

Rock Physics Driven Seismic Modeling of CO₂ Injection in a Carbonate Reservoir from Canada*

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Abstract

Monitoring CO₂ injection for enhanced hydrocarbon recovery in carbonate reservoirs poses a technical challenge interpreting changes in pressure and fluid saturations away from wells. The present study focuses on quantitative rock physics modeling of time-lapse (4D) changes in reservoir pressure and multi-fluid saturations in a carbonate reservoir from southern Canada. The field is currently under WAG (Water Alternate Gas) injection, and both pressure and CO₂ saturation change during the CO₂ flooding process. The goal of the dynamic reservoir modeling is to understand and predict CO₂ saturations over the reservoir. To achieve this goal, we modeled reservoir properties at different fluid saturations with various effective pressure regimes. 4D rock physics analysis provides the link between dynamic reservoir properties and 4D seismic responses. We calculated elastic properties of fluid mixtures (brine, oil, and CO₂) at different pressures, based on a constant reservoir temperature of 600 deg C, as the WAG injection does not significantly alter temperatures in the reservoir. Initially, effective properties of the brine saturated reservoir are measured at the original pressure (15 MPa). Then we replace the brine fluid with a different mixture of fluids and calculate effective properties of the reservoir at different expected pressure values. These elastic properties (incompressibility and rigidity) are affected by changes in the pressure for the same fluid saturation. Modeling results show a significant change (around 30-40% decrease) in the impedance for fluid saturation when the reservoir is saturated with CO₂ compared to the brine-saturated case. 4D rock physics models demonstrated that, at reservoir level, Lambda-Rho highly correlate with changes in fluid saturation, with lowest values when the reservoir is saturated with CO₂. Likewise, Mu-Rho, highly correlated with reservoir pressure, is higher as the effective pressure increases. During WAG injection, it is expected that changes in CO₂ saturation are more prominent compared to changes in effective pressure away from injection wells.

Selected References

Churcher, P.L., and A.C. Edmunds, 1994, Reservoir characterization and geological study of the Weyburn Unit, southeastern Saskatchewan: Report Number 1, Proposed Miscible Flood, Horizontal Well, and Waterflood Optimization Areas: Internal report prepared for PanCanadian Petroleum Ltd., 28 p.

Dietrich, J.R., and D.H. Magnusson, 1998, Basement controls on Phanerozoic development of the Birdstail-Waskada salt dissolution zone, Williston Basin, southeast Manitoba: 8th Int. Williston Basin Symp., SGS Special Pub. No. 13, p. 166-174.

Wegelin, A., 1984, Geology and reservoir properties of the Weyburn Field, southeastern Saskatchewan, *in* J.A. Lorsong and M.A. Wilsons, eds., Oil and Gas in Saskatchewan: Saskatchewan Geological Society Spec. Pub No. 7, p. 71-82.



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Ikon Science Americas

02 June 2015

The Present And Future
Of GeoPrediction

Outline

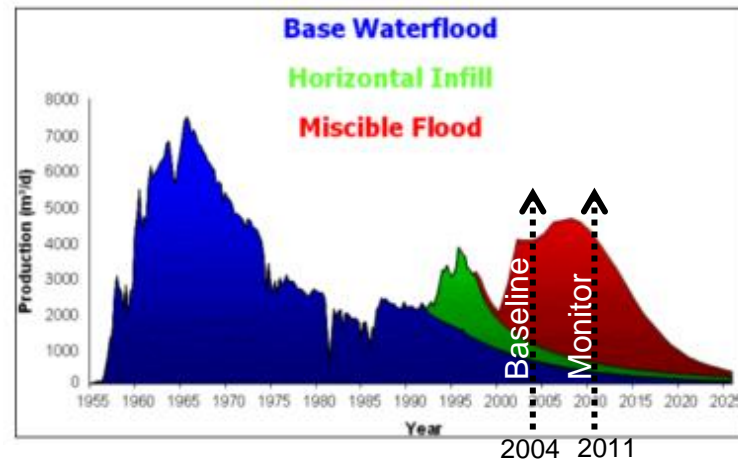
1. Introduction & Challenges
2. Rock Physics Modeling
3. Forward Seismic Modeling
4. Conclusions



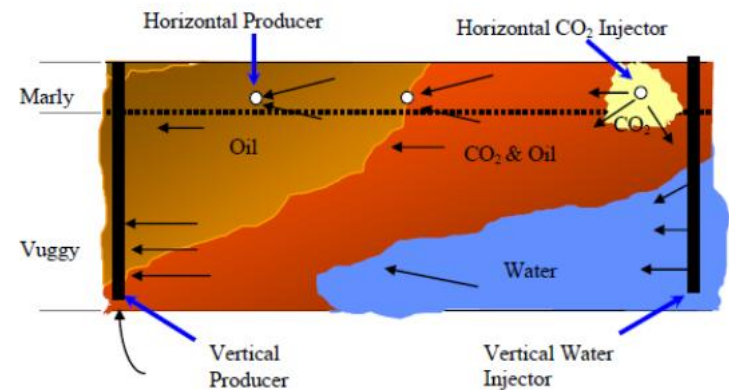
1. Introduction & Challenges



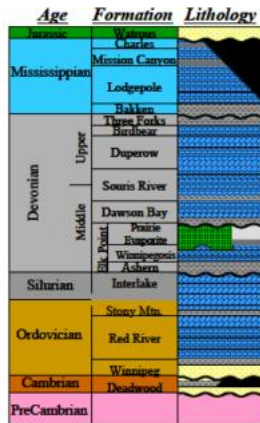
Weyburn Field



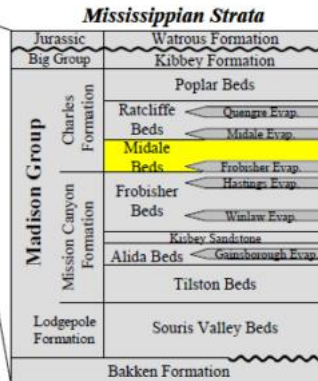
- Discovered in 1954
- Horizontal infill drilling started in 1991
- CO₂ injection started in 2000
- Seismic: Baseline (2004) & Monitor (2011)
- IOIP: 1.4 billion barrels



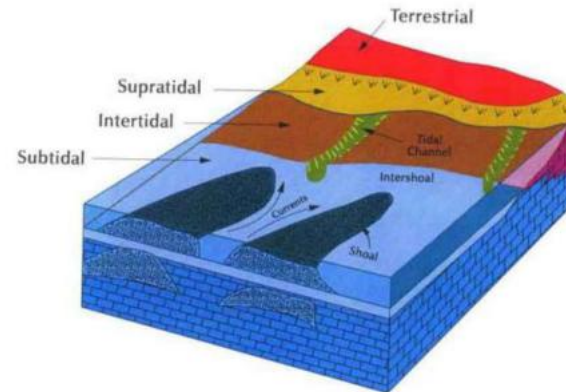
Weyburn Field – Petroleum System



(Dietrich and Magnusson, 1998)



(Wegelin, 1984)

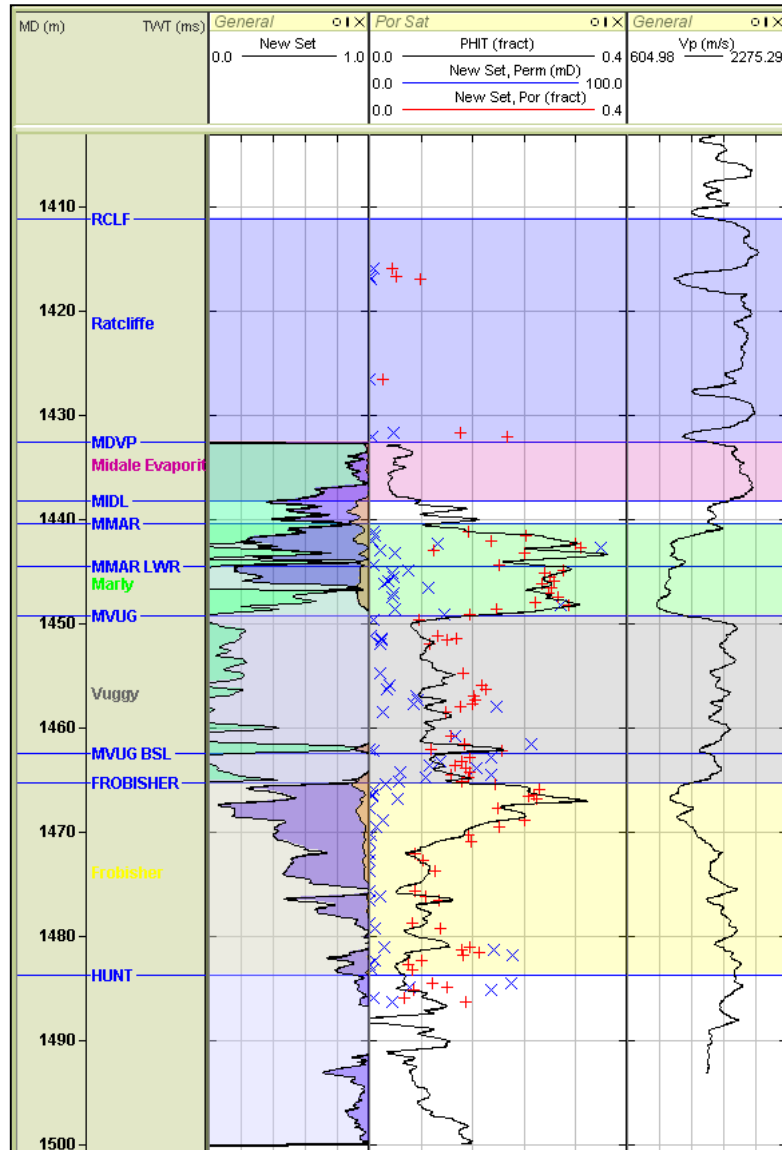


(Churcher and Edmunds, 1984)

Midale
Depositional
Environment

- Midale beds of the Mississippian Charles formation were formed during transgression-regression sequence.
- The Midale reservoir beds were deposited in a shallow carbonate shelf environment. The carbonate reservoir has been subdivided into the Marly dolostone and the Vuggy limestone.
- The Bakken shale is a possible source rock for the medium gravity crude oil at Weyburn field.
- The petroleum trap is both hydrodynamic and stratigraphic (Churcher and Edmunds, 1994).

Log – Core porosity calibration



+ Core porosity
X Core permeability

Ratcliffe
(Dolomite+Evaporites)

Midale Evaporite

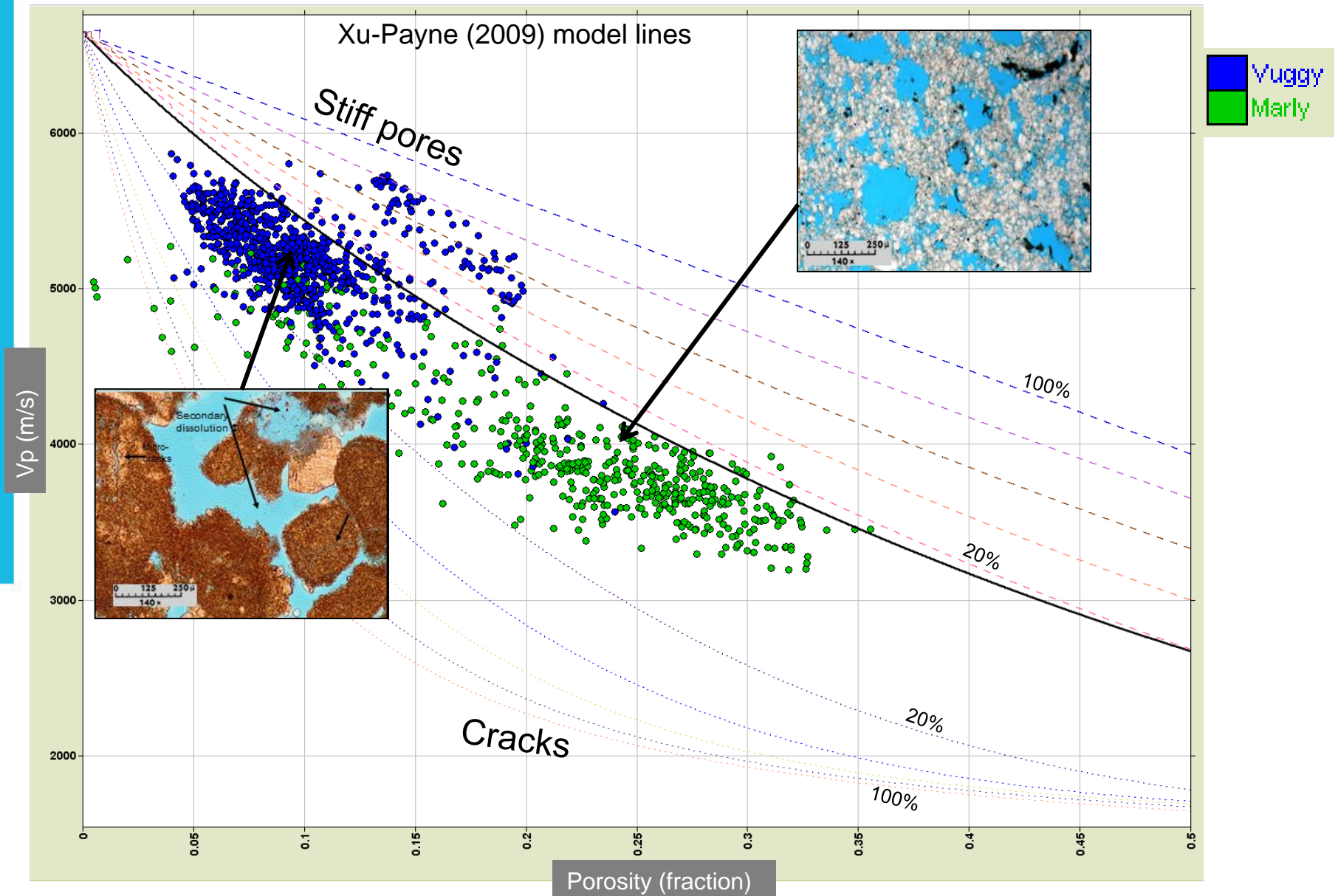
Midale Marly Dolomite
(Permeability: 1-50mD)

Midale Vuggy Limestone
(Permeability: 10-300mD)

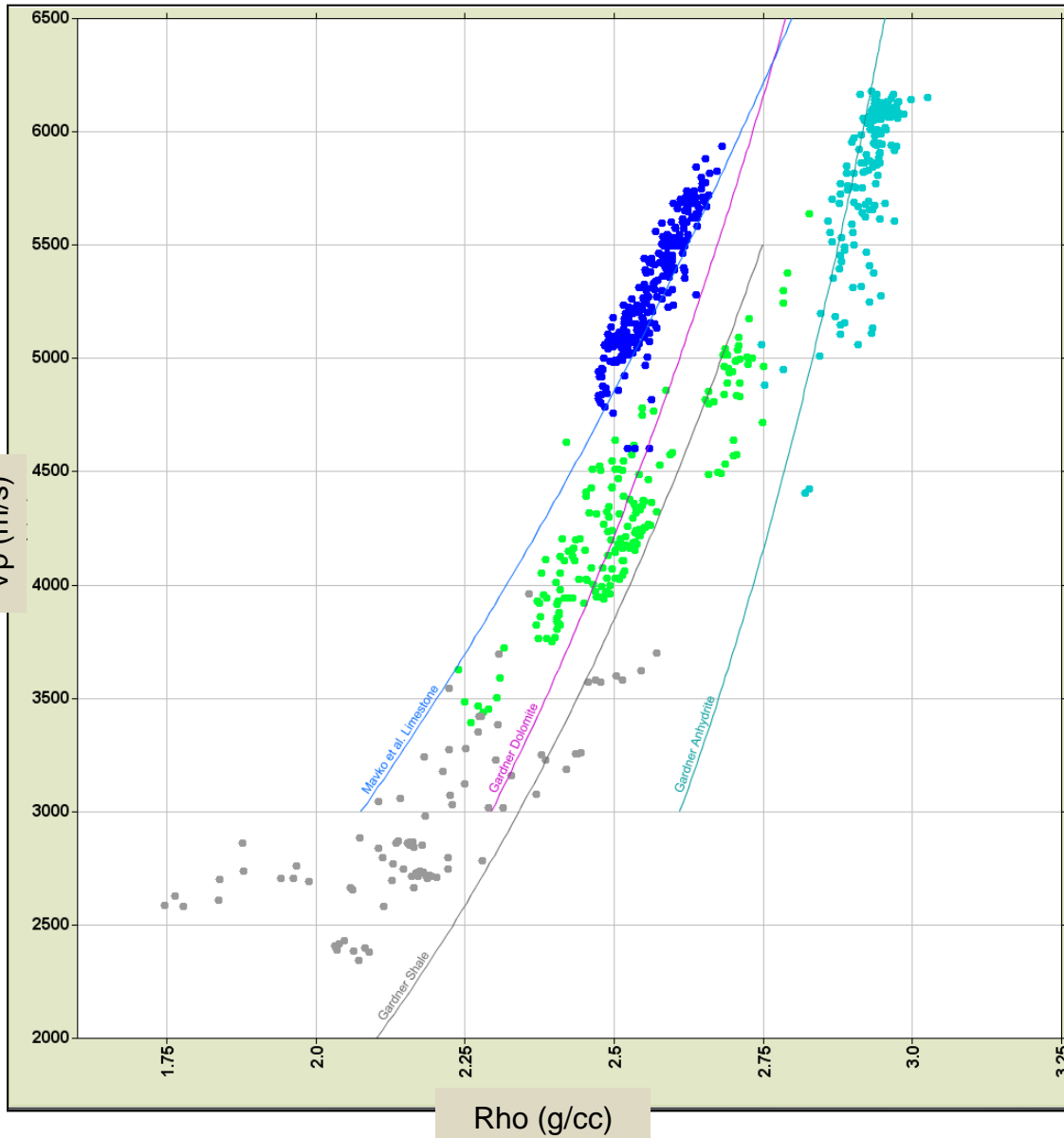
Frobisher

Good calibration
between log and core
porosities

Vp vs. Porosity



QC for lithofacies



Anhydrite	
Calcite	
Dolomite	
Illite	

2. Rock Physics Modeling

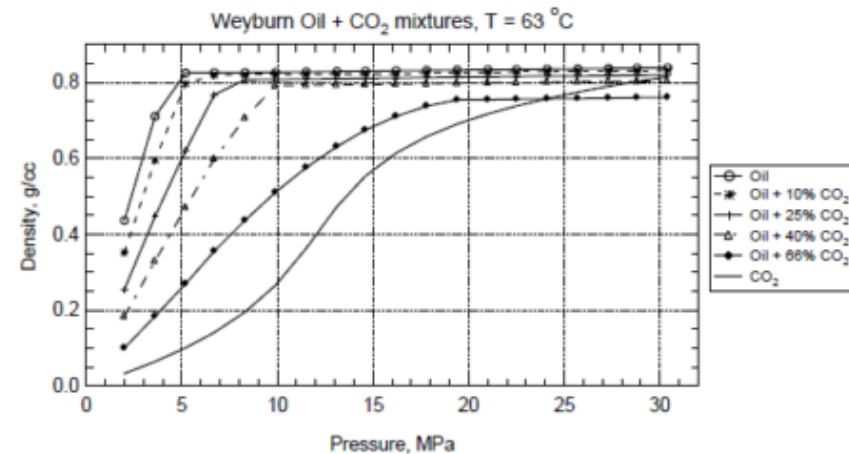
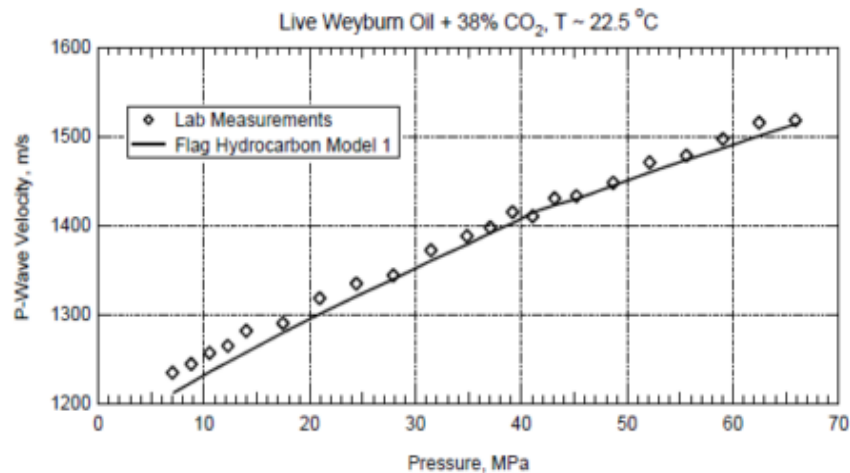


Fluid/Pressure Modeling Assumptions

Due to a lack of data, many assumptions needed to be made in order to perform the 4D fluid and pressure modelling. These are detailed below:

- That the baseline reservoir pressure was 15MPa. This assumption was based on a hydrostatic gradient with no overpressure effects.
- That baseline water salinity was 85000ppm while monitor salinity was 100000ppm.
- Baseline Oil API was 29API, Monitor was 27API
- Temperature was constant throughout at 60 degrees.
- The fluid properties for water, oil and CO₂ were calculated using FLAG
- Values for mixed miscible CO₂ in oil were calculated using Brown's Thesis.

Weyburn EOR reservoir properties



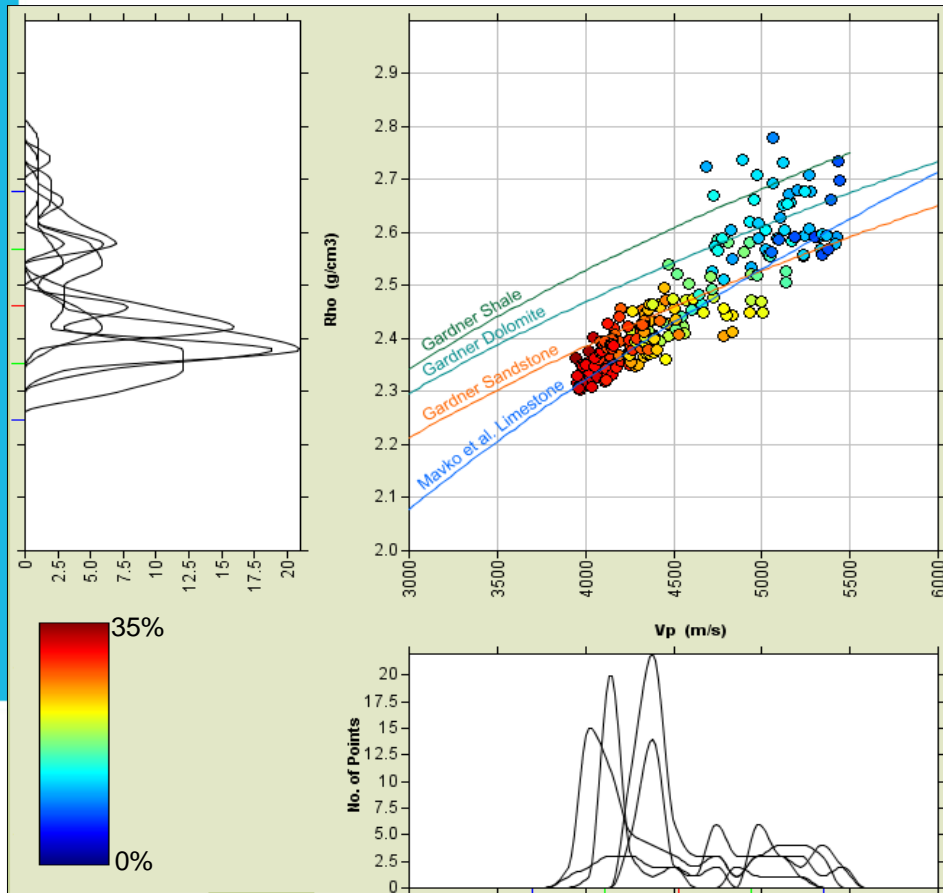
(Brown et al., 2004)

Oil and CO₂ mixture will attain miscibility at pressures of 14 to 17 MPa

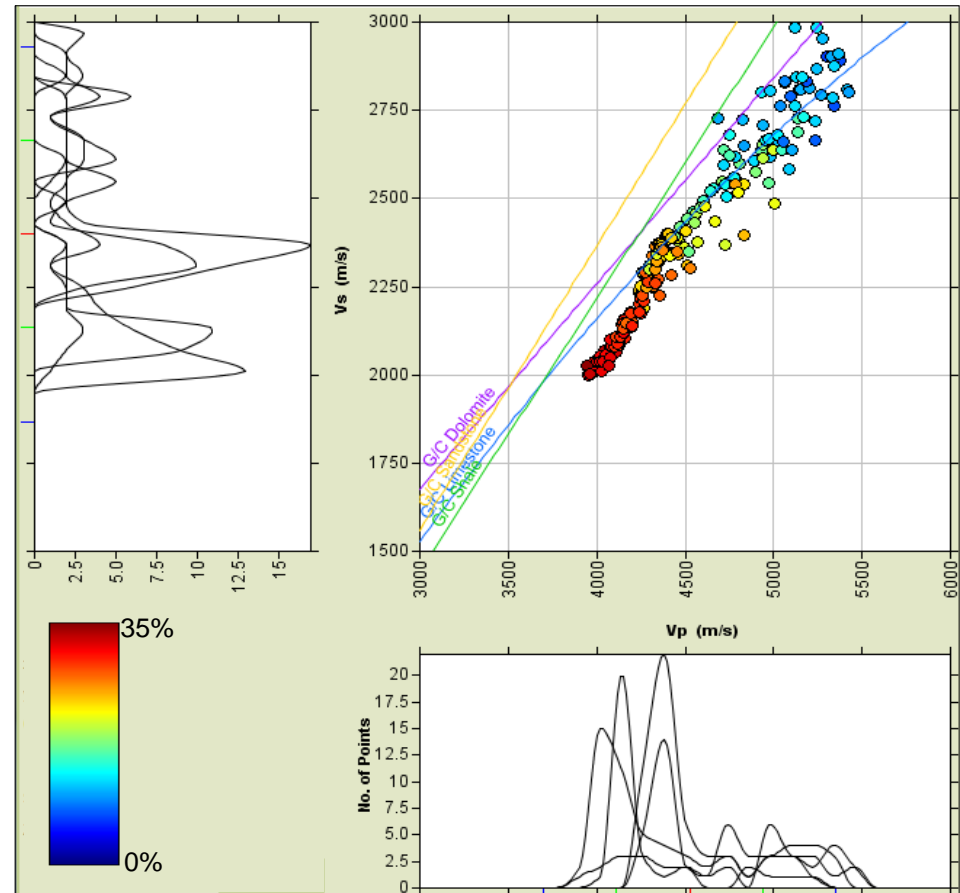
The fluid properties for various mixes of CO₂ and oil were taken directly from Brown's thesis (Brown et al., 2004). The mixes on the graph above were modelled at 5, 10, 15, 20 and 25 MPa.

5MPa (Marly)

Vp vs. Rho



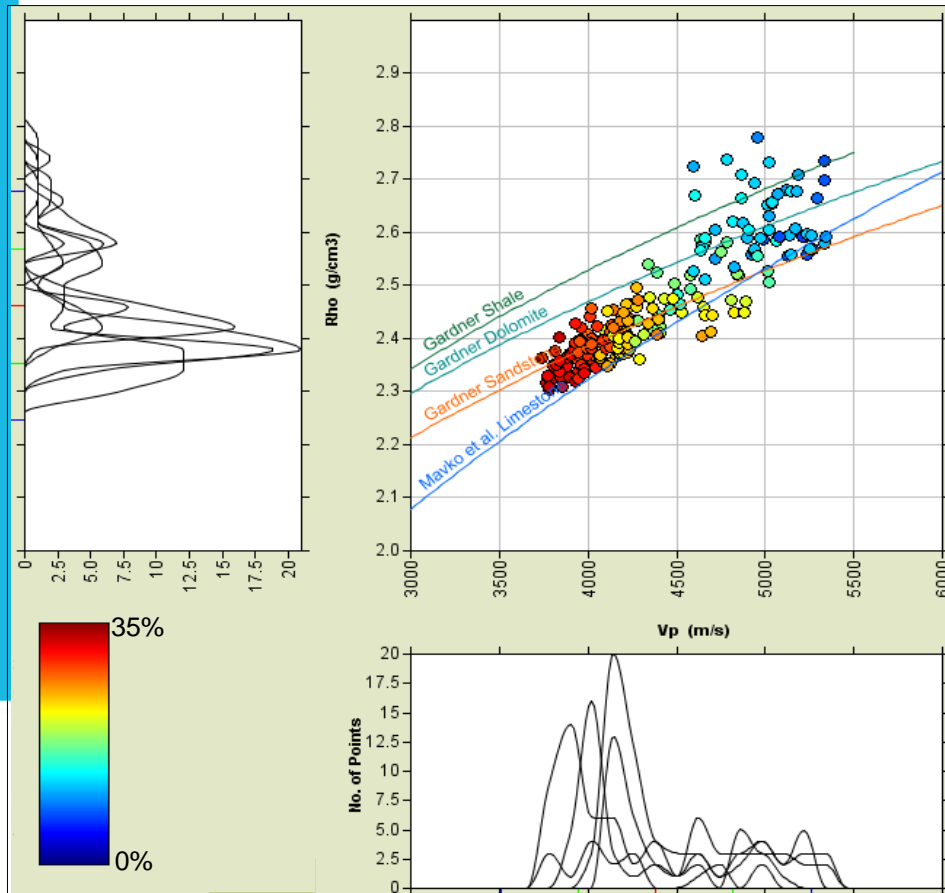
Vp vs. Vs



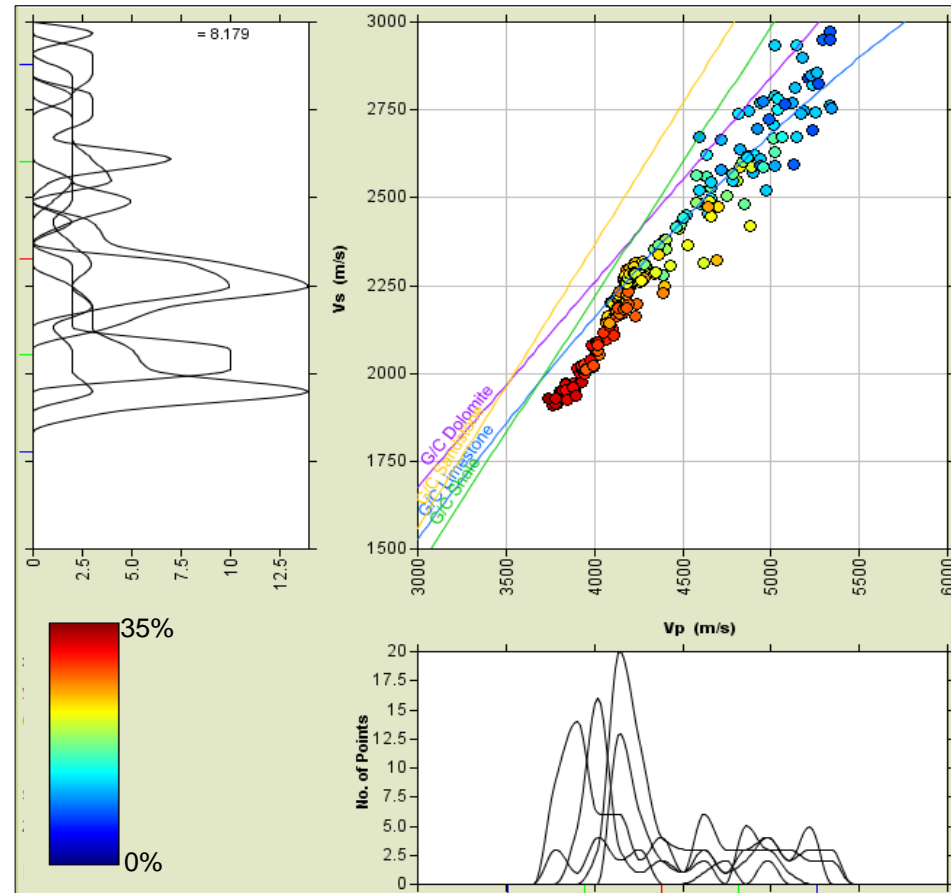
The plot above shows the Marly section data crossplot Vp vs. Rho and Vp vs. Vs. Both plots are coloured by Porosity. In these plots the data have been modulated from the initial in situ conditions to 100% Brine at 5MPa using the monitor fluid properties.

10MPa (Marly)

Vp vs. Rho



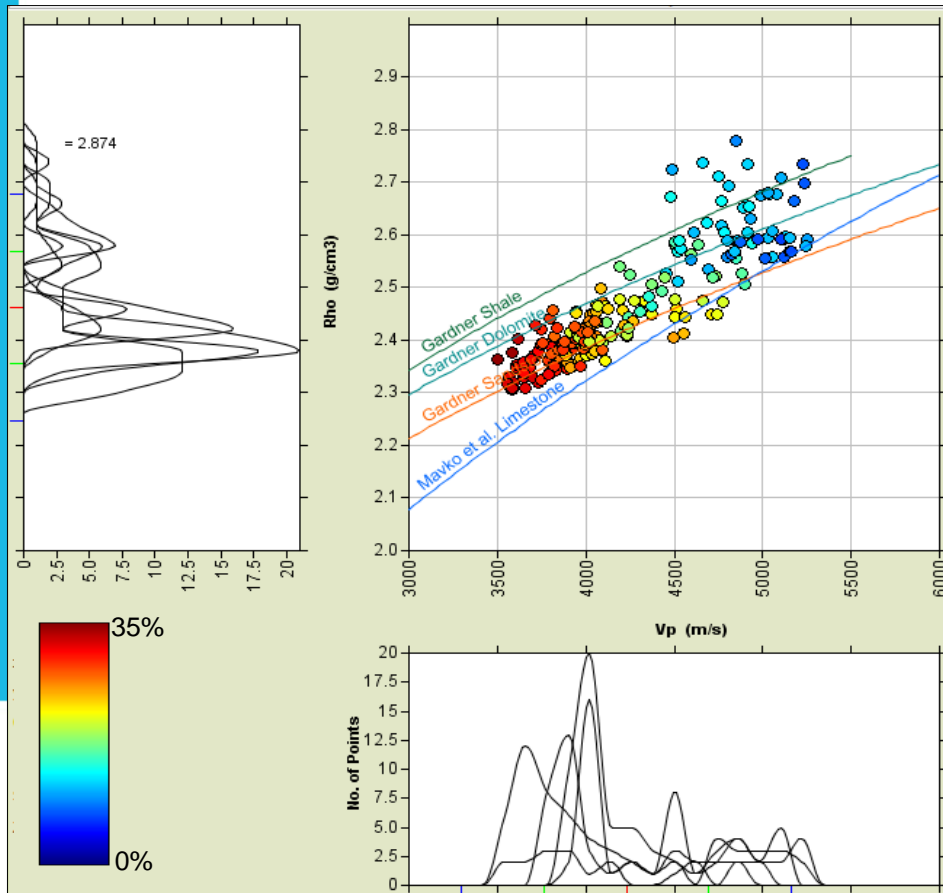
Vp vs. Vs



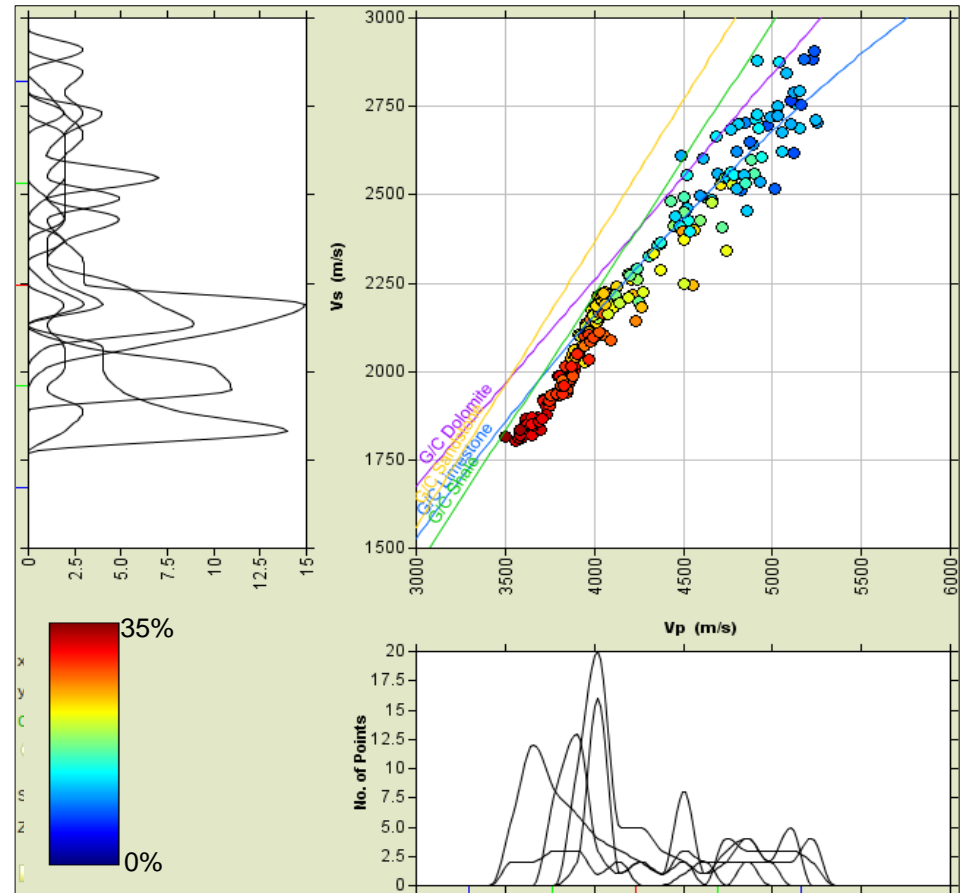
The plot above shows the Marly section data crossplot Vp vs. Rho and Vp vs. Vs. Both plots are coloured by Porosity. In these plots the data have been modulated from the initial in situ conditions to 100% Brine at 10MPa using the monitor fluid properties.

15MPa (Marly)

Vp vs. Rho



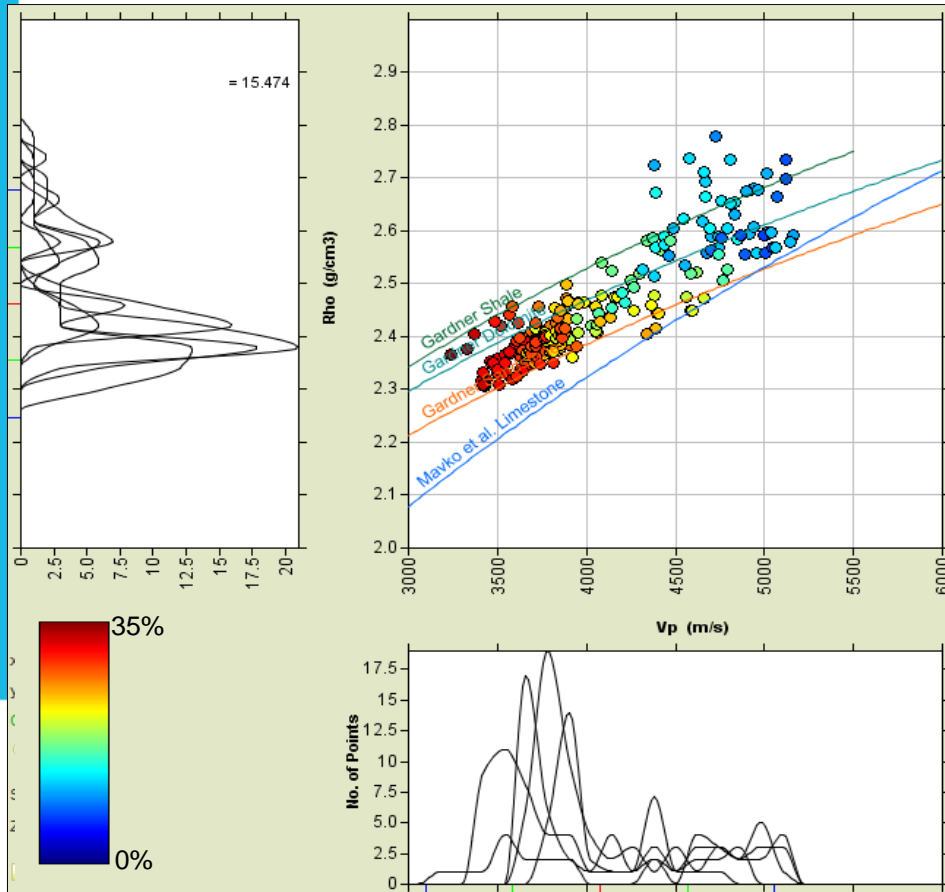
Vp vs. Vs



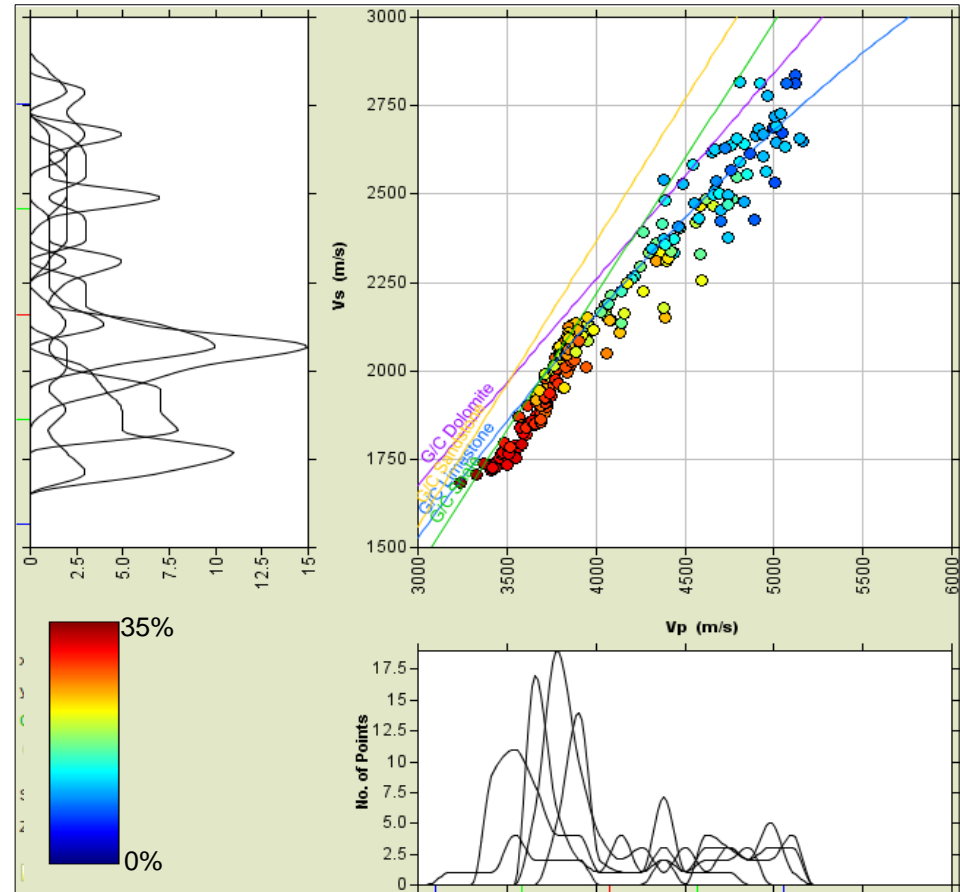
The plot above shows the Marly section data crossplot Vp vs. Rho and Vp vs. Vs. Both plots are coloured by Porosity. In these plots the data have been modulated from the initial in situ conditions to 100% Brine at 5MPa using the monitor fluid properties.

20MPa (Marly)

Vp vs. Rho



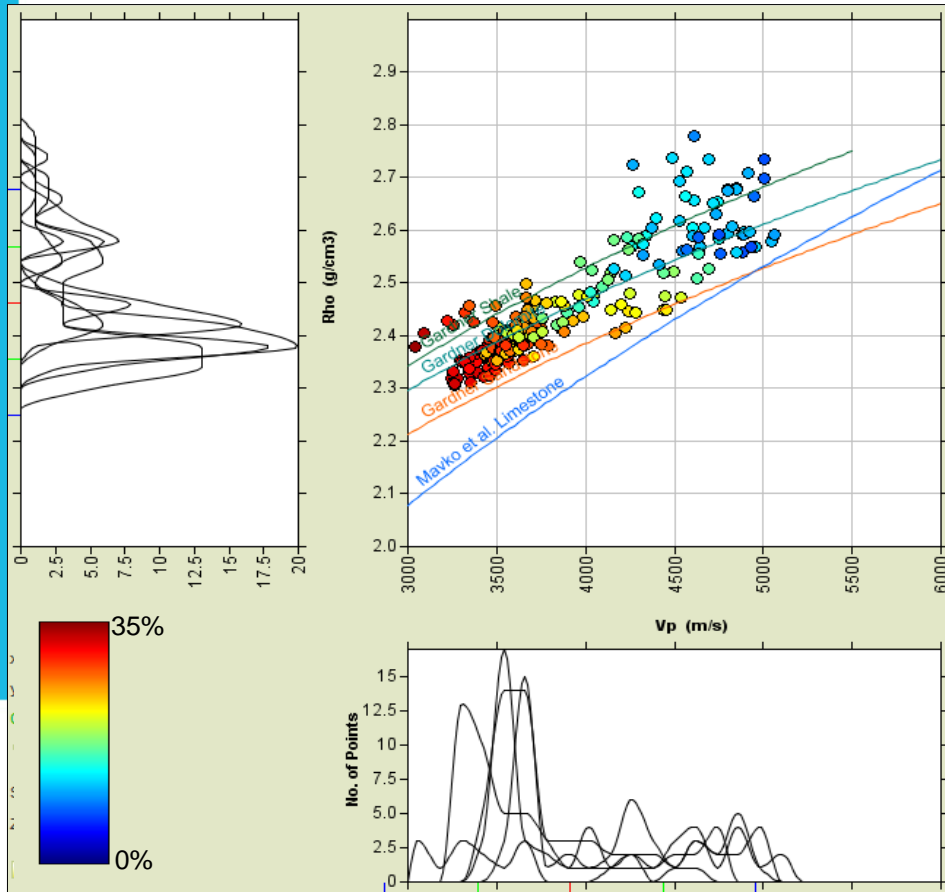
Vp vs. Vs



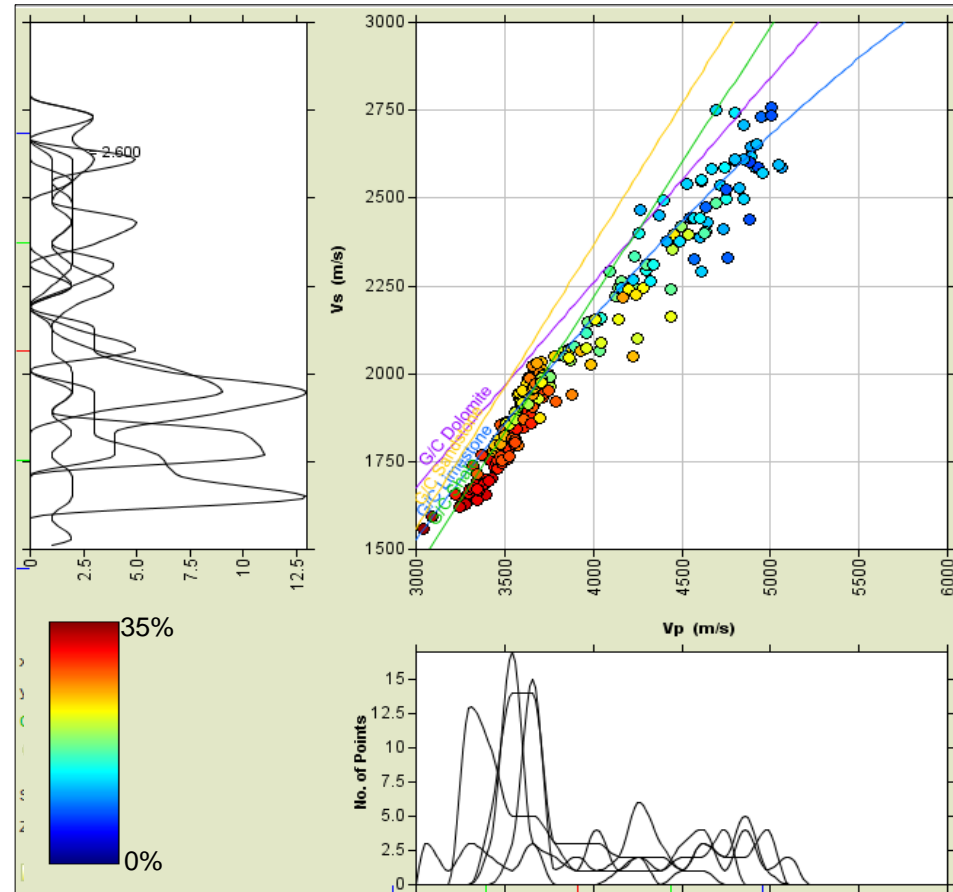
The plot above shows the Marly section data crossplot Vp vs. Rho and Vp vs. Vs. Both plots are coloured by Porosity. In these plots the data have been modulated from the initial in situ conditions to 100% Brine at 5MPa using the monitor fluid properties.

25MPa (Marly)

Vp vs. Rho

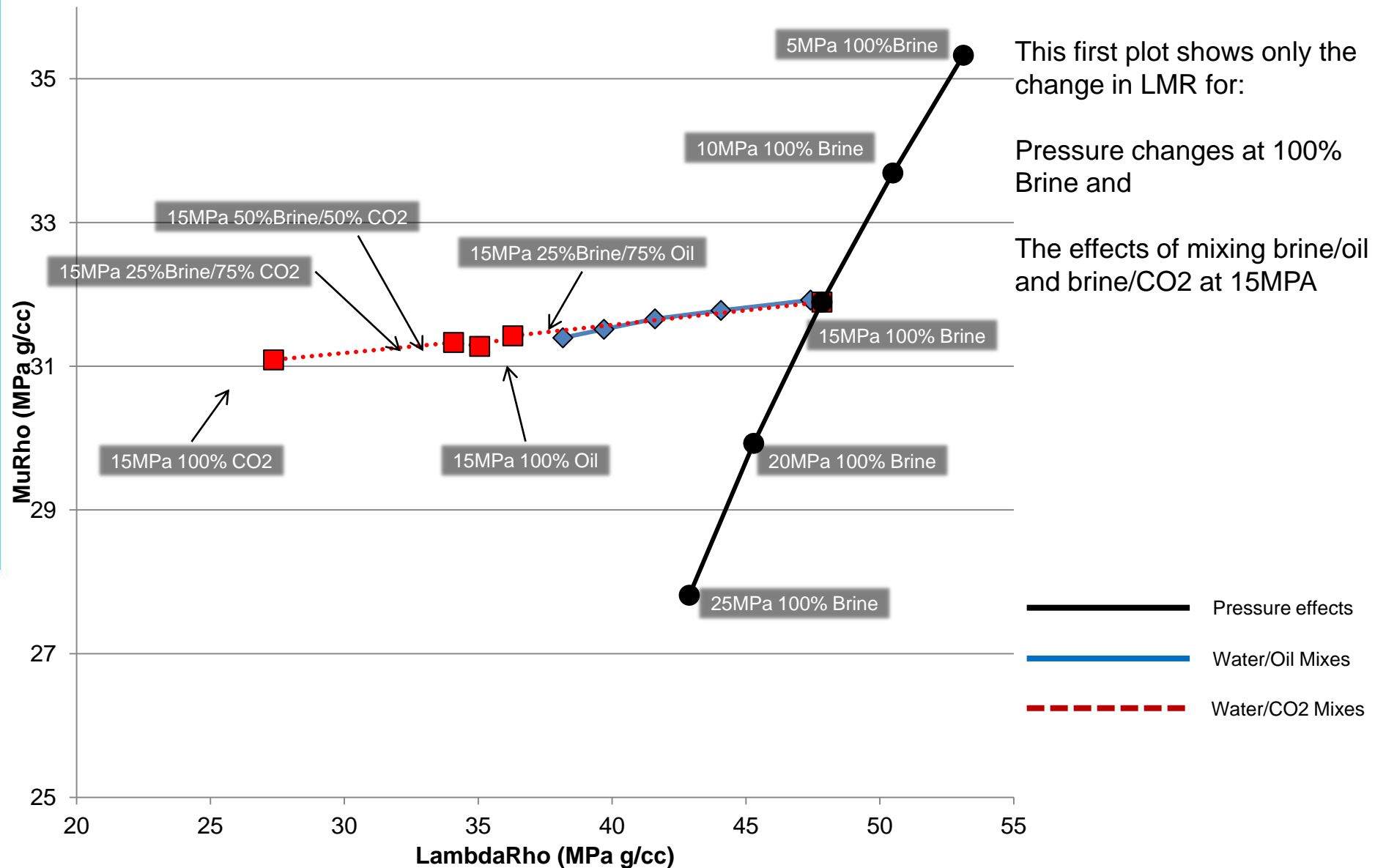


Vp vs. Vs

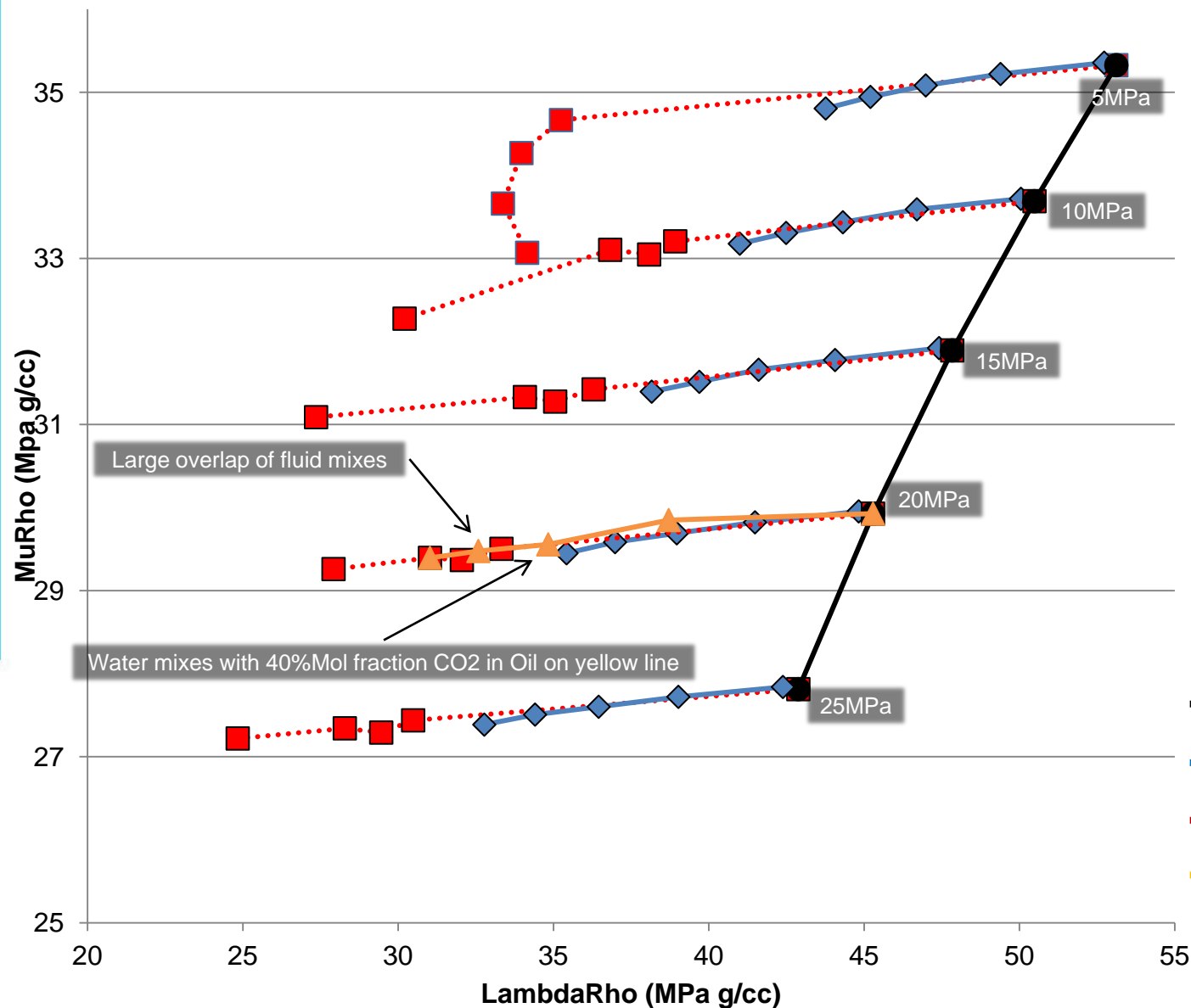


The plot above shows the Marly section data crossplot Vp vs. Rho and Vp vs. Vs. Both plots are coloured by Porosity. In these plots the data have been modulated from the initial in situ conditions to 100% Brine at 5MPa using the monitor fluid properties.

LambdaRho vs. MuRho (Marly)



LambdaRho vs. MuRho (Marly)



Finally a mix of 40% Mol fraction CO2 is added to the plot.

At this point there is no need to increase the complexity of the plot. It can be seen that no matter what percentage of CO2 is mixed into the oil it will always lie between our end member of 100% CO2 and 100% Brine. This was true no matter what impedance space was looked at: AI/SI, AI/GI, LMR, etc.

- Pressure effects
- Water/Oil Mixes
- Water/CO2 Mixes
- Water/Oil plus 40% Mol Fraction CO2 Mixes

3. Forward Seismic Modeling



Reflectivity Analysis

- With the nine fluid-pressure cases, three substitution target scenarios were modeled (3 wells):
 - Marly
 - Vuggy
 - Marly and Vuggy
- Synthetic seismic was produced from these 27 cases (9 cases for each target scenario) using the mid-stack wavelet extracted from the baseline survey
- Measurement events were picked at the maximum negative reflection at the Marly-Overburden interface and at the maximum positive reflection at the Vuggy-Frobisher interface
- The average intercept and gradient as well as percent change (from scenario 4) along these measurement horizons was then cross plotted

Construction of Fluid Mixes

Oil/Water/CO₂ mixes:
background 35% oil and 65% water

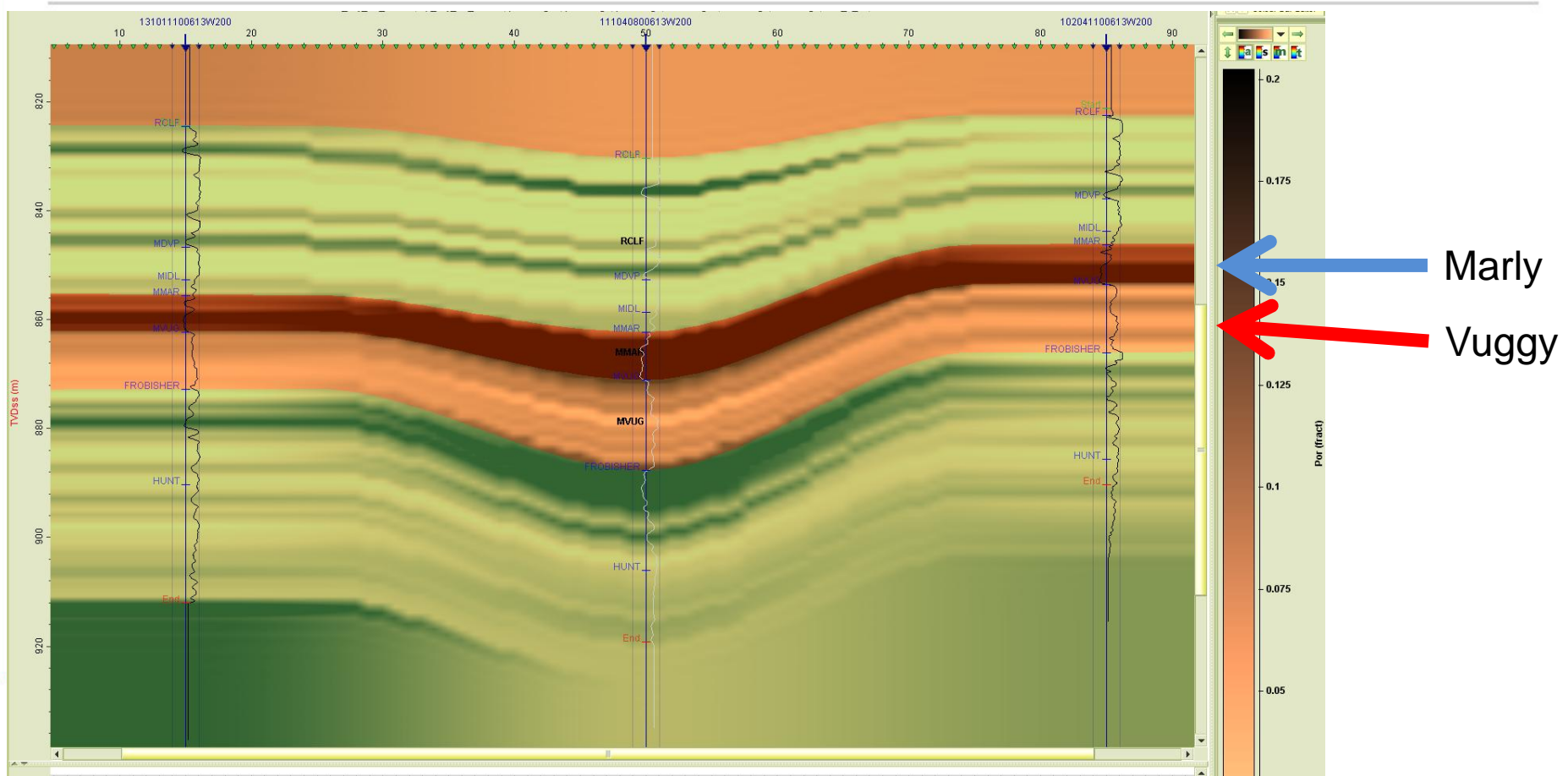
Pp (MPa)	Saturation	Cases 1,4,7 0.0 % CO ₂	Cases 2,5,8 max miscible CO ₂	Cases 3,6,9 90% CO ₂
8 (cases 1-3)	So	0.35	0.35	0.0
	Sw	0.65	0.65	0.1
	Sg	0.0	0.0	0.9
15 (cases 4-6)	So	0.35	0.35	0.0
	Sw	0.65	0.65	0.1
	Sg	0.0	0.0	0.9
20 (cases 7-9)	So	0.35	0.35	0.0
	Sw	0.65	0.65	0.1
	Sg	0.0	0.0	0.9

Pressure Perturbation

Pressure Dependent Fluid Subs

Computed % and absolute difference between Monitor and Baseline

2D Model – Pressure perturbation and Fluid Substitutions applied to Marly and Vuggy bodies



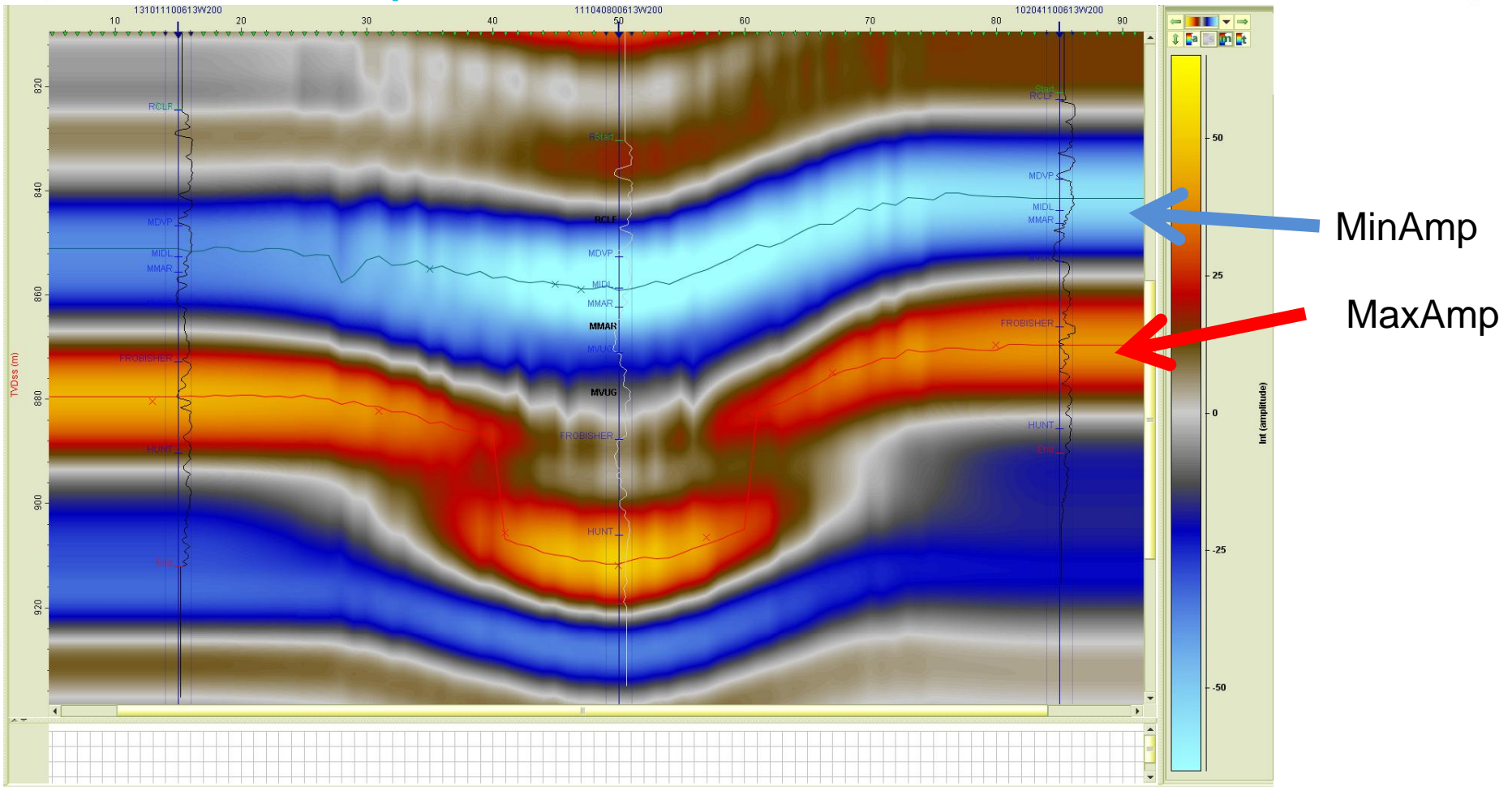
In order to understand subtle seismic amplitude changes on the thinly bedded reservoir units, Fluid and Pressure perturbations made on:

- Marly only

- Vuggy only

- Both Marly and Vuggy

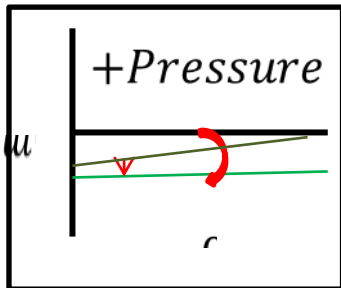
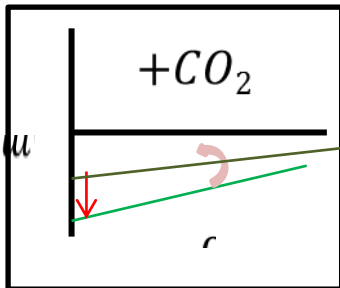
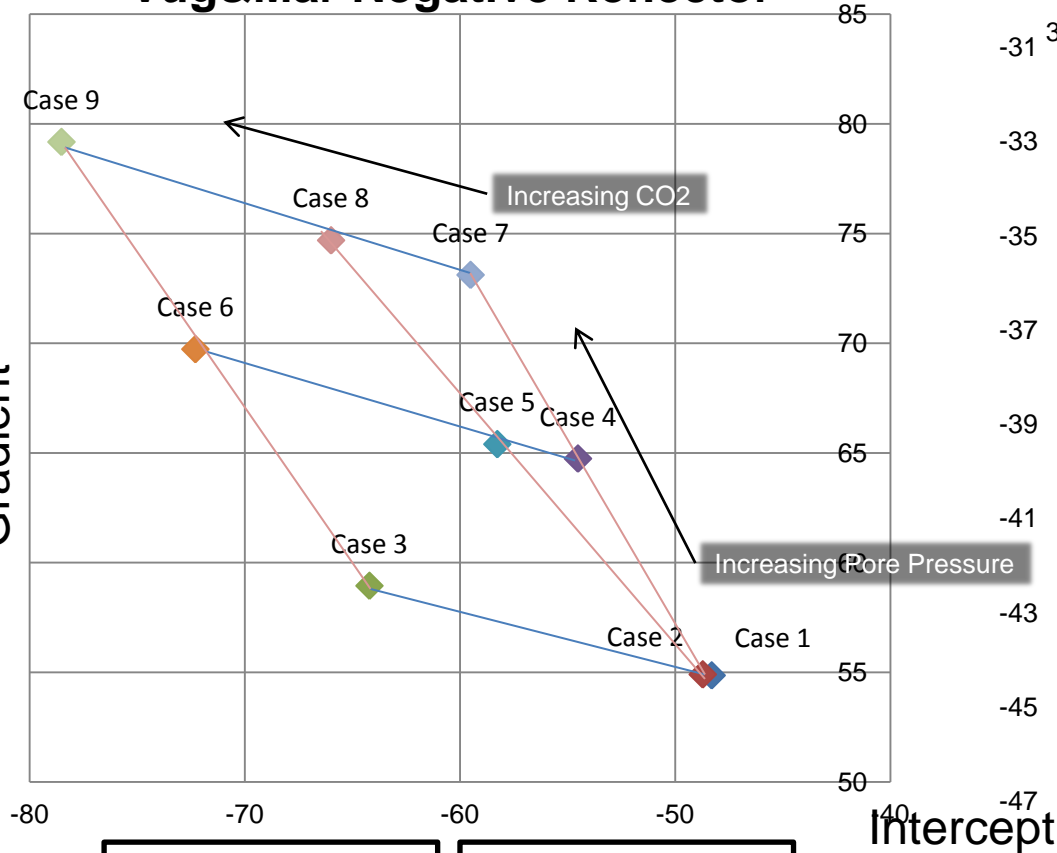
Measurement events at minimum and maximum amplitudes at reservoir.



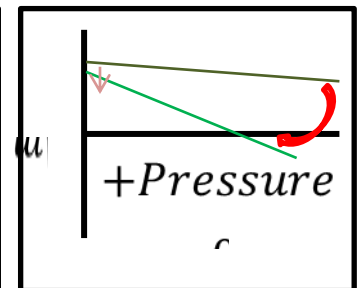
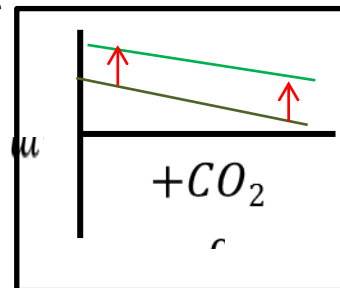
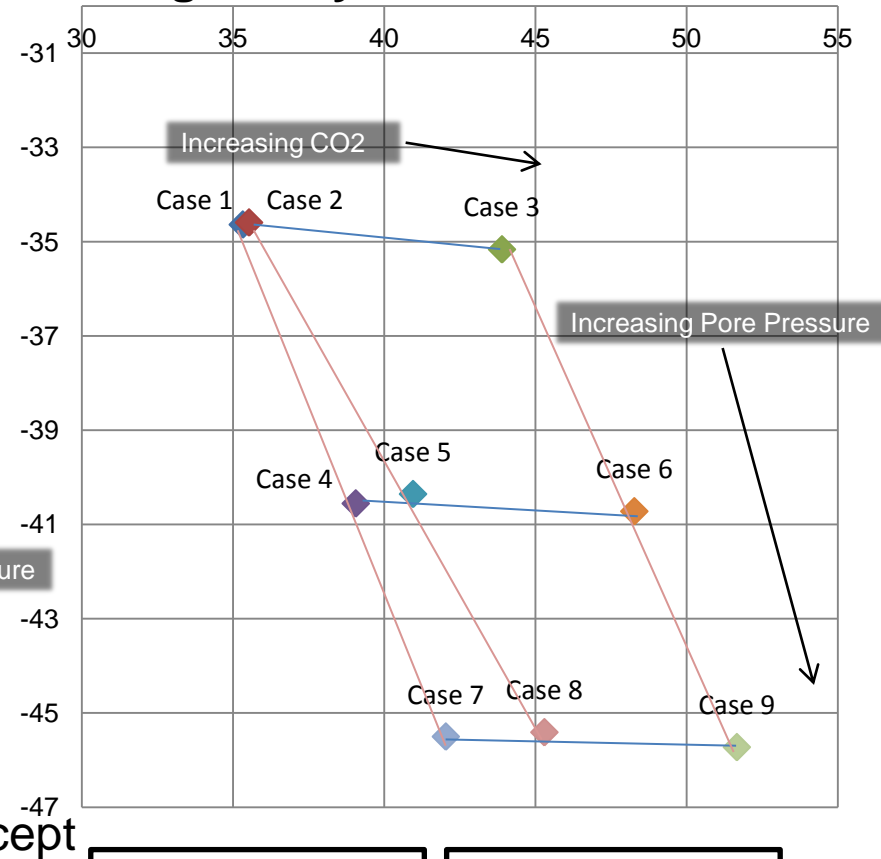
Intercept and gradient amplitude values for the various fluid cases were extracted along these max +/- reflectors. The extracted values are averaged and cross plotted on the following slides. The relative AVO effects are visualized at the bottom of the absolute amplitude plot slides. The following three slides show percent changes.

Marly & Vuggy Substitutions Int vs Grad

Vug&Mar Negative Reflector

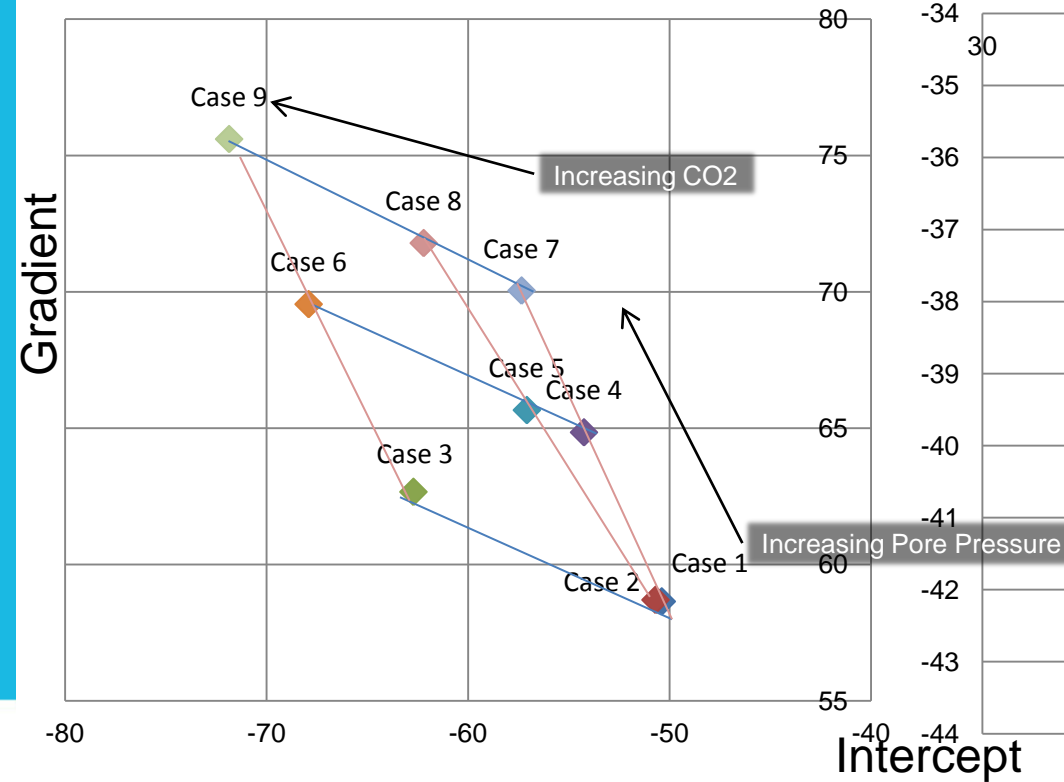


Vug&Marly Positive Reflector

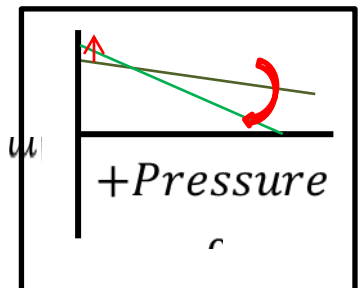
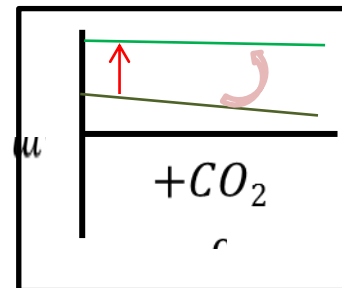
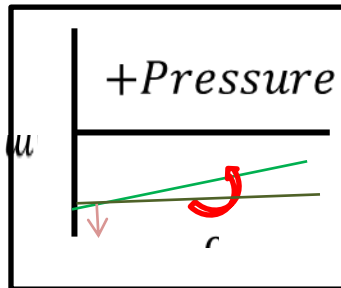
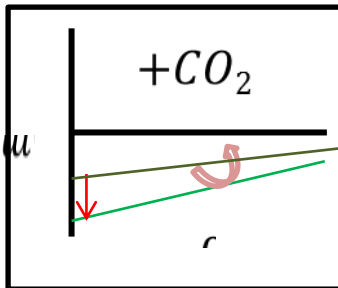
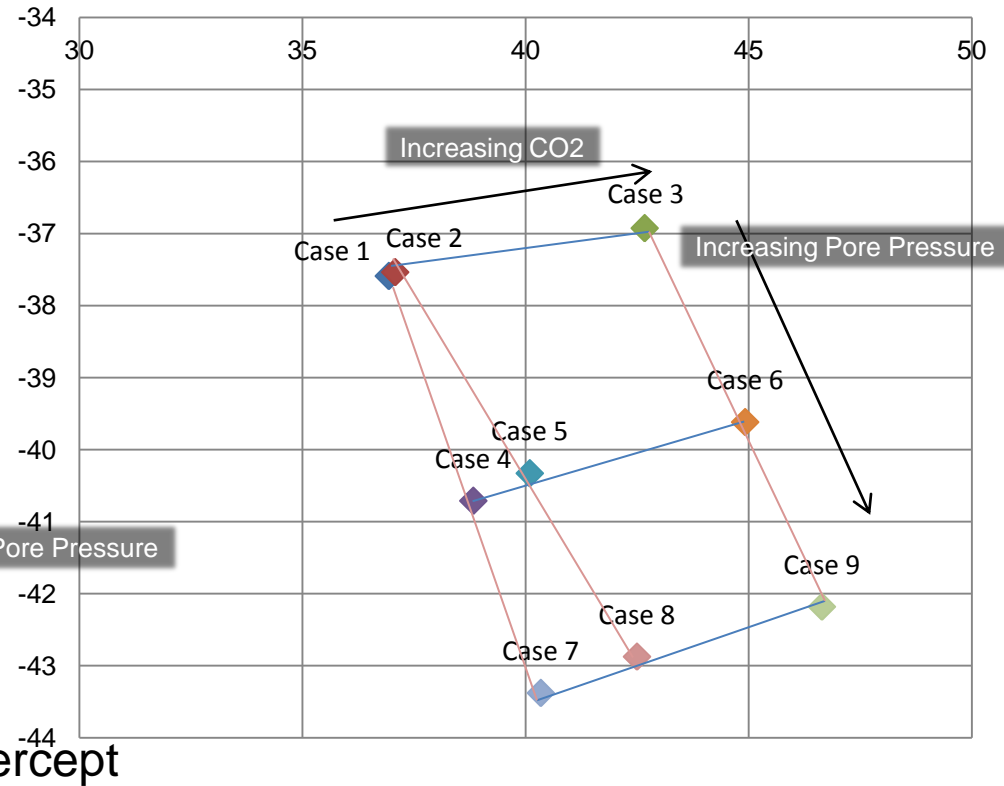


Marly Substitutions Int vs Grad

Marly Sub Negative Reflector

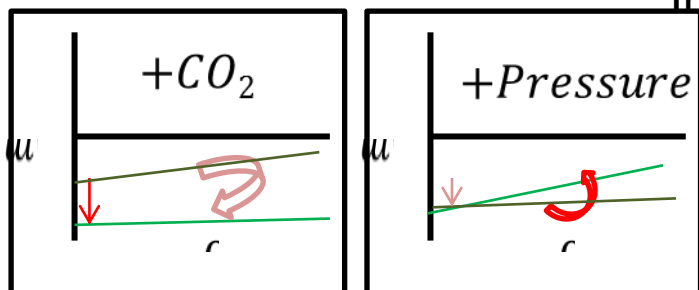
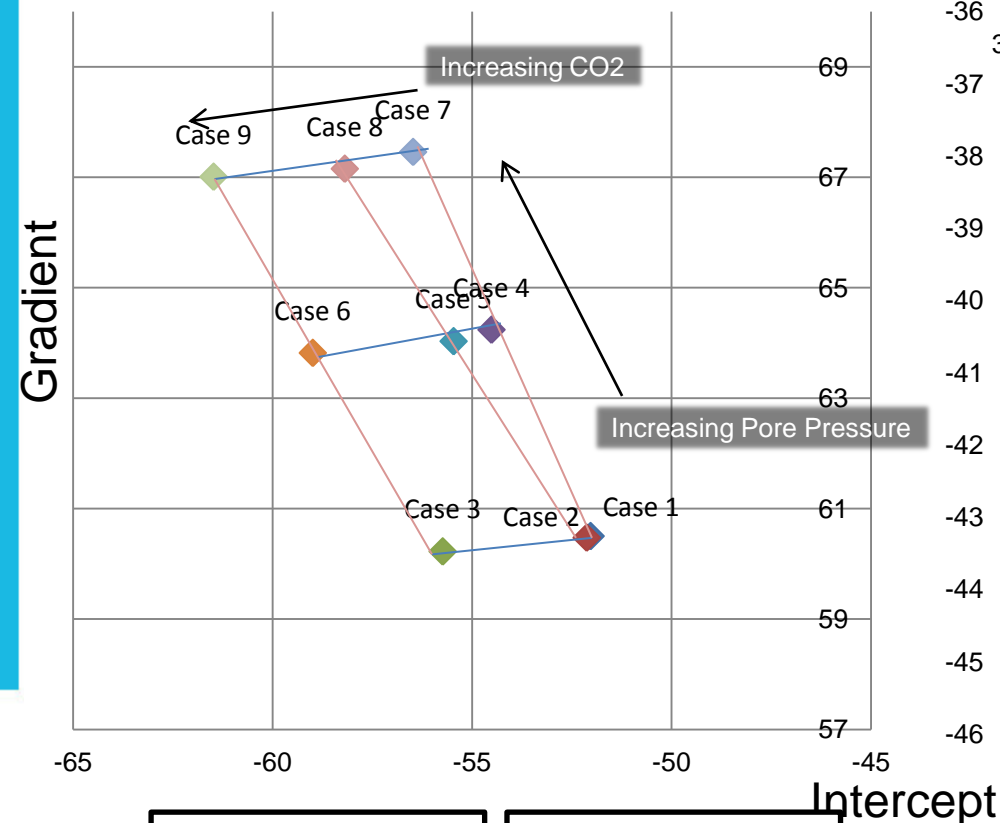


Marly Sub Positive Reflector

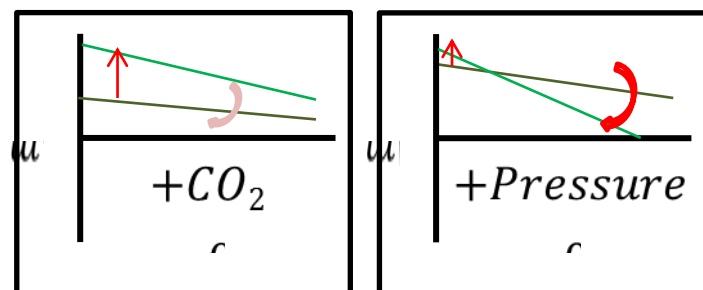
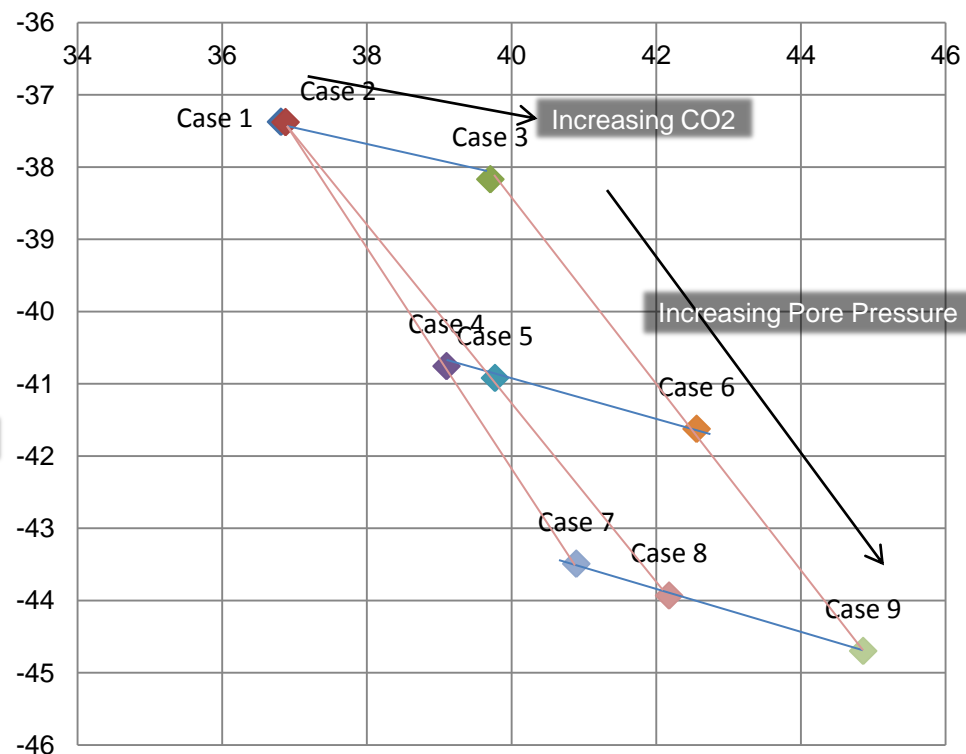


Vuggy Substitutions Int vs Grad

Vuggy Sub Negative Reflector

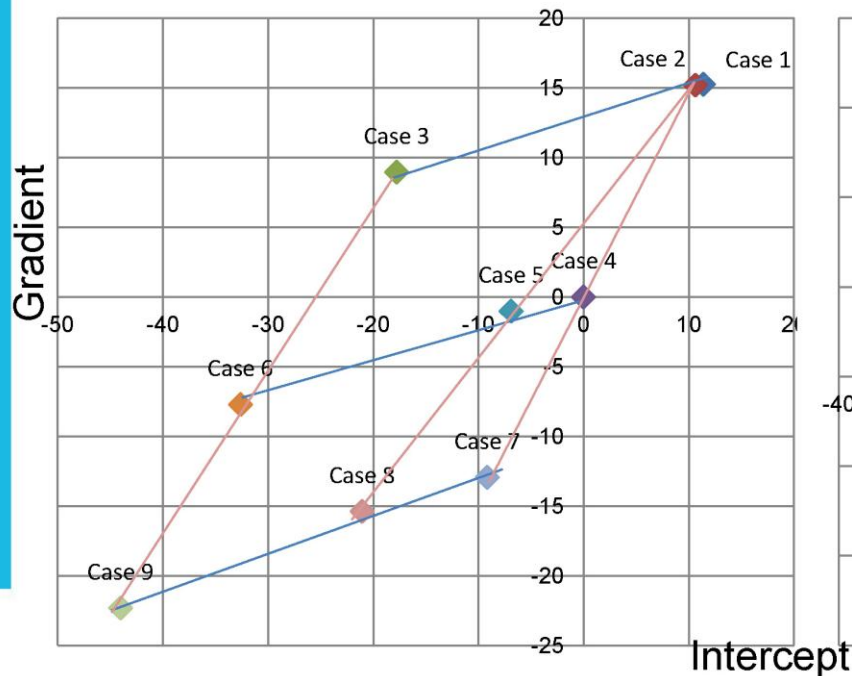


Vuggy Sub Positive Reflector

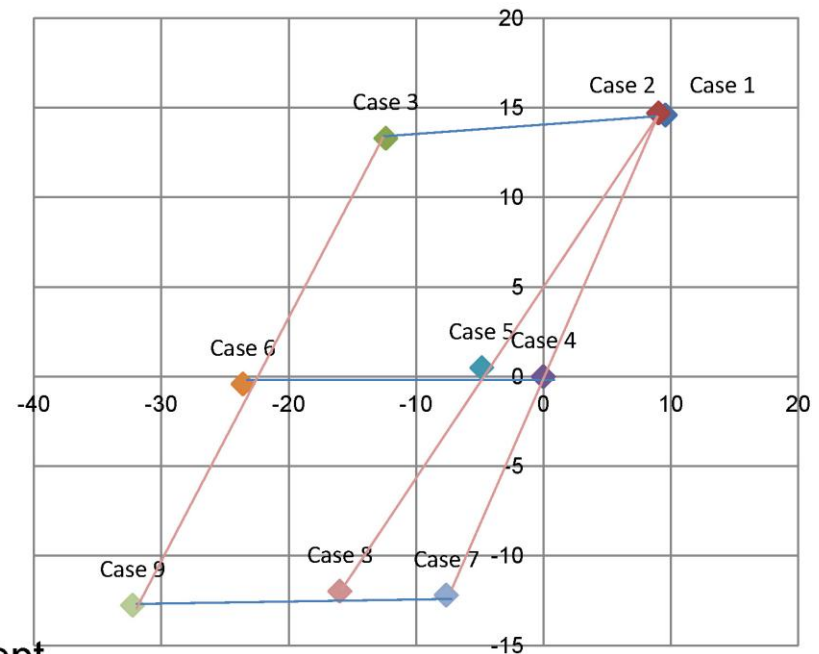


Marly & Vuggy Substitutions $\% \Delta$ Int vs Grad

Vug & Mar Negative Reflector
 $\% \Delta$ Monitor-Baseline



Vug & Marly Positive Reflector
 $\% \Delta$ Monitor-Baseline

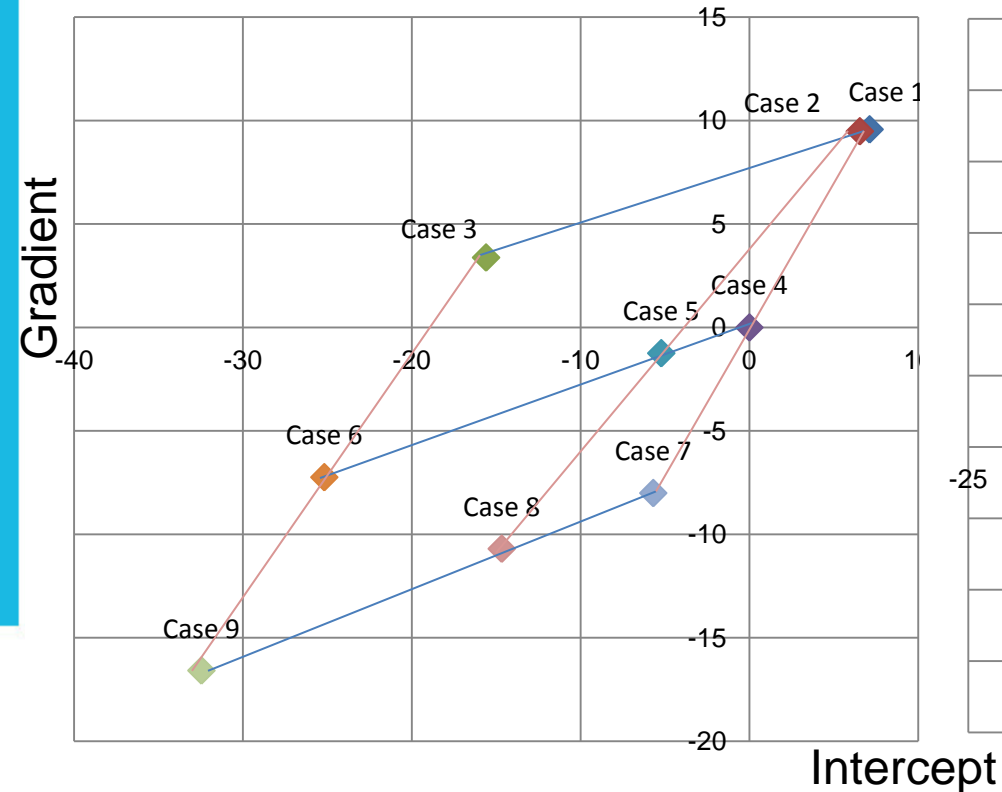


Presenter's notes: With CO₂ flooding in both units, the effect on the gradient to fluid (not pressure) seems to be minimized – slope of line decreases when both units are flooded – the sign of fluid effects on gradient in Marly and Vuggy are opposite. See Vuggy only vs Marly only vs Both. If we are sure both units are flooded, gradient changes are even more likely to be due to pressure!

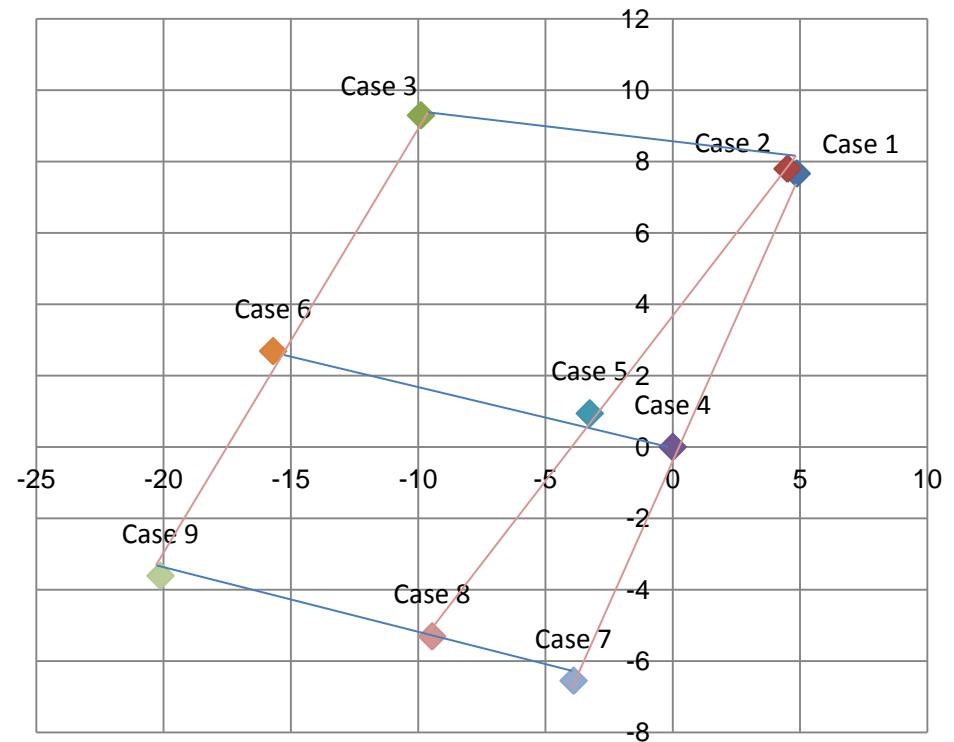
Red lines link similar fluid cases between pressure cases – they are all similar in slope

Marly Substitutions $\% \Delta$ Int vs Grad

Marly Sub Negative Reflector
 $\% \Delta$ Monitor-Baseline

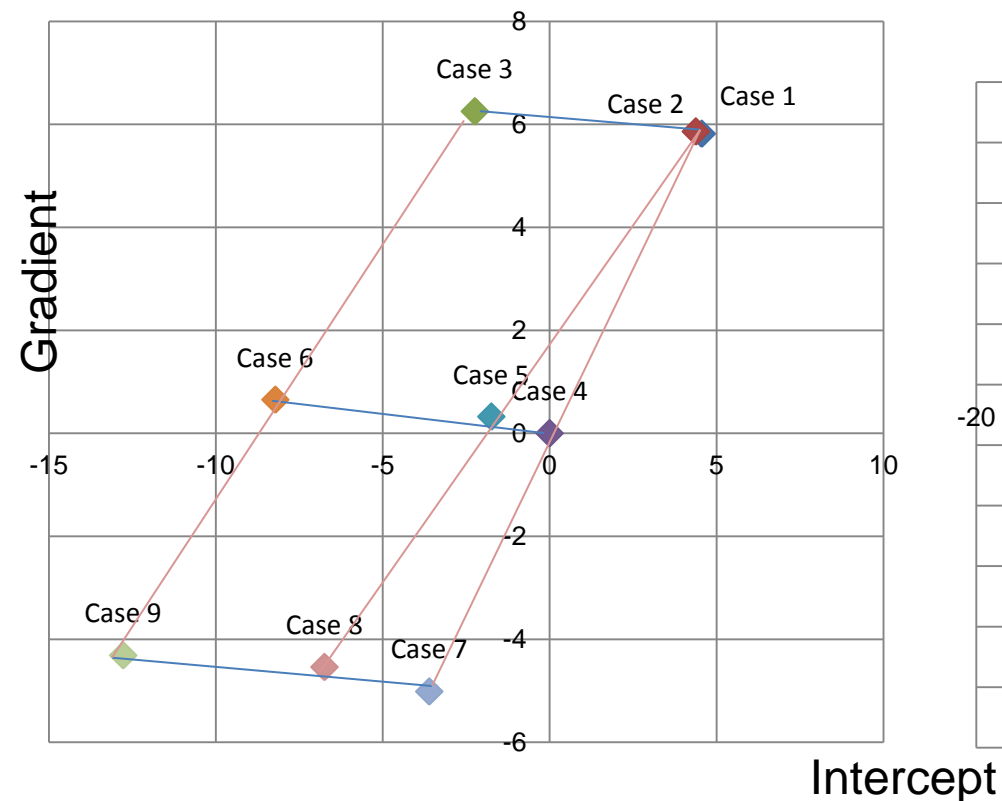


Marly Sub Positive Reflector
 $\% \Delta$ Monitor-Baseline

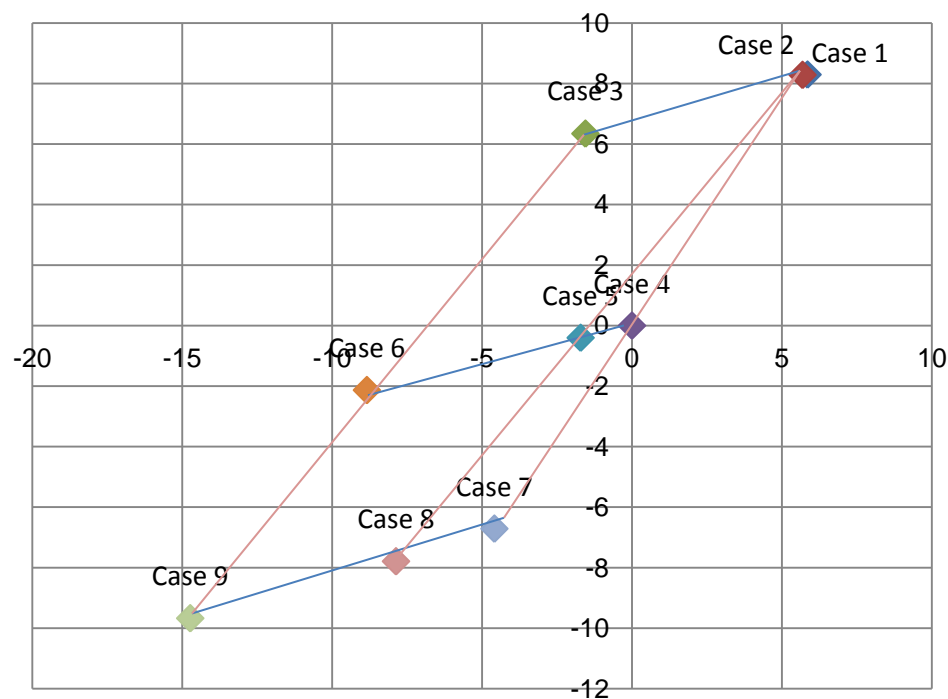


Vuggy Substitutions $\% \Delta$ Int vs Grad

Vuggy Sub Negative Reflector
 $\% \Delta$ Monitor-Baseline



Vuggy Sub Positive Reflector
 $\% \Delta$ Monitor-Baseline



4. Conclusions



- Our Rock Physics modeling approach is useful to understand both pressure and saturation effects.
- Fluid saturation effects are visible in Lambda-Rho domain.
- Pressure changes are visible in Mu-Rho domain.
- Forward seismic modeling results show that both Intercept and Gradient are affected by fluid and pressure changes in Marly & Vuggy intervals during CO₂ injection.