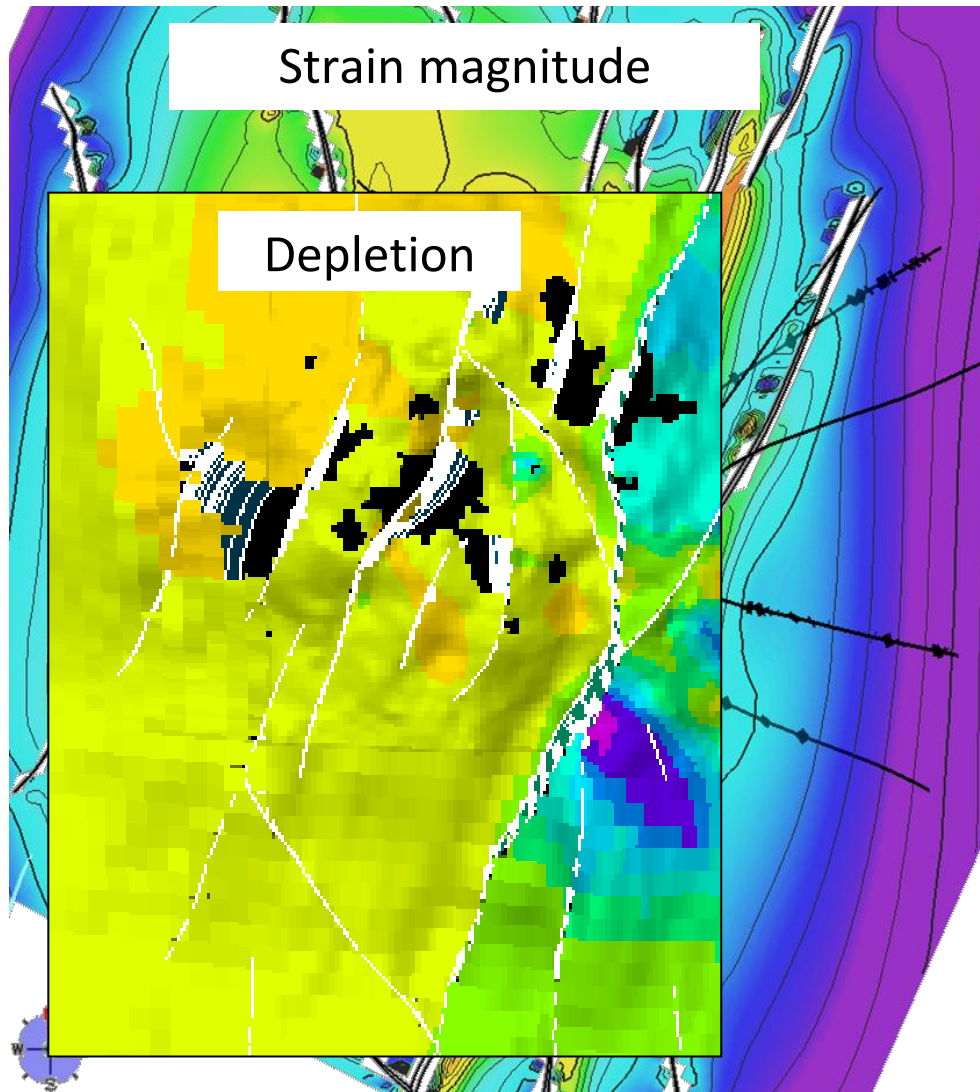
Flipping between the two image there is a clear and strong correspondence between depletion (blue) and high strain magnitude (red)



Densely fractured hot areas,  
sparsely fractured cold



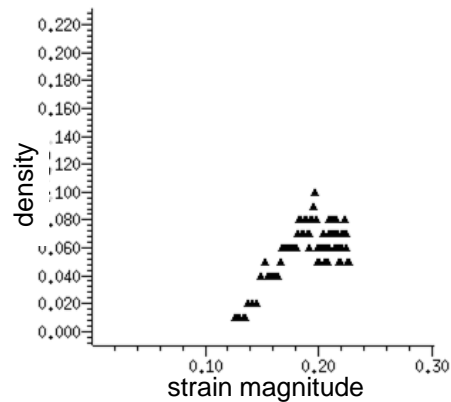
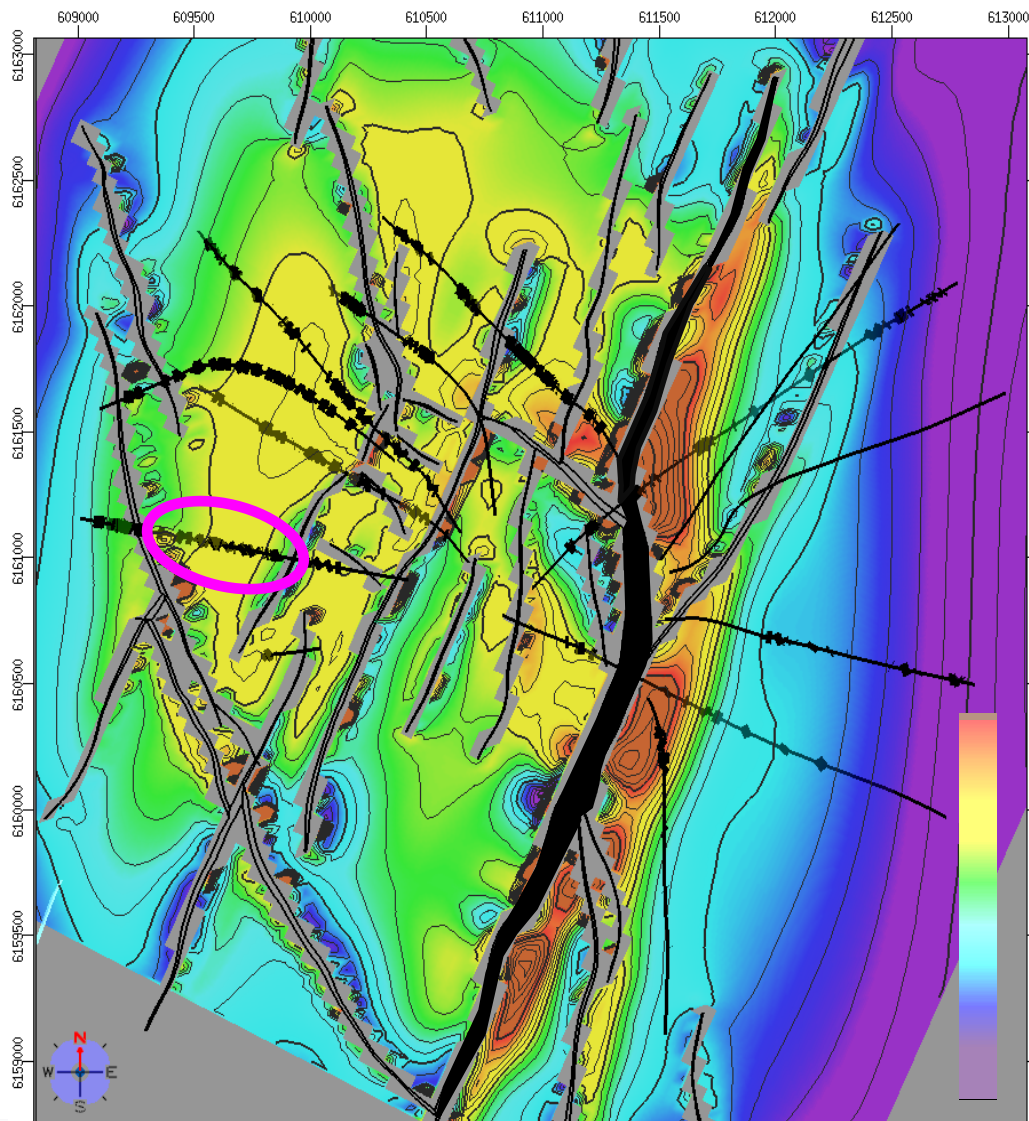
Pore fluid pressure (psi). Virgin pressures between 4000 psi and 4500 psi



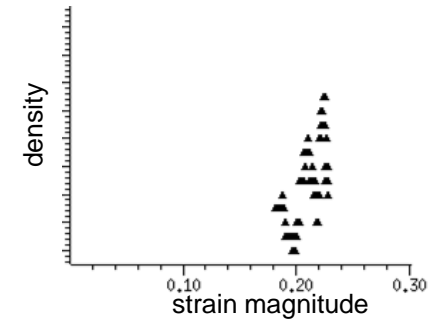
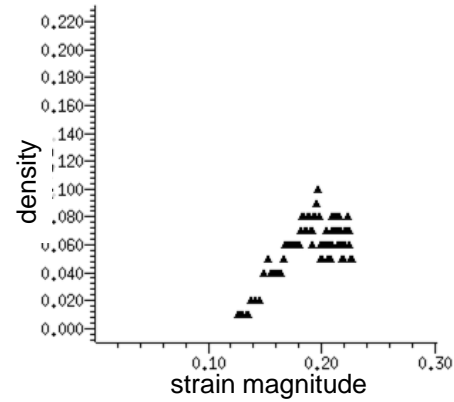
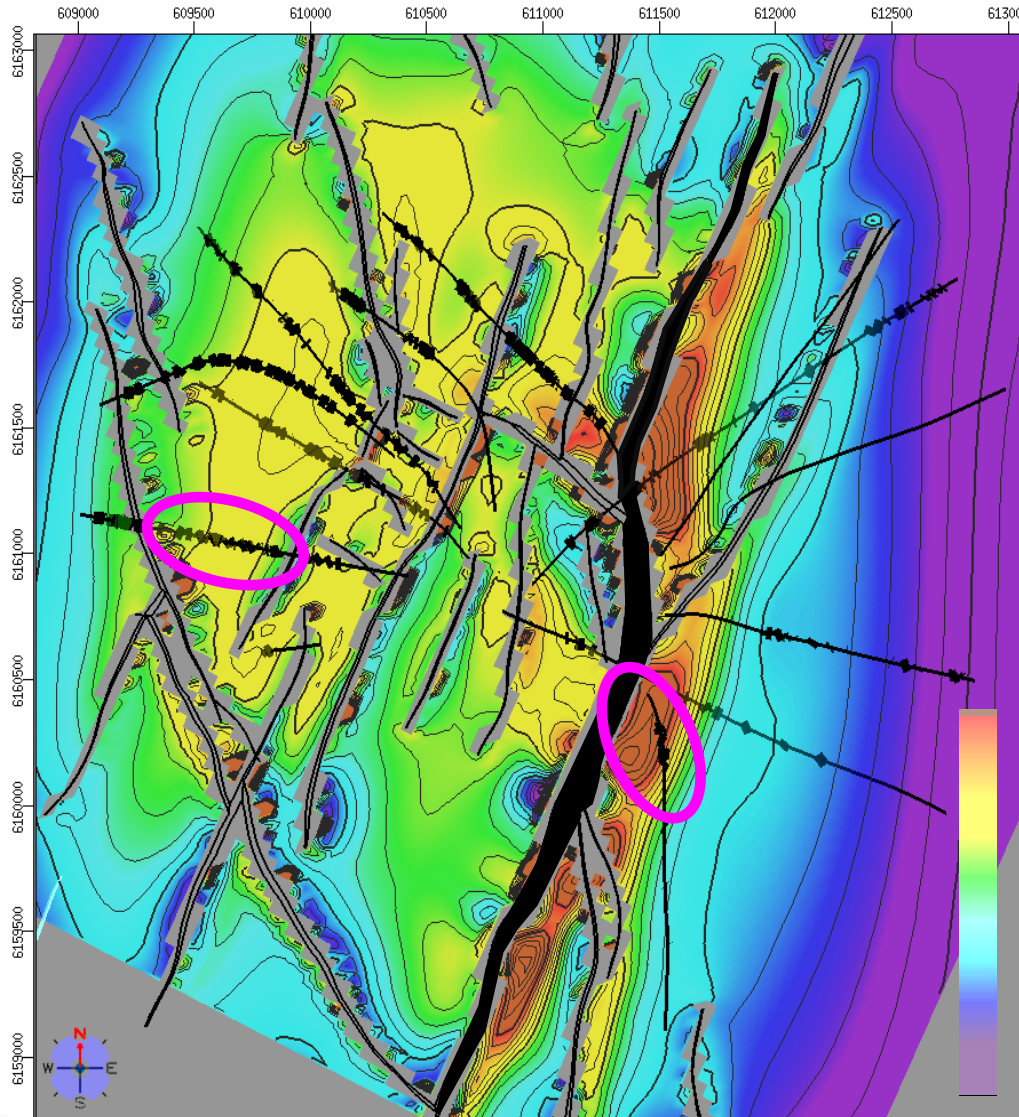
Well tracks with logged major faults/fractures

Flipping between the two image there is a clear and strong correspondence between depletion (blue) and high strain magnitude (red)

# Fracture density calibration, local domains



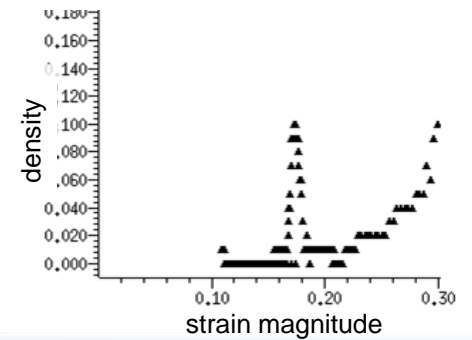
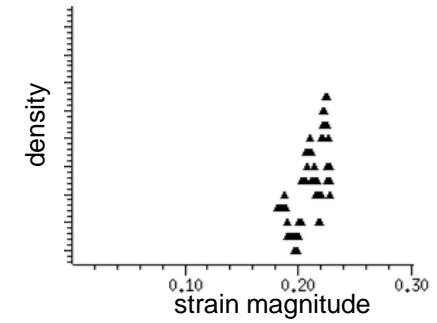
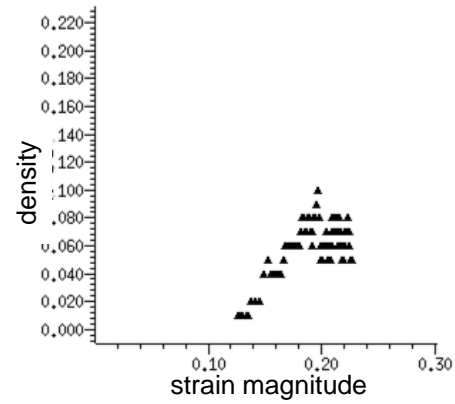
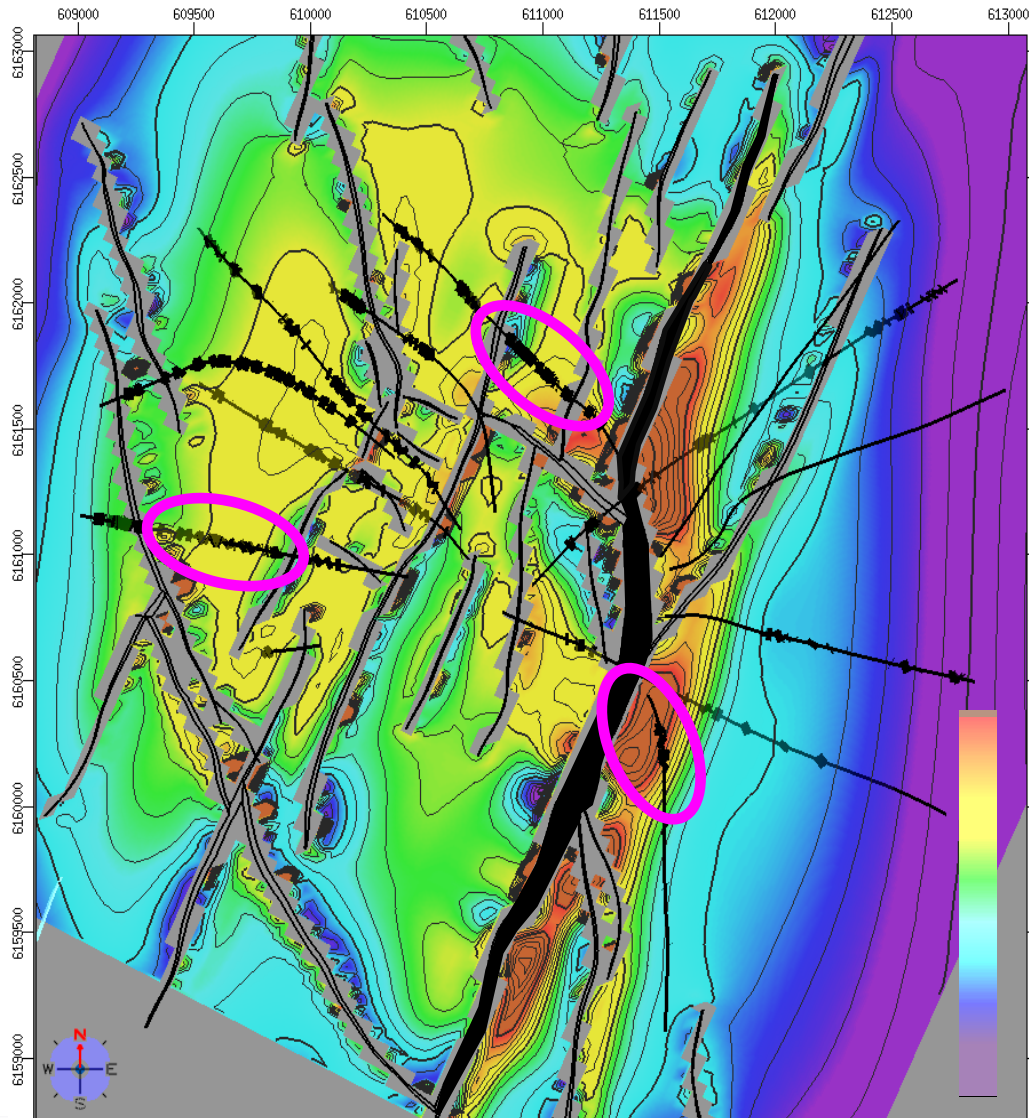
# Fracture density calibration, local domains



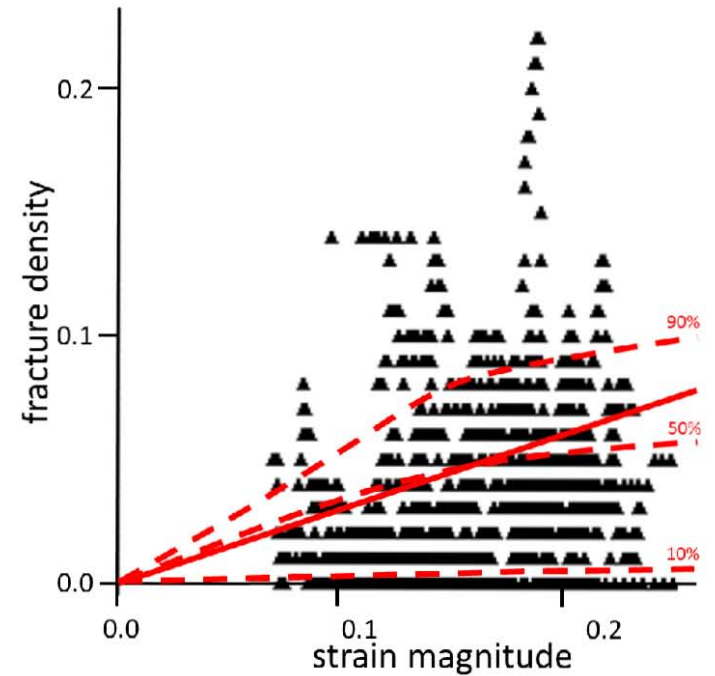
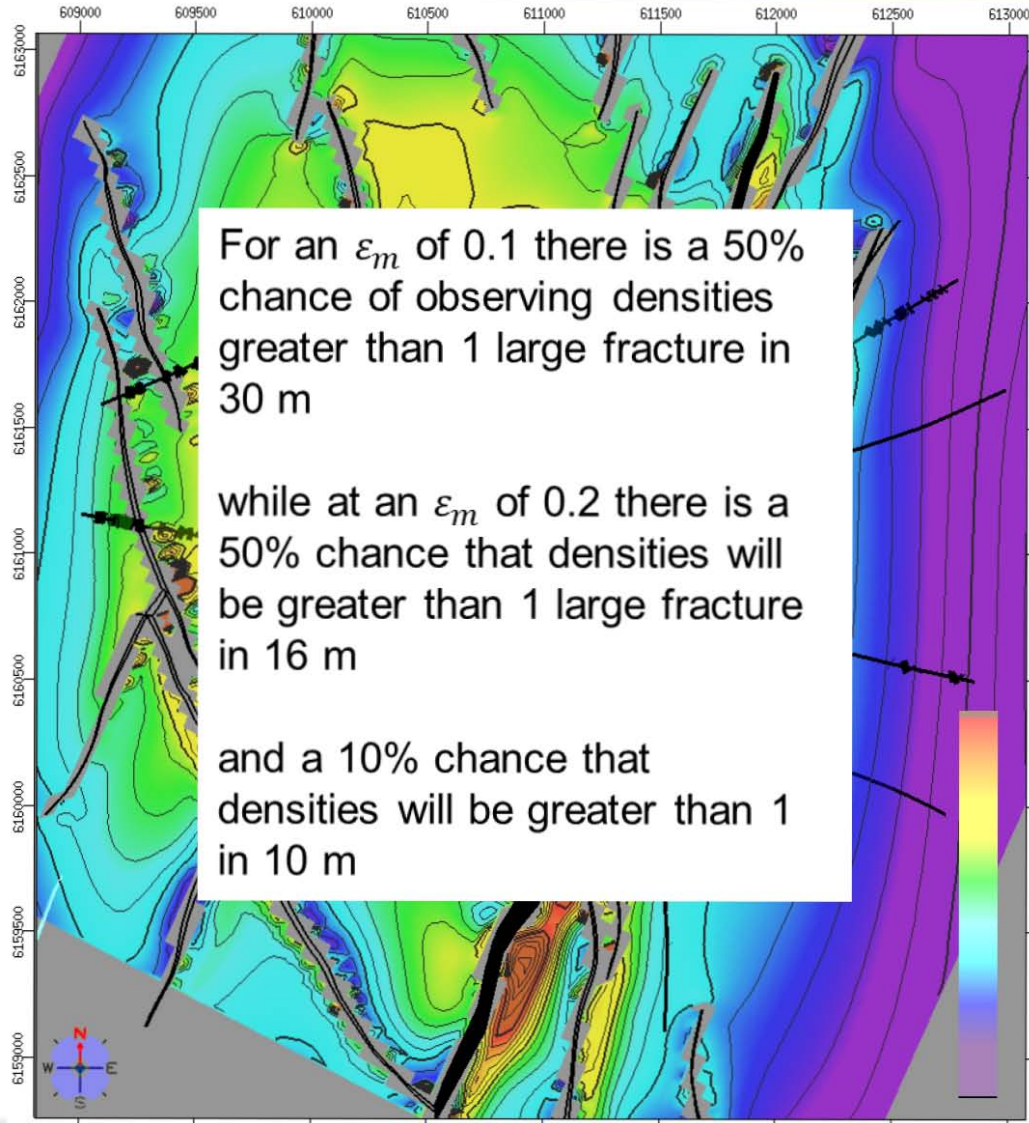


T SEVEN

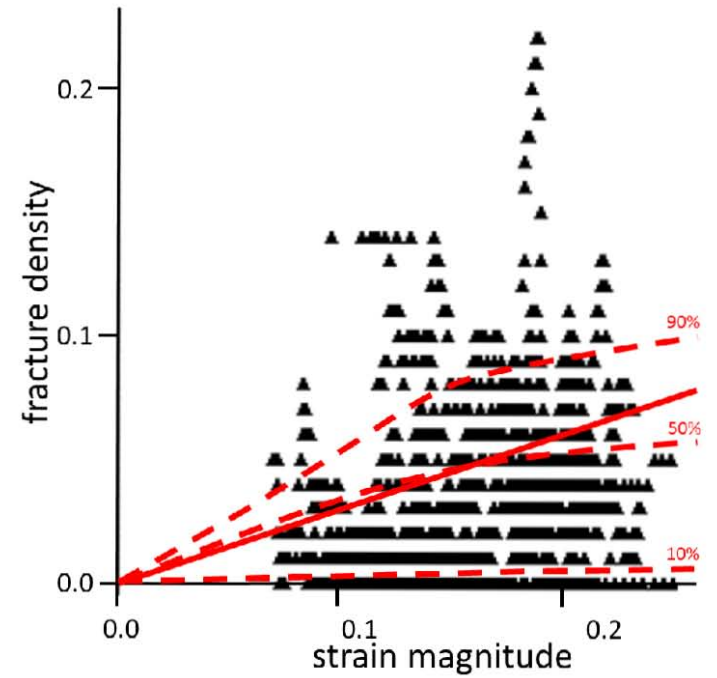
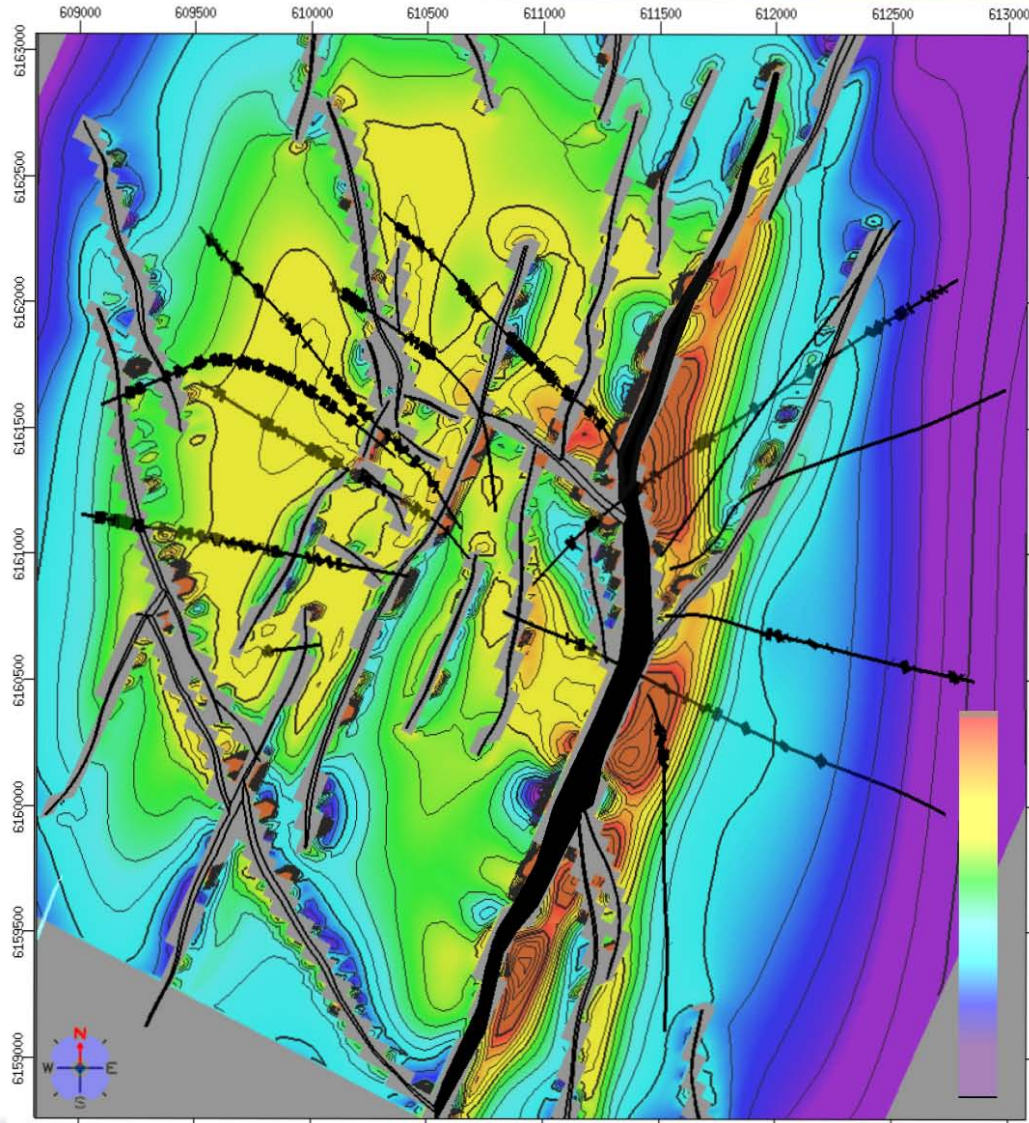
# Fracture density calibration, local domains



# Fracture density calibration, all domains



# Fracture density calibration, all domains



- Strains calculated from an ED model incorporating faults and salt interface as mechanical boundaries correlate with natural fracture orientation and natural fracture density
- Quantitative comparison from 13 wells shows statistically significant correlations between observed and predicted fracture orientations with the median  $\Delta p$  less than  $30^\circ$  and 75% of  $\Delta p$  less than  $44^\circ$
- Given a broad range of model configurations and other sensitivities the unadulterated geometry derived from the validated mapping is our preferred model
- Our strain magnitude maps correlate with reservoir depletion maps
- Some individual structural domains exhibit nearly linear correlations with observed fracture density – the relationship in some others is less simple
- Collecting data from all domains gives a useful predictive overview showing that the highest observed densities occur at the highest strain magnitudes and that high densities will not be observed at low strain magnitudes